

/A Computer-Based Respiratory Measurement System
and a Temperature Transducer for
Monitoring Respiratory Flow Temperature /

by

MICHAEL HARRY MASTERS

B.S., Kansas State University, 1982

A MASTER'S THESIS

submitted in partial fulfillment of the requirements

for the degree

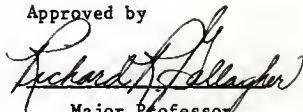
MASTER OF SCIENCE

Department of Electrical and Computer Engineering

KANSAS STATE UNIVERSITY
Manhattan, Kansas

1985

Approved by



Major Professor

LD
2668
174
1985
M3775
C.2

TABLE OF CONTENTS



A11209 480787

i

<u>Chapter</u>		<u>Page</u>
I.	INTRODUCTION	1
II.	GENERAL SYSTEM DESCRIPTION	3
	2.1 <u>The Respiratory Signals</u>	3
	2.2 <u>The Computer-Based Respiratory Measurement System</u> ..	7
III.	DESIGN OF A RAPIDLY RESPONDING TEMPERATURE TRANSDUCER	15
	3.1 <u>Transducer Design</u>	16
	3.2 <u>Calibration of the Temperature Transducer</u>	25
	3.3 <u>Temperature Transducer Testing</u>	28
IV.	CALCULATION OF RESPIRATORY VOLUMES	34
V.	SYSTEM CALIBRATION	39
	5.1 <u>Temperature Calibration</u>	39
	5.2 <u>Flow Calibration</u>	41
VI.	SYSTEM SOFTWARE	47
	6.1 <u>CAP2.CODE: A Pascal Routine</u> <u>for System Calibration</u>	49
	6.2 <u>DAP2.CODE: A Pascal Routine to</u> <u>Collect Respiratory Data</u>	52
	6.3 <u>AUTOST, CAPCRUNCH, and DAPCRUNCH:</u> <u>Auto-start and File Compaction Routines</u> ...	54
	6.4 <u>ANALYSIS: A Basic Routine to</u> <u>Calculate the Respiratory Parameters</u>	56
	6.5 <u>Computation of the Binary Volumes</u>	63
	6.6 <u>STOREHR: A Basic Routine to Store</u> <u>the Heart Rate Values</u>	65
VII.	EXPERIMENTAL VERIFICATION OF THE SYSTEM	67
	7.1 <u>Experimental Methods</u>	69
	7.2 <u>Experimental Results and Conclusions</u>	71
	7.3 <u>Subject Exercise Data</u>	74
VIII.	CONCLUSIONS	88

IX.	SUGGESTED AREAS FOR FUTURE DEVELOPMENT	90
9.1	<u>System Improvements</u>	90
9.2	<u>Storage and Extended Analysis of</u> <u>the Breath-by-Breath Results</u>	92
X.	BIBLIOGRAPHY	95
XI.	ACKNOWLEDGMENTS	97
APPENDIX I.	DEFINITION OF ACRONYMS	A1.1
APPENDIX II.	PRINCIPLES OF OPERATION OF THE PERKIN-ELMER 1100 MEDICAL GAS ANALYZER	A2.1
APPENDIX III.	DERIVATION OF RESPIRATORY PARAMETER CALCULATIONS	A3.1
APPENDIX IV.	A TUTORIAL OF THERMOCOUPLE PRINCIPLES	A4.1
APPENDIX V.	OPERATION OF THE COMPUTER- BASED RESPIRATORY MEASUREMENT SYSTEM	A5.1
A5.1	<u>The Computer System: An Overview</u>	A5.2
A5.2	<u>System Power up</u>	A5.5
A5.3	<u>Configuration of the ASCII Data Disks</u>	A5.9
A5.3.1	Procedure for setting the status of an ASCII data disk to empty	A5.10
A5.3.2	Changing the volume label of a disk	A5.11
A5.4	<u>Calibration and Data Collection</u>	A5.12
A5.4.1	Operator instructions for calibration of the CBRMS	A5.12
A5.4.2	Operator instructions for collection of respiratory data with the CBRMS	A5.17
A5.5	<u>Compaction of the Calibration</u> <u>and Respiratory Data</u>	A5.19
A5.6	<u>Data Analysis and Display</u>	A5.22
A5.7	<u>Storage and Display of the Heart Rate Data</u> ...	A5.29
APPENDIX VI.	PASCAL PROGRAM DOCUMENTATION AND LISTINGS	A6.1
A6.1	<u>CAP2: a Pascal</u> <u>Routine for System Calibration</u>	A6.1
A6.1.1	Ask_Y_or_N Procedure	A6.2

A6.1.2	BEEP Procedure	A6.2
A6.1.3	BIT_HI and BIT_TST Procedures	A6.2
A6.1.4	Calc_Incr_vol Procedure	A6.3
A6.1.5	CAP2 Procedure	A6.4
A6.1.6	CLKSET Procedure	A6.7
A6.1.7	DATA_COLLECT Procedure	A6.8
A6.1.8	FLOWCAL Procedure	A6.9
A6.1.9	GASCAL Procedure	A6.14
A6.1.10	HOLD_UP Procedure	A6.16
A6.1.11	Line_feed Procedure	A6.16
A6.1.12	Rel_viscos Function	A6.17
A6.1.13	TEMPCAL Procedure	A6.17
A6.1.14	Valid_pointer Procedure	A6.20
A6.1.15	CAP2 Program Listing	A6.21
A6.2	<u>DAP2: a Pascal Routine for</u> <u>Collection of Respiratory Data</u>	A6.49
A6.2.1	BEEP Procedure	A6.49
A6.2.2	BIT_HI and BIT_TST Procedures	A6.49
A6.2.3	CHECK_IF_DISK_FULL Procedure	A6.49
A6.2.4	CHECK_SATURATION Procedure	A6.50
A6.2.5	CLKSET Procedure	A6.51
A6.2.6	DAP2 Procedure	A6.51
A6.2.7	DATA_COLLECT Procedure	A6.52
A6.2.8	DATA_STORAGE Procedure	A6.54
A6.2.9	HOLD_UP Procedure	A6.56
A6.2.10	Line_feed Procedure	A6.56
A6.2.11	MAXMIN Procedure	A6.57
A6.2.12	SET_DISK_FULL_FLAG Procedure	A6.58
A6.2.13	DAP2 Program Listing	A6.60
A6.3	<u>ASCII_CONF: a Pascal Routine to Configure</u> <u>the ASCII Data Disks to Accept Data</u>	A6.74
A6.3.1	ASCII_CONF Procedure	A6.74
A6.3.2	BEEP Procedure	A6.75

A6.3.3	Line_feed Procedure	A6.75
A6.3.4	ASCII_CONF Program Listing	A6.76
APPENDIX VII. BASIC PROGRAM DOCUMENTATION AND LISTINGS		
A7.1	<u>Definition of the COMMON Blocks</u>	A7.1
A7.2	<u>Description of the Respiratory Variable Array</u> .	A7.7
A7.3	<u>AUTOST: a Basic Program</u> <u>Linking all Basic Programs</u>	A7.8
A7.3.1	AUTOST Program Listing	A7.10
A7.4	<u>CAPCRUNCH: a Basic Program Which Compacts</u> <u>the ASCII Calibration Data</u> <u>Collected by CAP2 to Numeric Format</u>	A7.13
A7.4.1	The Main Routine of CAPCRUNCH	A7.13
A7.4.2	File_locations Subroutine	A7.16
A7.4.3	CAPCRUNCH Program Listing	A7.18
A7.5	<u>DAPCRUNCH: a Basic Program Which Compacts</u> <u>the ASCII Respiratory Data</u> <u>Collected by DAP2 to Numeric Format</u>	A7.22
A7.5.1	The Main Routine of DAPCRUNCH	A7.22
A7.5.2	File_locations Subroutine	A7.24
A7.5.3	Rd_and_crunch Subroutine	A7.25
A7.5.4	Write_data Subroutine	A7.26
A7.5.5	DAPCRUNCH Program Listing	A7.27
A7.6	<u>ANALYSIS: a Basic Program Which</u> <u>Computes the Respiratory Parameters</u>	A7.31
A7.6.1	The Main Routine of ANALYSIS	A7.31
A7.6.2	Avg_breath Subroutine	A7.43
A7.6.3	Avg_window Subroutine	A7.45
A7.6.4	Calc_sig_val Subroutine	A7.46
A7.6.5	Disp_results Subroutine	A7.50
A7.6.6	Expanded_dump Subroutine	A7.52
A7.6.7	Expiration Function	A7.53
A7.6.8	Inspiration Function	A7.54
A7.6.9	Make_axes Subroutine	A7.55
A7.6.10	Max_co2_ptr Function	A7.57
A7.6.11	Max_min Subroutine	A7.58

A7.6.12 Plot_values Subroutine	A7.59
A7.6.13 Print_values Subroutine	A7.61
A7.6.14 Rel_viscos Subroutine	A7.64
A7.6.15 View Subroutine	A7.65
A7.6.16 ANALYSIS Program Listing	A7.66
A7.7 <u>STOREHR: a Basic Program Which Stores the Heart Rate Values</u>	A7.110
A7.7.1 The Main Routine of STOREHR	A7.110
A7.7.2 Load_autost Subroutine	A7.110
A7.7.3 Load_plot Subroutine	A7.111
A7.7.4 Options Subroutine	A7.111
A7.7.5 STOREHR Program Listing	A7.112
A7.8 <u>TXDCR_VALS: a Basic Program Which Computes the Component Values of the Temperature Transducer</u>	A7.115
A7.8.1 The Main Routine of TXDCR_VALS	A7.115
A7.8.2 Enter_rfrs Subroutine	A7.115
A7.8.3 Enter_rs Subroutine	A7.116
A7.8.4 Print Subroutine	A7.116
A7.8.5 Print_results Subroutine	A7.118
A7.8.6 Txdcr_range Subroutine	A7.119
A7.8.7 Vr Subroutine	A7.119
A7.8.8 Vtc Function	A7.120
A7.8.9 TXDCR_VALS Program Listing	A7.121

ABSTRACT

LIST OF FIGURES

<u>Figure</u>		<u>Page</u>
2.1.1	A respiratory model for understanding breath-by-breath measurements made at the mouth ...	4
2.1.2	The respiratory signals appearing at the mouth	5
2.2.1	The block diagram of the CBRMS	8
2.2.2	Example of average data obtained from 125 Watts of steady-state exercise	10
2.2.3	An illustration of the window breath averaging technique ..	12
2.2.4	Example of the tabular output obtained by window averaging the breath-by-breath data	14
3.1.1	The block diagram of the temperature transducer	16
3.1.2	The temperature transducer; The power supply	17
3.1.3	The output of TXDCR_VALS program	24
4.1	The denominator terms of Wilke's equation versus respiratory flow	37
5.1.1	The equipment setup for the calibration of the temperature transducer	40
5.2.1	The variation of the relative viscosity throughout the respiratory cycle	42
5.2.2	Equipment setup for the calibration of the PTG	43
6.1	Organization of the CBRMS software	48
6.1.1	Calibration program, CAP2	50
6.1.2	Flow calibration Procedure	51
6.2.1	Data acquisition program, DAP2	53
6.3.1	AUTOST, CAPCRUNCH, and DAPCRUNCH programs	55
6.4.1	Data analysis program, ANALYSIS	57
6.4.2	Display of the breath-by-breath data	60
6.4.3	The breath averaging procedure	61
6.4.4	The window averaging procedure	62
6.5.1	Computation of the binary volumes	64
6.6.1	The heart rate storage program, STOREHR	66
7.1.1	Experimental setup used to cycle a known volume of gas under known conditions through the PTM	70
7.2.1	Typical CBRMS signals obtained from the Harvard respirator	73
7.3.1	Example respiratory signals	75

7.3.2	Graphical display of the respiratory parameters	77
7.3.3	O ₂ consumption and CO ₂ production responses	79
7.3.4	Example of the tabular output of the CBRMS using a 20 second window	81
7.3.5	Example of the tabular output of the CBRMS using a 90 second window	82
7.3.6	O ₂ consumption versus work load	85
7.3.7	CO ₂ production versus work load	85
7.3.8	Inspiratory ventilation versus work load	86
7.3.9	Inspiratory tidal volume versus work load	86
7.3.10	Respiratory quotient, R, versus work load	87
9.2.1	Flowchart for averaging the breath- by-breath results from several subjects or different runs of the same subject	94
A2.1	AGC block diagram of the GMS	A2.2
A3.2	Flow, flow temperature, and water vapor signals	A3.3
A4.1	The basic thermocouple circuit	A4.1
A4.2	Hardware compensation of the reference junction temperature	A4.4
A7.2.1	Construction of the respiratory variable array	A7.8

LIST OF TABLES

<u>Table</u>		<u>Page</u>
3.3.1	The calculated water bath temperature, measured bath temperature, and the associated error versus output voltage of the compensator for three trials	29
3.3.2	The calculated water bath temperature, measured bath temperature, and the associated error versus output voltage of the temperature transducer for three trials	30
3.3.9	Calculated flow sensitivity to temperature errors in the flow temperature versus the flow temperature	33
4.1	Linear approximations of pure gas viscosities between 20°C and 40°C	36
4.2	Average values of the denominator terms of Wilke's equation	37
4.3	Modified linear approximations for pure gas viscosities between 20°C and 40°C	38
7.2.1	The average conditions of the flow gas	71
7.2.2	Experimental results which compare the calculation of a known volume with and without temperature and viscosity corrections	72
7.3.1	Average respiratory parameters	83
A3.1	Linear approximations of pure gas viscosities between 20°C and 40°C	A3.2
A4.1	True thermocouple voltage, second order thermocouple voltage estimate, and associated error value versus sensing junction temperature	A4.2
A5.1.1	Computer system peripheral designations	A5.4

Chapter I. INTRODUCTION

A primary interest of the respiratory physiologist is the ability to obtain a quantitative measure of ventilation, the exchange of oxygen and carbon dioxide between the alveolar spaces in the lung and the venous blood. Such measurements may be approximated by measuring the gas exchange between the subject and the atmosphere. Classical ventilation measurements (e.g. bag techniques) rely on the collection of expired gases for several respiratory cycles [14]. Such measurements yield average ventilation values so that only steady-state responses may be considered. By making the ventilatory measurements on a per breath basis the ventilatory response to transient or short duration stimuli is possible while, by totaling the per breath values, study of the response to a steady-state stimulus is maintained. These breath-by-breath measurements may provide both the clinician and the researcher new insights into the health or conditioning of a subject [6,14].

Recordings at the mouth of the bi-directional (inspiratory and expiratory) respiratory gas flow and flow temperature signals and the concentration signals of the component gases yield a complete history of the gas exchanged between the atmosphere and the subject. Integration of the flow, which is converted to constant and standard conditions using the flow temperature and ambient conditions, over an inspiratory cycle and over an expiratory cycle yields the respective inspiratory and expiratory tidal volumes. Also, the flow signal can be multiplied by the individual gas concentrations to obtain flows of the individual gases. These gas flows can be integrated to obtain their respective tidal volumes. The difference between the inspiratory volume and the expiratory volume of a gas yields the volume of gas exchanged for the respiratory cycle. These per breath tidal volumes and exchanged volumes can be converted to minute values by dividing by the respiratory cycle time. Also, several breath-by-breath values may be totaled and averaged to obtain an average response over a specified period of time.

With current technology, transducers are available to monitor the necessary signals to make the respiratory measurements. Pneumotachometer and low inertia turbine flow transducers provide the ability to monitor bi-directional respiratory flow. Rapidly responding gas analyzers have the ability to monitor the rapidly varying respiratory gas concentration signals. A rapidly responding temperature transducer can monitor the flow temperature signal. These signals may be digitally recorded with a computer-based data

acquisition system. The computer provides the ability to numerically integrate the gas flows. The computer also provides the flexibility to provide a variety of techniques for data display.

A Computer-Based Respiratory Measurement System (CBRMS) has been developed by Creel [4] and Riblett [13] to monitor four respiratory signals; respiratory flow, fractional concentration of O_2 and CO_2 in the dry gas, and respiratory flow temperature. A Godart PneumoTachoGraph (PTG), using a Fleisch #2 PneumoTachoMeter (PTM), is used to transduce the respiratory flow signal. A Perkin-Elmer 1100 Medical Gas Analyzer (the acronym GMS, Gas Mass Spectrometer, is used to refer to the gas analyzer) is used to transduce the dry gas concentration signals of O_2 , F_{O_2} , and CO_2 , F_{CO_2} . The design of a rapidly responding temperature transducer based on a 0.001 inch chromel-constantan thermocouple is presented in this study. This transducer is used to monitor the respiratory flow temperature signal.

Using the fore-mentioned signals the CBRMS can make a variety of ventilation measurements. These breath-by-breath ventilation measurements are a measure of gas exchange between the lungs and the atmosphere on a per breath basis and approximate, assuming no change in pulmonary gas stores, alveolar ventilation; the exchange of respiratory gases between the alveolar spaces and the venous blood. Other studies have extended similar systems, using the same measured signals, to calculate the true alveolar gas exchange on a breath-by-breath basis [2] yielding additional insight into transient changes in ventilation. An effort to provide such an extension to the CBRMS of this study is currently under way with promising preliminary results [12].

Chapter II. GENERAL SYSTEM DESCRIPTION

To appreciate the types of respiratory measurements made with the Computer-Based Respiratory Measurement System (CBRMS) it is necessary to have a general understanding of the respiratory signals and how the system monitors, records, and manipulates these signals. The measurements necessary for assessing respiratory ventilation are the various gas volumes (air, oxygen, carbon dioxide), both on a tidal and time rate basis and respiratory frequency. Obtaining these measurements for each breath allows investigation of the respiratory system's transient and, by averaging these breath-by-breath values, steady-state responses.

An overview of the CBRMS is presented in this chapter while the details of the system are explained later. This overview provides the respiratory physiologist the necessary understanding to make confident respiratory function measurements. Prior to the overview a brief discussion of the respiratory signals correlated with the various stages of the respiratory cycle is presented. Reference to several introductory physiology texts provides the necessary description of the respiratory system and defines the necessary terminology.

2.1 The Respiratory Signals

Investigation of respiratory signals appearing at the mouth is essential in understanding how a system may be developed which can take these signals and compute values for the respiratory variables. Consider the respiratory model shown in Figure 2.1.1. This model is a simple representation of the pulmonary system.

The model contains the necessary detail for understanding the computation of the breath-by-breath gas volumes based on measurements made at the mouth. The two volumes included in the model are the constant dead space volume, including that added by the PTM, and the lung volume which varies throughout the respiratory cycle. The lung volume includes the various pulmonary volumes (tidal volume, inspiratory reserve volume, expiratory reserve volume, and residual volume) and the pulmonary capacities (functional residual capacity, inspiratory capacity, vital capacity, total lung capacity) [6]. The alveolar oxygen consumption and carbon dioxide production are also included in the model. These values may be derived from the mouth values

using this model [2,12].

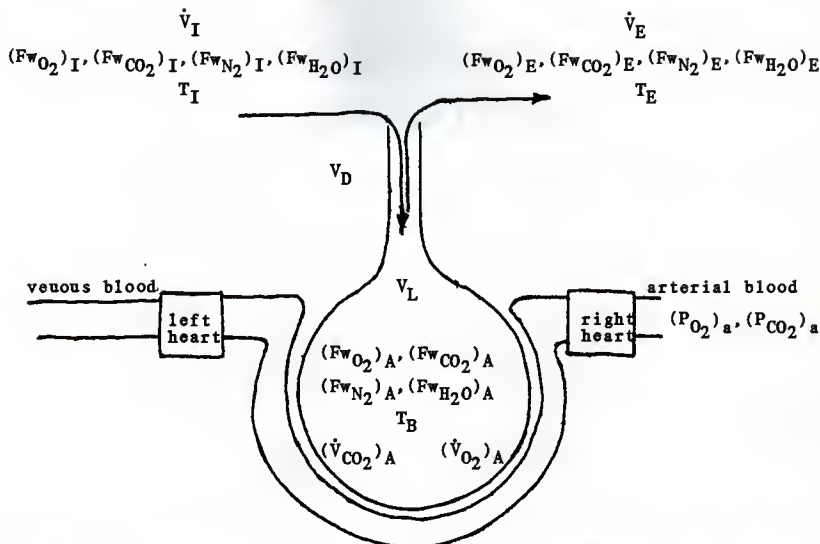


Figure 2.1.1 A respiratory model for understanding breath-by-breath measurements made at the mouth.

A mask containing a heated PTM flow transducer is placed over the subject's mouth and nose. Mounted in the PTM are the GMS and temperature transducer probes. The heated PTM alters the respiratory system's dead space, resistance, and inspiratory temperature and is the only transducer which has an effect on the respiratory system. The specific effects of the heated PTM are not investigated in this study.

The respiratory gas movement and composition can be summarized by monitoring six variables at the mouth. These variables are total gas flow, the gas concentrations, and the gas temperature. Figure 2.1.2 shows these variables during two respiratory cycles. These signals can be correlated with the inspiratory (negative flow and the dotted lines) and expiratory (positive flow and the solid lines) phases of the respiratory cycle.

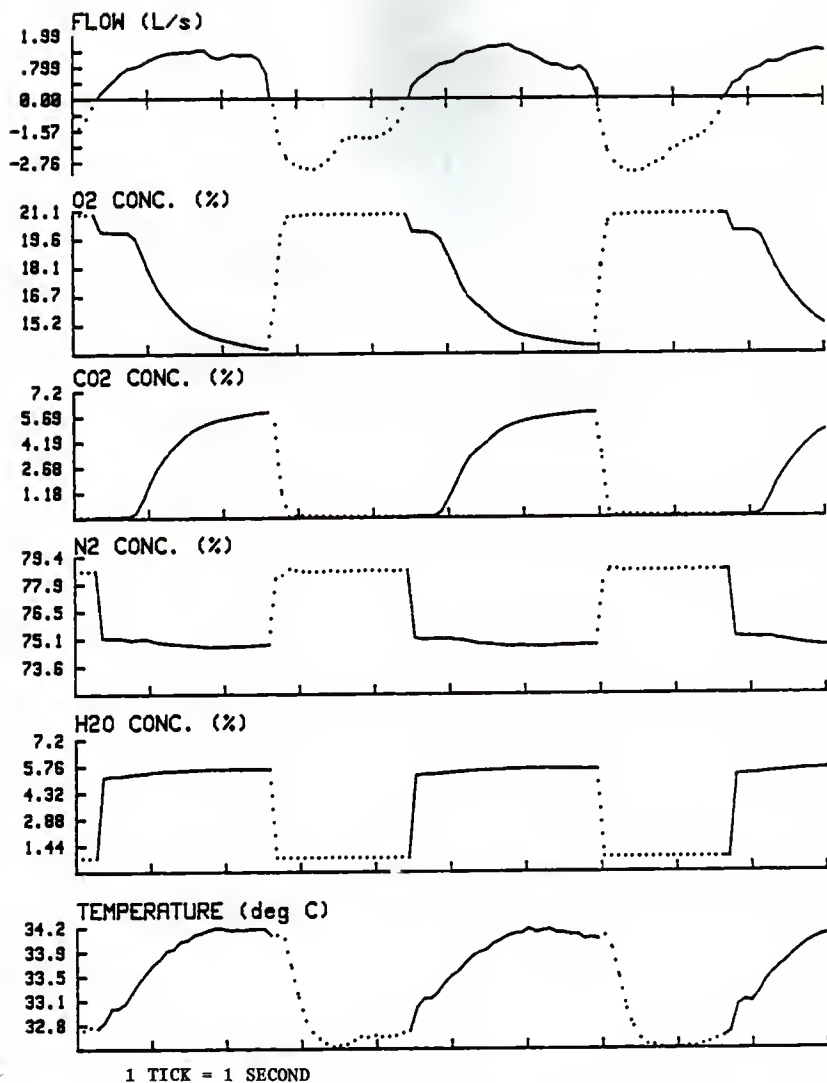


Figure 2.1.2 The respiratory signals appearing at the mouth.

During inspiration the gas composition signals reflect room air conditions. Room air contains oxygen, nitrogen, carbon dioxide, water vapor, and a small (negligible) amount of fixed gases. Neglecting the volume of water vapor (dry room air) the concentrations of oxygen, carbon dioxide, and nitrogen are 20.93%, 0.04%, and 78.00% respectively. These concentrations are slightly diluted by the amount of water vapor contained in room air.

Room air water vapor concentration is found by observing the ambient conditions. If the barometric pressure is approximately one atmosphere (760 torr) saturated water vapor pressure is dependent only upon temperature. With a typical ambient temperature of 21°C the saturated water vapor pressure is 18.65 torr. The actual water vapor pressure, P_{H_2O} , is found by multiplying the saturated value by the relative humidity. The water vapor concentration, F_{H_2O} , is found by dividing the actual vapor pressure by the barometric pressure. These values under typical ambient conditions of 21°C temperature, 30% relative humidity, and a 730 torr barometric pressure are

$$P_{H_2O} = 18.65 \cdot 30.0\% = 5.60 \text{ torr}$$

$$F_{H_2O} = \frac{5.60}{730} = 0.76\%$$

Even though the gas is heated by the PTM, the water vapor concentration is computed with the ambient temperature.

The actual gas concentrations may be found by multiplying the individual dry concentrations by the factor $100\% - F_{H_2O}$ (refer to Appendix II). This air passes through the dead space and into the alveolar spaces (assuming the inspiratory tidal volume is larger than the dead space) where it is mixed with the alveolar gas.

During expiration, the gas appearing at the mouth has been in contact with moist surfaces of the trachea and the alveoli; therefore, it is assumed to be saturated. The saturated water vapor pressure is found using the gas temperature signal (the saturated water vapor pressure is a function of temperature only). The water vapor concentration is found by dividing the saturated water vapor pressure by the barometric pressure.

Upon initial expiration, the gas appearing at the mouth comes from the dead space. Since, by definition, no gas exchange occurs with the blood in the dead space, the dead space gas contains the same amounts of O_2 , CO_2 , and N_2 as room air. However, there is a dilution of the dead space gas with

water vapor. This dilution causes the step drop in the O_2 and N_2 concentration signals. The F_{CO_2} signal does not reflect this dilution because of the minimal amount of CO_2 present in the upper portions of the dead space.

With continued expiration the alveolar gas arrives at the mouth causing the drop in O_2 concentration and rise in the CO_2 concentration. The alveolar gas, due to gas exchange with the venous blood, contains a higher concentration of CO_2 (4% to 8%) and lower concentration of O_2 (12% to 17%). The O_2 and CO_2 concentrations flatten out but continue to change as the alveolar gas arrives at the mouth. The slight continual changes are due to the ongoing exchange of O_2 and CO_2 with the venous blood. Nitrogen is not exchanged with the blood so that there is minimal variation in alveolar nitrogen concentration.

With the onset of inspiration the gas composition immediately reverts to room air conditions.

2.2 The Computer-Based Respiratory Measurement System

A system has been developed by Creel [4] and modified by Riblett [13] which provides the ability to monitor respiratory signals. A rapidly responding temperature transducer has been added to arrive at the present system. The present system, shown in Figure 2.2.1, has the ability to record four of the subject's respiratory signals; respiratory flow, dry fractional concentration of O_2 and CO_2 , and respiratory flow temperature. The subject is placed on a bicycle ergometer. The GMS samples the respiratory gas and produces an output voltage proportional to F_{O_2} and an output voltage proportional to F_{CO_2} . The PTG produces an output voltage proportional to the differential pressure developed across the screen of a PTM. This differential pressure is related to the flow through the PTM. A temperature transducer has been designed (Chapter III) to produce an output voltage related to the temperature of the respiratory flow gas. These voltages are sampled and digitized with a Data Acquisition Module (DAM) [5]. The digital samples are collected with the computer system (refer to Section A5.1 of Appendix V for an overview of the computer system). The computer system can relate these samples to the respiratory signals. An ECG telemetry system is used to monitor the subject's heart rate and record the heart rate on the termination of thirty second periods.

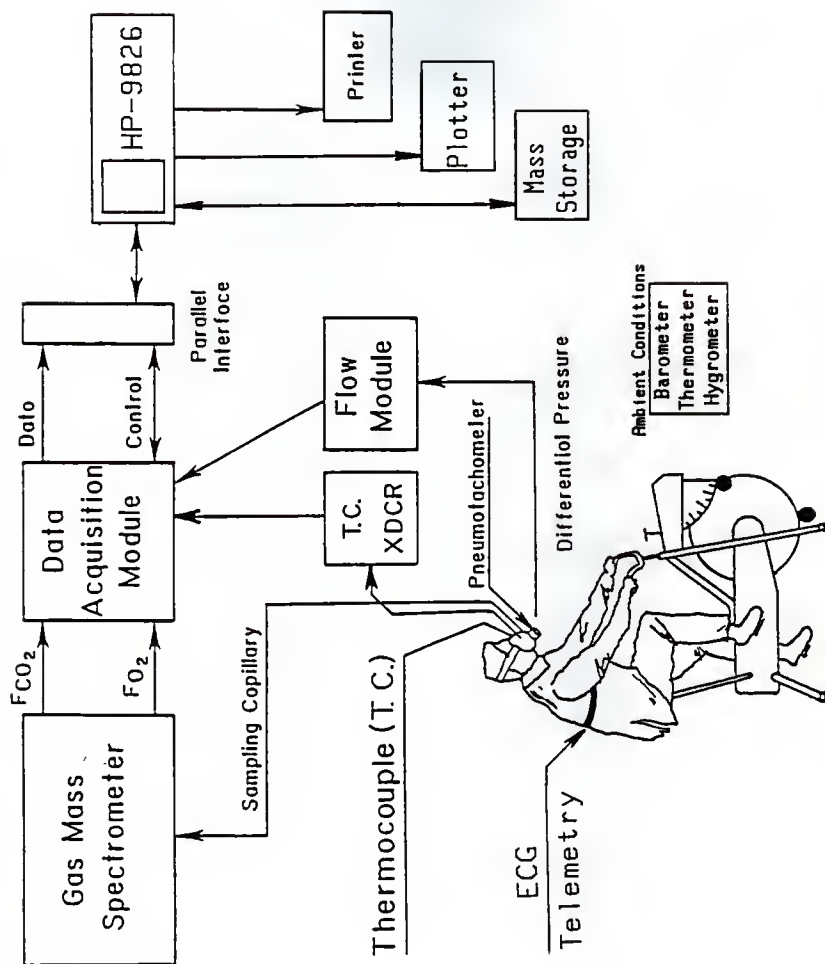


Figure 2.2.1 The block diagram of the CBRMS.

The calculated gas viscosity is used to convert the digitized differential pressure signal to a flow signal. This flow is converted to STPD conditions using both the temperature signal and the ambient conditions. This STPD flow is integrated over an inspiration to obtain an inspiratory tidal volume, V_I , and an expiration to obtain an expiratory tidal volume, V_E . These tidal volumes are then converted to BTPS conditions. The STPD flow is multiplied by the F_{CO_2} signal and the result is similarly integrated to obtain the STPD volume of CO_2 inspired and the volume expired. The same procedure is followed with the O_2 signal to obtain the volume of O_2 inspired and O_2 expired. Taking the difference of inspiratory and expiratory O_2 and CO_2 volumes yields the STPD volumes of O_2 consumed, V_{O_2} , and CO_2 produced, V_{CO_2} , during the breath. These volumes are calculated and displayed in tabular form, one line per breath, for every breath in a selected time window. The breath-by-breath tidal volumes (V_I and V_E), volume of O_2 consumed (V_{O_2}), and volume of CO_2 produced (V_{CO_2}) are expressed as minute volumes by dividing by the duration of the respiratory cycle (in minutes). The individual breath-by-breath respiratory quotient, R , and respiratory frequency values are also computed. The minute values, respiratory quotient, and respiratory frequency are not displayed in the tabular format but are retained for later display.

After every breath in the window has been analyzed the average values for the time window are displayed. These values include:

1. the inspiratory and expiratory volumes
 - a. tidal volume (L_{BTPS}/breath)
 - b. O_2 volume (L_{STPD}/breath)
 - c. CO_2 volume (L_{STPD}/breath),
2. the volume of O_2 consumed (L_{STPD}/breath),
3. the volume of CO_2 produced (L_{STPD}/breath),
4. the minute ventilation values
 - a. inspiratory ventilation (L_{BTPS}/min)
 - b. expiratory ventilation (L_{BTPS}/min)
 - c. O_2 consumption (L_{STPD}/min)
 - d. CO_2 production (L_{STPD}/min),
5. the respiratory quotient, and
6. the respiratory frequency (breaths/min).

The average minute values are found by dividing their respective total volume for the window by the total respiratory time. The average respiratory

quotient, R , is found by dividing the total volume of CO_2 produced by the total volume of O_2 consumed. The average respiratory frequency is equal to the total number of breaths analyzed divided by the total respiratory time.

SUBJECT IDENTIFIER: Subject A

DATE: NOV/02/1984

COMMENT: 125 Watt Exercise; Steady State

Summary data and average values

	Data Point	Time (sec)
Beginning analysis point:	11250	284.98
The first inspiration:	11272	285.42
The last inspiration:	15553	371.04
Ending analysis point:	15750	374.98

Inspiratory minnte volume = -56.2 liters per minnte BTPS

Expiratory minnte volume = 52.6 liters per minnte BTPS

O_2 consumed per minnte = -2.430 liters per minnte STPD

CO_2 produced per minute = 1.895 liters per minnte STPD

RESPIRATORY QUOTIENT = .780

Inspiratory tidal volume = -2.2183 liters BTPS

Expiratory tidal volume = 2.0749 liters BTPS

Respiratory frequency = 25.3 breaths per minnte

Mean O_2 inspired = -.372 liters STPD

Mean O_2 expired = .276 liters STPD

Mean CO_2 inspired = -.002 liters STPD

Mean CO_2 expired = .077 liters STPD

Mean O_2 consumed per breath = -.096 liters STPD

Mean CO_2 prodnced per breath = .075 liters STPD

Total time of inspiration = 38.7 sec

Total time of expiration = 48.9 sec

Total time of respiration = 87.6 sec

Number of good inspirations = 37.0

Number of good expirations = 37.0

Number of good breaths = 37.0

Figure 2.2.2 Example of average data obtained from 125 watts of steady-state exercise.

Shown in Figure 2.2.2 is an example of the average ontpt. The experimental protocol covers an eleven minute (660 seconds) period. Collection of

the respiratory data begins at the 60 second mark. Eight minutes (480 seconds) of respiratory data is collected from the subject. The subject begins exercise at the 100 second mark (40 seconds after data collection begins) and exercises for 320 seconds (to the 420 second mark). Shown in Figure 2.2.2 are the average results from 90 seconds of steady-state, 125 watt exercise (from the 285 second mark to 375 second mark). Also included in the average output, but not shown in Figure 2.2.2 are the calibration data and ambient conditions.

Display of the breath-by-breath values is possible after the tabular and average results have been printed. The individual breath-by-breath values may be displayed or averages of small groups of the breath-by-breath values may be displayed. The groups may be averaged in one of two ways:

- (1) the average of successive breath-by-breath values - the various breath-by-breath values are averaged over a specified number of breaths.
- (2) window averaging - to understand this technique refer to Figure 2.2.3. Shown in the top display are the individual breath-by-breath values and shown in the bottom display are the windowed combinations. A window of width τ is centered about the time t_i . The average of all breaths occurring in the window corresponds to the window averaged value at the time t_i . The center of the window is then slid in time to t_{i+1} to obtain the windowed average for the time t_{i+1} . The center of the window is then then slid to t_{i+2} and averaged, etc.

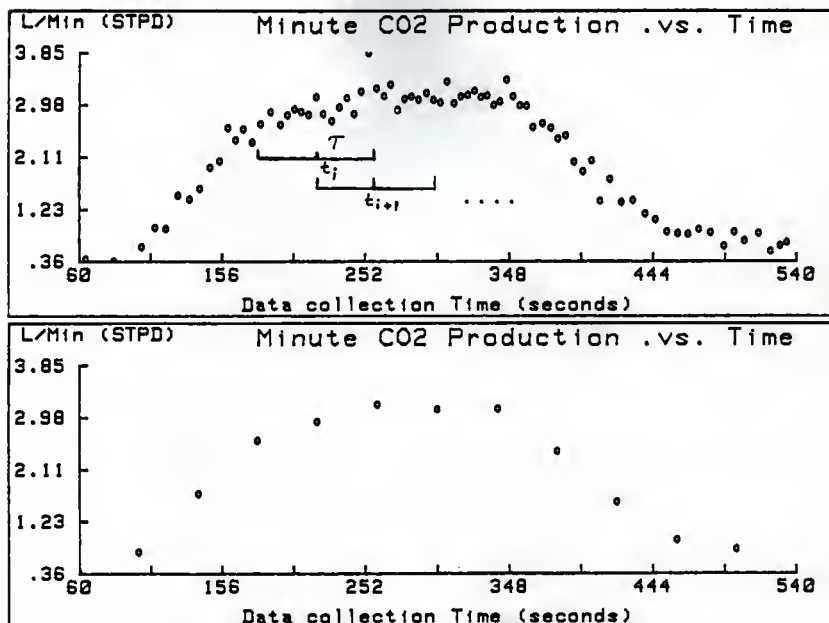


Figure 2.2.3 An illustration of the window breath averaging technique.

The average minute values are obtained by averaging the individual breath-by-breath minute values, causing some error. Considering three breaths, the true minute ventilation is obtained by dividing the total volume involved in the three breaths by the total time of the three breaths. That is

$$\text{Average} = \frac{V_1 + V_2 + V_3}{T_1 + T_2 + T_3}$$

On the other hand, averaging the three breath-by-breath values is done by

$$\text{Average} = (1/3) [V_1/T_1 + V_2/T_2 + V_3/T_3]$$

The error however is small if the duration of the various respiratory cycles are nearly equal so that

$$T = T_1 = T_2 = T_3$$

$$\text{Average} = (1/3T) [V_1 + V_2 + V_3]$$

This same type of error is possible with the respiratory quotient average and respiratory frequency average.

The averaging techniques may be used to display the respiratory data either graphically or in a tabular format. This graphical feature allows quick recognition of transient responses while the tabular output allows the more detailed analysis. The graphical output is similar to Figure 2.2.3 which shows \dot{V}_{CO_2} for a 175 Watt exercise regimen (the 175 Watt exercise regimen was terminated at the 360 second mark rather than the 420 second mark).

Shown in Figure 2.2.4 is an example of the tabular output. This output uses the window averaging technique with a 90 second wide window. The window is slid along with a periodicity of 30 seconds. The window centered about 330 seconds averages the same breaths that is included in the analyzed window of Figure 2.2.1. Note that the average minute values for the 330 second window are nearly equal to the average values obtained in Figure 2.2.1.

This points out one of the advantages of this display method. Steady-state average values may be obtained quickly and easily by analyzing the entire run and selecting windows of a wide width. Previously each individual window would have to be analyzed and the average values obtained. This requires a great deal more of the operator's time.

Although not fully explored with the present system, the windowing feature is a powerful tool. By defining a standard window width and a standard window period, a set of points [average value, time] from one set of data has the same set of time values as another set of data. So that, for a given exercise regimen comparison of a subject's day-to-day variations or comparison of different subjects' responses can be made. Also, with a large population of normal subjects, an average response and corresponding standard deviation to a particular regimen may be defined (refer to system improvements). One problem of using the windowing averaging to accomplish this is the variation of respiratory frequency between exercise levels and between subjects. This variation alters the number of breaths averaged per window and therefore, alters the statistical significance of each subject's averaged value for the standard window.

Date: NOV/02/1984

Comment: 125 Mett Exercise

Subject Identifier: Subject A

The window period is 30.0 seconds

The window width is 90.0 seconds

The starting time is 60 seconds

The ending time is 540 seconds

The breaths are combined by WINDOWING. The breaths occurring in a window 90 seconds(e) wide are averaged. The center of the window is moved 30 seconds between successive averages. The center of the first window is 60 seconds and the ending time is 540 seconds.

* BAD BREATHS OMITTED *

The bad breaths are not included in the averaging technique. Bad breaths are those breaths with an inspiratory volume or an expiratory volume of less than 0.4 Liters.

The R' value is equal to the averaged CO2 produced value divided by the averaged O2 consumed value. It is a better estimate of the true R value for the breaths averaged than the average of the individual R values.

Time (sec)	O2 Consumed (L/min) (STPD)	CO2 Produced (L/min) (STPD)	Alveolar O2 Consumed (L/min) (STPD)	Alveolar CO2 Produced (L/min) (STPD)	Rasp. Quotient	Averaged ICO2/O2 R' (L/min) (STPD)	Ventilation (L/min) (BTPS)	Insp. (L) (BTPS)	Expr. (L) (BTPS)	Tidal Volume (L) (BTPS)	Resp. Freq. (br/min)	Lung Vol. (L) (BTPS)
60.0	.296	.301	.296	.301	.807	1.025	11.31	11.49	.91	.93	16.41	.400
90.0	.549	.523	.549	.523	.879	.805	19.25	13.12	1.07	1.06	18.73	.400
120.0	1.077	.784	1.077	.784	.812	.728	26.12	25.42	1.24	1.21	20.84	.400
150.0	1.625	1.168	1.625	1.168	.800	.719	35.93	14.42	1.62	1.56	22.33	.400
180.0	2.001	1.492	2.001	1.492	.757	.746	44.77	42.51	1.91	1.81	21.74	.400
210.0	2.189	1.672	2.189	1.672	.771	.764	49.51	46.61	2.06	1.94	24.39	.400
240.0	2.104	1.789	2.104	1.789	.786	.776	53.26	49.91	2.11	1.98	25.53	.400
270.0	2.340	1.810	2.340	1.810	.784	.771	51.40	49.89	2.14	2.00	25.18	.400
300.0	2.189	1.871	2.189	1.871	.811	.784	55.54	52.03	2.18	2.04	25.64	.400
330.0	2.416	1.894	2.416	1.894	.805	.777	56.51	52.81	2.22	2.08	25.64	.400
360.0	2.488	1.891	2.488	1.891	.796	.761	57.62	51.66	2.17	2.02	26.78	.400
390.0	2.466	1.813	2.466	1.811	.769	.741	56.27	52.18	2.15	2.00	26.36	.400
420.0	2.207	1.714	2.207	1.714	.830	.777	51.30	49.77	2.12	1.99	25.42	.400
450.0	1.640	1.424	1.640	1.424	1.001	.868	48.61	41.26	2.01	1.91	22.90	.400
480.0	1.011	1.067	1.011	1.067	1.216	1.035	36.98	13.31	1.70	1.65	22.08	.400
510.0	.700	.797	.700	.797	1.216	1.138	10.23	23.31	1.45	1.41	21.24	.400
540.0	.596	.643	.596	.643	1.248	1.080	28.96	26.19	1.24	1.21	21.77	.400

Figure 2.2.4 Example of the tabular output obtained by window averaging the breath-by-breath data.

Chapter III. DESIGN OF A RAPIDLY RESPONDING TEMPERATURE TRANSDUCER

Dependency of respiratory breath-by-breath volumes derived from a PTG signal on respiratory flow temperature has been recognized by several researchers [4,13,17,18,19]. Creel [4] pointed out the need for monitoring respiratory temperature so that volumes computed under various conditions could be converted to standard conditions, either STPD conditions or BTPS conditions. In addition, the gas viscosity, used in calculating the flow from the PTG differential pressure, is dependent on the respiratory gas temperature.

In order to facilitate compensation of temperature variations throughout the respiratory cycle, a temperature transducer for monitoring respiratory flow temperature near the flow sensing sight will be designed and integrated into the CBRMS. The temperature transducer must

1. have a probe which can be conveniently placed in the respiratory flow stream and has a minimal effect on the respiratory flow,
2. have a rapid thermal time constant so that the respiratory flow temperature may be faithfully monitored,
3. have an output voltage compatible with the input range of the DAM,
4. be able to measure and have maximum sensitivity to temperatures in the respiratory range (20°C to 40°C),
5. have a simple calibration procedure, and
6. be stable to avoid frequent re-calibration.

Both thermocouples and thermistors are available in a size small enough so that when inserted into the respiratory flow stream each would have little effect on the flow. Thermocouples, however, are available with a response time (time required for the sensor to reach 63.2% of a step change in temperature) as low as 3 ms while the fastest thermistors, due to their larger mass, have thermal time constants in the 500 ms range. For the faster response time the thermocouple is selected as the sensing element of the temperature transducer.

A type E (chromel-constantan), bead welded, thermocouple having a diameter of 0.001 inch is selected. The response time of this thermocouple is 4.5 ms. In addition, among the commonly available thermocouples the voltage-temperature relationship of the type E thermocouple is the most linear and has the highest degree of sensitivity (change in thermocouple

voltage per change in temperature) over the respiratory temperature range.

A respiratory temperature transducer was designed such that goals three thru six are realized. For a tutorial on thermocouple principles refer to Appendix IV.

3.1 Transducer Design

A block diagram of the temperature transducer is shown in Figure 3.1.1 and the actual electronics are shown in Figure 3.1.2. The type E thermocouple is connected to lead wires with the connection being made in an isothermal body. The isothermal body is made of molded fiberglass which also contains the reference junction temperature sensor. The lead wires are connected to a pre-amplifier which amplifies the thermocouple differential voltage.

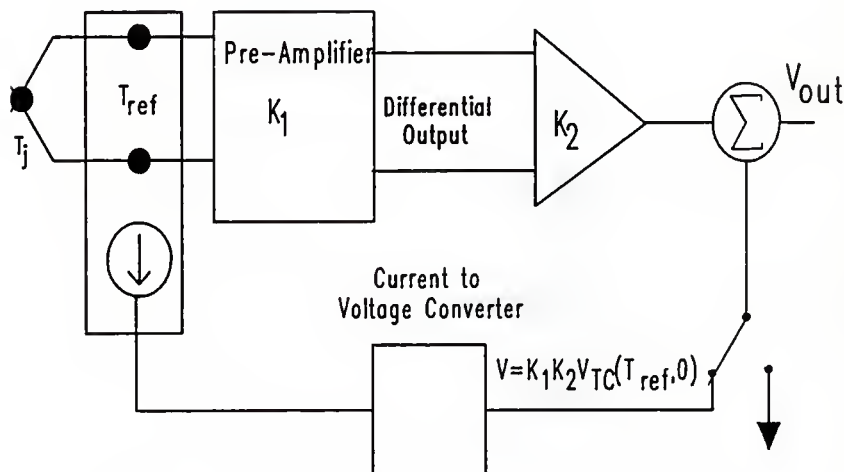
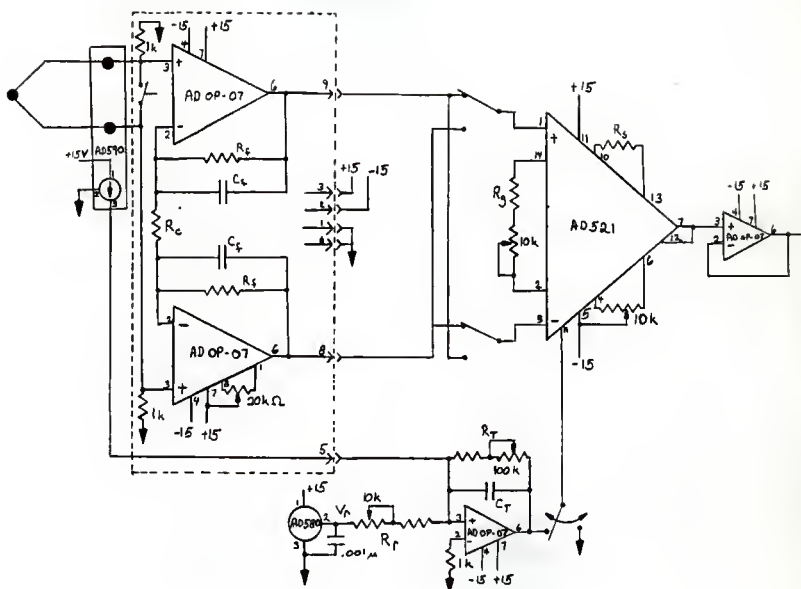


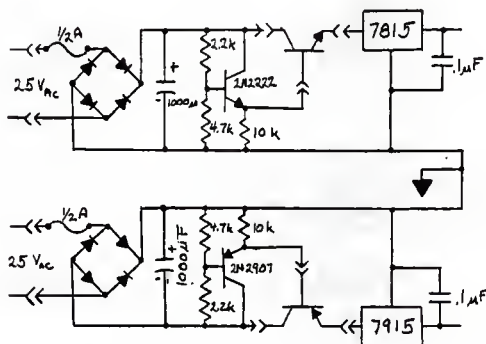
Figure 3.1.1 The block diagram of the temperature transducer.

The differential output of the pre-amplifier is connected to a differential amplifier, resulting in a ground referenced output voltage of

$$V = K_1 K_2 V_{TC}(T_j, T_{ref})$$



(a)



(b)

Figure 3.1.2 (a) The temperature transducer. (b) The power supply

Hardware compensation is used to account for the non-ice point reference junction temperature. The compensator output is given by

$$V_{\text{comp}}(T_{\text{ref}}) = K_1 K_2 V(T_{\text{ref}}, 0)$$

The outputs of the differential amplifier and the compensator are summed so that the transducer output voltage is

$$V_o(T_j, T_{ref}) = K_1 K_2 [V_{TC}(T_j, T_{ref}) + V(T_{ref}, 0)] \quad 3.1.1$$

which reduces to

$$V_o(T_j, T_{ref}) = K_1 K_2 V_{TC}(T_j, 0) \quad 3.1.2$$

The transducer output voltage is sampled by the computer system. The computer system can determine the temperature T_j using the appropriate calibration factors.

The transducer consists of three physical sections, the thermocouple probe, the pre-amplifier, and a TM plug-in module. The TM plug-in module is a blank bread board for constructing custom circuitry to be used with the Tektronix TMS00 Power Module Series. The AD521, reference junction compensator (excluding the sensing element), the power supply, and BNC connectors are placed in the module. The TM plug-in module is used in order to remain compatible with many of the other instruments in the Bioengineering Research Laboratory.

The pre-amplifier, a configuration identical to the input stage of a three-operational amplifier instrumentation amplifier, is constructed with two Analog Devices AD OP-07 operational amplifiers. The AD OP-07 is chosen for its minimal offset voltage, minimal bias current temperature drifts, and its low noise. The pre-amplifier's configuration provides high input impedance, high CMRR (Common Mode Rejection Ratio), and, due to its symmetry, reduces the errors caused by the input bias currents and temperature drifts of the bias currents and offset voltages. The resistors connected to the input terminals of the pre-amplifier provide a path to ground for the input bias currents of the two operational amplifiers.

The voltage across the resistor R_c , assuming an ideal operational amplifier and neglecting the thermocouple and lead resistances, is equal to the thermocouple voltage, V_{TC} . This voltage causes a current to flow through R_c which is equal to $V_{TC}(T_j, T_{ref})/R_c$. This current also passes through the feedback impedances. Writing a KVL equation, the differential output of the pre-amplifier is

$$V_{o_{pre-amp}} = (V_{TC}(T_j, T_{ref})/R_c)R_f + (V_{TC}(T_j, T_{ref})/R_c)R_c + (V_{TC}(T_j, T_{ref})/R_c)R_f$$

which simplifies to

$$V_{O_{\text{pre-amp}}} = (1 + 2R_f/R_c)V_{TC}(T_j, T_{\text{ref}}) = K_1 V_{TC}(T_j, T_{\text{ref}})$$

where K_1 is the pre-amplifier gain and is given by

$$K_1 = 1 + 2R_f/R_c$$

The output of the pre-amplifier is used as the input to an Analog Device's AD521 precision instrumentation amplifier. The AD521 is a true differential amplifier whose gain, in this configuration, is set by two resistors, R_s and R_g . The AD521 also has an external voltage reference which is used to perform the voltage summing operation illustrated in the block diagram. The output of the AD521 is given by

$$V_O = V_i(R_s/R_g) + V_{\text{ref}}$$

The output of the pre-amplifier is used as the input to the AD521 and the compensator output is connected to the voltage reference terminal. In this application the output of the AD521 is a function of T_j and T_{ref} ,

$$V_O(T_j, T_{\text{ref}}) = K_1 K_2 V_{TC}(T_j, T_{\text{ref}}) + V_{\text{comp}}(T_{\text{ref}})$$

where

$$K_1 = 1 + 2R_f/R_c$$

$$K_2 = R_s/R_g$$

The reference junction compensator is based on an AD590 two-terminal integrated circuit temperature transducer, which produces an output current proportional to absolute temperature. A current device is selected to eliminate the compensator sensitivity to voltage drops over a long lead wire. The reference junction is embedded in fiberglass to provide an isothermal block. The AD590 is embedded in the fiberglass in order to sense the temperature of this isothermal block. The current output of the AD590 transducer as a function of temperature is

$$I(T) = (T + 273.2) \mu\text{A}/^\circ\text{K} \quad -55^\circ\text{C} < T < 150^\circ\text{C}$$

where

$$T = \text{sensor temperature } (^\circ\text{C})$$

This sensor is connected to the compensator op-amp. This op-amp is an AD OP-07 amplifier connected to be a summing amplifier. The output of the summing amplifier is a linear function of the reference junction temperature. The compensator output is given by

$$V_{\text{comp}}(T_{\text{ref}}) = [I(T_{\text{ref}}) - V_r/R_r]R_T$$

Since the thermocouple has a nonlinear voltage-temperature relationship some error is created with a linear compensation schema. However, if the reference junction temperature varies only over a small range a linear compensation schema performs satisfactorily, since over small temperature variations the type E thermocouple is very linear.

In summary, the output of the temperature transducer with a sensing temperature of T_j and reference junction temperature of T_{ref} is

$$V_o(T_j, T_{\text{ref}}) = K_1 K_2 V_{TC}(T_j, T_{\text{ref}}) + V_{\text{comp}}(T_{\text{ref}}) \quad 3.1.3$$

where the gain constants K_1 (pre-amp) and K_2 (AD521) are

$$K_1 = 1 + 2R_f/R_c$$

$$K_2 = R_s/R_g$$

The output voltage of the compensation circuit is

$$V_{\text{comp}}(T_{\text{ref}}) = [I(T_{\text{ref}}) - V_r/R_r]R_T \quad 3.1.4$$

where

$$I(T_{\text{ref}}) = (T_{\text{ref}} + 273.2) \mu\text{A}/^\circ\text{K}$$

A scheme for the determination of component values will now be presented.

The transducer is used to measure the temperature range T_{min} to T_{max} , with the reference junction temperature fluctuating about the average ambient temperature. The transducer provides an output voltage in the range V_{min} to V_{max} , corresponding to T_{min} and T_{max} respectively. The voltage range V_{min} to V_{max} must be compatible with the input of the Data Acquisition Module (DAM). With the temperature range, corresponding voltage range, and with the reference junction temperature equal to the average ambient temperature (T_{amb}), Equation 3.1.3 yields these two equations:

$$V_{\text{min}} = V_o(T_{\text{min}}, T_{\text{amb}}) = K_1 K_2 V_{TC}(T_{\text{min}}, T_{\text{amb}}) + V_{\text{comp}}(T_{\text{amb}})$$

$$V_{\text{max}} = V_o(T_{\text{max}}, T_{\text{amb}}) = K_1 K_2 V_{TC}(T_{\text{max}}, T_{\text{amb}}) + V_{\text{comp}}(T_{\text{amb}}).$$

These two equations allow for the determination of the two unknown values, the total gain ($K_1 K_2$) and ambient compensation voltage. The total gain is found by taking the difference of these two equations and solving for the product $K_1 K_2$

$$K_1 K_2 = \frac{V_o(T_{\text{max}}, T_{\text{amb}}) - V_o(T_{\text{min}}, T_{\text{amb}})}{V_{TC}(T_{\text{max}}, T_{\text{amb}}) - V_{TC}(T_{\text{min}}, T_{\text{amb}})} \quad 3.1.5$$

By substituting this gain value into one of the two equations the necessary compensation voltage with the reference junction at ambient temperature is found.

$$V_{\text{comp}}(T_{\text{amb}}) = V_{\text{min}} - K_1 K_2 V_{\text{TC}}(T_{\text{min}}, T_{\text{amb}}) \quad 3.1.6$$

The gain is developed with the resistors R_f , R_c , R_s , and R_g such that

$$K_1 K_2 = (1 + 2R_f/R_c)(R_s/R_g)$$

Most of the gain should come from the pre-amplifier stage in order to maximize the signal-to-noise ratio at the output [7]. Realizable values of R_f and R_c are selected to obtain the desired K_1 gain. The value of R_s is limited to be $100\text{k}\Omega \pm 15\%$ by the AD521's specifications. The value of R_g necessary to yield the gain $K_1 K_2$ is calculated and accomplished by a fixed resistor in series with a $10\text{k}\Omega$ potentiometer.

The components of the compensation amplifier (V_x , R_x , and R_T) are found by considering Equation 3.1.6 and the goal of the compensation amplifier to have the same voltage-temperature relationship as the amplified thermocouple voltage. If a similar relationship is obtained the transducer output will not change with small variations of the reference junction temperature from the average ambient temperature (provided the sensing junction temperature is constant). This goal expressed mathematically is

$$\begin{aligned} dV_o(T_j, T_{\text{ref}})/dT_{\text{ref}} = 0 &= K_1 K_2 [dV_{\text{TC}}(T_j, T_{\text{ref}})/dT_{\text{ref}}] + dV_{\text{comp}}(T_{\text{ref}})/dT_{\text{ref}} \\ T_j &= \text{constant} \end{aligned}$$

so that

$$\begin{aligned} dV_{\text{comp}}(T_{\text{ref}})/dT_{\text{ref}} &= -K_1 K_2 [dV_{\text{TC}}(T_j, T_{\text{ref}})/dT_{\text{ref}}] \\ &= -K_1 K_2 [dV_{\text{TC}}(T_j, 0)/dT_{\text{ref}} - dV_{\text{TC}}(T_{\text{ref}}, 0)/dT_{\text{ref}}] \\ &= K_1 K_2 dV_{\text{TC}}(T_{\text{ref}}, 0)/dT_{\text{ref}} \end{aligned}$$

Taking the derivative of V_{comp} in Equation 3.1.4 with respect to reference junction temperature and equating the result to the above derivative of the compensation voltage yields

$$dV_{\text{comp}}(T_{\text{ref}})/dT_{\text{ref}} = (10^{-6})R_T = K_1 K_2 dV_{\text{TC}}(T_{\text{ref}}, 0)/dT_{\text{ref}}$$

so that the value, in $\text{M}\Omega$, of the resistor R_T is

$$R_T = K_1 K_2 [dV_{TC}(T_{ref}, 0)/dT_{ref}] \quad M\Omega \quad 3.1.7$$

$T_{ref} = T_{amb}$, the average ambient temperature

The derivative of the thermocouple voltage is found from the second order fit developed in Appendix IV (Equation A4.1).

$$\begin{aligned} dV_{TC}(T, 0)/dT &= 2V_a T + V_b \\ V_a &= 45.85(10)^{-6} \text{ (mV/} (^{\circ}\text{C})^2\text{)} \\ V_b &= 58.65(10)^{-3} \text{ (mV/} (^{\circ}\text{C})\text{)} \end{aligned}$$

Once the value of R_T is determined, the ratio V_r/R_r is found from the ambient compensation voltage, Equation 3.1.6, such that

$$V_r/R_r = (T_{amb} + 273.2)(10^{-6}) - V_{comp}(T_{amb})/R_T \quad 3.1.8$$

A commercially available precision reference voltage is selected, having the same sign as the result of Equation 3.1.8. Using this value for V_r the resistance R_r is calculated.

The bypass capacitors (C_f, C_T) are selected to give the appropriate high cutoff frequencies. The temperature signals do not contain significant components beyond 60 Hz. Since the reference junction temperature varies very slowly a cutoff frequency of 2 Hz is selected for the compensator. The capacitors are then

$$C_f = \frac{1}{2\pi(60)R_f} \quad C_T = \frac{1}{2\pi(2)R_T}$$

A program, TXDCR_VALS Appendix XI, Section A6.9, has been written to help determine the transducer component values for a given temperature measurement range, output voltage range, and the average ambient temperature. The program calculates the necessary component values. The program prints the ideal transducer output voltages for the range $T_{min} - 5^{\circ}\text{C}$ to $T_{max} + 5^{\circ}\text{C}$ in 0.1°C increments. The compensator output voltages for the range $T_{ambient} - 5^{\circ}\text{C}$ to $T_{ambient} + 15^{\circ}\text{C}$ in 0.1° increments are also printed.

The temperature transducer used in the present CBRMS monitors the respiratory temperature range, 20°C to 40°C . The output voltage range is -3.5V to 3.5V , -3.5V corresponding to 20°C and an output of 3.5V corresponding to 40°C . The average ambient temperature in the Bioengineering Research Laboratory is 70°F , 21.1°C . The component values and output voltages are determined with TXDCR_VALS. The output of TXDCR_VALS is shown in Figure 3.1.3.

A 187Ω resistor is selected for R_c and a $348\text{k}\Omega$ resistor selected for

R_f . This combination provides high gain in the pre-amplifier stage. The total gain necessary for the transducer and the pre-amplifier gain are

$$\text{Total Gain } (K_1 K_2) = 5700.2 \quad K_1 = 3722.9$$

so that $K_2 = 1.5311$. Use of a $95\text{k}\Omega$ resistor for R_s and the mentioned R_c and R_f resistor values require a $62.05\text{k}\Omega$ resistor for R_g . The value of R_g consists of a $58\text{k}\Omega$ fixed resistor in series with a $10\text{k}\Omega$ potentiometer.

The required value for R_T is $345.3\text{k}\Omega$. Using an Analog Device's AD580 2.50V voltage reference voltage for V_r requires the value of R_r to be $8.24\text{k}\Omega$. R_T consists of a $317\text{k}\Omega$ fixed resistor in series with a $100\text{k}\Omega$ potentiometer and R_r consists of a $7.68\text{k}\Omega$ resistor in series with a $10\text{k}\Omega$ potentiometer.

The reference junction temperature corresponding to $V_{\text{comp}}(T_{\text{ref}}) = 0$, T_0 , is 30.14°C . With the reference junction temperature equal to T_0 the compensator output is independent of the R_T resistor. This point is important in the calibration of the compensator circuitry since R_r can be adjusted to yield $V_{\text{comp}} = 0$ independent of R_T .

Figure 3.1.3 The output of the TXDCR_VALS program. The program yields the necessary component values of the temperature transducer and the ideal output voltages of the transducer and compensator verse temperature.

TEMPERATURE RANGE: 20.00 TO 40.00

$$V_o(20,0) = -3.5$$

$$V_o(40,0) = 3.5$$

$$T_{\text{ambient}} = 21.1$$

$$\text{TOTAL GAIN} = 5700.23$$

$$K1 = 3722.92513369$$

$$K2 = 1.53111671348$$

$$R_c = 1.870E+02 \quad R_f = 3.480E+05$$

$$R_s = 9.500E+04 \quad R_g = 6.205E+04$$

$$\text{VOLTAGE REFERENCE} = 2.5000$$

$$R_r = 8.242E+03 \quad R_t = 3.453E+05$$

$$T_{\text{ref}}(V_{\text{comp}}=0) = 30.14$$

**** The output voltage of the reference junction compensator. ****

	.0	.1	.2	.3	.4	.5	.6	.7	.8	.9
16	-4.882	-4.847	-4.813	-4.778	-4.744	-4.709	-4.674	-4.640	-4.605	-4.571
17	-4.536	-4.502	-4.467	-4.433	-4.398	-4.364	-4.329	-4.295	-4.260	-4.226
18	-4.191	-4.156	-4.122	-4.087	-4.053	-4.018	-3.984	-3.949	-3.915	-3.880
19	-3.846	-3.811	-3.777	-3.742	-3.708	-3.673	-3.638	-3.604	-3.569	-3.535
20	-3.500	-3.466	-3.431	-3.397	-3.362	-3.328	-3.293	-3.259	-3.224	-3.190
21	-3.155	-3.120	-3.086	-3.051	-3.017	-2.982	-2.948	-2.913	-2.879	-2.844
22	-2.810	-2.775	-2.741	-2.706	-2.671	-2.637	-2.602	-2.568	-2.533	-2.499
23	-2.464	-2.430	-2.395	-2.361	-2.326	-2.292	-2.257	-2.223	-2.188	-2.153
.										
35	1.680	1.714	1.749	1.784	1.818	1.853	1.887	1.922	1.956	1.991
36	2.025	2.060	2.094	2.129	2.163	2.198	2.232	2.267	2.302	2.336

**** The respiratory temperature transducer output voltage. ****

	.0	.1	.2	.3	.4	.5	.6	.7	.8	.9
15	-5.217	-5.183	-5.149	-5.115	-5.080	-5.046	-5.012	-4.978	-4.943	-4.909
16	-4.875	-4.841	-4.806	-4.772	-4.738	-4.704	-4.669	-4.635	-4.601	-4.566
17	-4.532	-4.498	-4.463	-4.429	-4.395	-4.360	-4.326	-4.292	-4.257	-4.223
18	-4.189	-4.154	-4.120	-4.085	-4.051	-4.017	-3.982	-3.948	-3.913	-3.879
19	-3.845	-3.810	-3.776	-3.741	-3.707	-3.672	-3.638	-3.603	-3.569	-3.534
20	-3.500	-3.466	-3.431	-3.397	-3.362	-3.328	-3.293	-3.259	-3.224	-3.189
21	-3.155	-3.120	-3.086	-3.051	-3.017	-2.982	-2.948	-2.913	-2.879	-2.844
22	-2.809	-2.775	-2.740	-2.706	-2.671	-2.636	-2.602	-2.567	-2.533	-2.498
.										
29	-.376	-.341	-.306	-.271	-.236	-.201	-.166	-.131	-.096	-.061
30	-.026	.009	.044	.079	.114	.149	.184	.219	.254	.289
31	.324	.359	.394	.429	.464	.499	.535	.570	.605	.640
.										
42	4.211	4.247	4.283	4.318	4.354	4.390	4.425	4.461	4.497	4.532
43	4.568	4.604	4.639	4.675	4.711	4.746	4.782	4.818	4.854	4.889
44	4.925	4.961	4.997	5.032	5.068	5.104	5.140	5.175	5.211	5.247
45	5.283	5.318	5.354	5.390	5.426	5.462	5.497	5.533	5.569	5.605

3.2 Calibration of the Temperature Transducer

Calibration of the temperature transducer involves two steps. First, the calibration of the reference junction compensation circuitry and secondly, the calibration of the thermocouple amplifier. The compensation circuitry must be calibrated first so that the correct voltage is being added to the amplified thermocouple voltage to obtain the transducer output.

The compensation circuit produces a voltage that is a linear function of the reference junction temperature, given by Equation 3.1.4 (repeated here)

$$V_{\text{comp}}(T_{\text{ref}}) = [I(T_{\text{ref}}) - V_r/R_r]R_T. \quad 3.1.4$$

By the adjustment of feedback potentiometer (the potentiometer in the feedback path) and the reference potentiometer (the potentiometer in series with R_r) the correct linear relationship can be generated. By creating a reference junction temperature corresponding to the $V_{\text{comp}}(T_{\text{ref}})=0$, the reference potentiometer can be adjusted independent of the feedback resistance, since

$$0 = [I(T_0) - V_r/R_r]R_T$$

T_0 - temperature corresponding to $V_{\text{comp}}(T_{\text{ref}}) = 0$

so that R_T may be divided out. This adjustment also cancels the constant operational amplifier errors, offset voltage and bias current errors, the base-line error of AD590 temperature sensor, and the deviation of the voltage reference from its specified value.

The slope of the output voltage-reference junction temperature relationship is controlled by the feedback resistor. After the zero voltage adjustment is made the reference junction temperature is changed to near ambient temperature. This temperature is measured and the corresponding ideal output voltage found. The feedback potentiometer is adjusted to obtain this correct output.

After the compensator has been calibrated, the thermocouple amplifier is calibrated. By applying a known sensing junction temperature to the thermocouple, the AD521 gain potentiometer which is the potentiometer in series with R_s , is adjusted to obtain the correct output voltage. The reference junction should be maintained near the average room temperature during this adjustment.

Next is a step-by-step procedure for calibration of the temperature transducer. The necessary equipment for calibration of the thermocouple are listed here:

1. The three water baths used in the system calibration procedure, Figure 5.1.1. One water bath should be equal to ambient temperature, one having a temperature slightly higher than T_0 , and the other equal to T_{\max} .
2. The Tektronix Module extension cable. The temperature transducer should be connected to this extension cable so that the calibration potentiometers are available for adjustment.
3. A calibrated thermometer.
4. A voltmeter.
5. A small screwdriver or potentiometer screwdriver.

Junction temperature compensation amplifier.

1. Connect the voltmeter to the BNC connector labeled $V_{T_{\text{ref}}}$ located on the front panel of the temperature transducer.
2. Adjustment of the output voltage to zero for a reference junction temperature of T_0 .
 - a) Submerge the entire thermocouple assembly into the water bath having the temperature slightly higher than T_0 . Allow enough time for the thermocouple assembly to be in temperature equilibrium with the water bath. Check to make certain the bath temperature is slightly above T_0 . If the bath temperature is not above T_0 , the bath temperature must be raised.
 - b) Allow the bath temperature to drift down to T_0 while stirring the bath occasionally in order to maintain a uniform bath temperature.
 - c) Adjust the reference resistor, R_x , so that the output of the reference junction compensator is zero volts.
3. Adjustment of the temperature sensitivity of the reference junction compensator.
 - a) Submerge the entire thermocouple assembly into the water bath having a temperature equal to room temperature. Allow enough time

for the assembly to reach temperature equilibrium with the water bath.

- b) Adjust R_T to obtain the correct output voltage of the reference junction compensator for the bath temperature.
- c) Remove the thermocouple assembly from the water bath.

Thermocouple amplifier adjustments.

1. Offset null adjustment of the thermocouple pre-amplifier.
 - a) Connect the voltmeter to the differential output of the pre-amplifier circuit using the banana plug jacks located on the pre-amplifier unit.
 - b) Depress the input shorting button of the pre-amplifier and adjust the offset null potentiometer of the pre-amplifier to obtain a differential output of zero volts.
2. Offset null adjustment of the differential amplifier.
 - a) Connect a voltmeter to the BNC connector labeled V_{out} located on the temperature transducer.
 - b) Ground the AD521's reference voltage terminal, which removes the compensation voltage, by flipping the switch on the front panel of the transducer.
 - c) Depress the input shorting button on the thermocouple pre-amplifier.
 - d) Adjust the offset null of the AD521 to obtain a transducer output of zero volts.
3. Gain adjustment of the thermocouple amplifier.
 - a) Leave the voltmeter connected to the output of the temperature transducer.
 - b) Apply the compensation voltage to the reference terminal of the AD521.
 - c) Insert the sensing junction of the thermocouple into a well mixed water bath having a temperature in the upper end of the measurement range.

- d) Adjust R_g to obtain the correct output voltage for the temperature of the water bath.

3.3 Temperature Transducer Testing

The temperature transducer is essentially two temperature transducers in one. The first uses the thermocouple to sense the difference between the sensing junction temperature and the reference junction temperature. The second, the compensator, senses the reference junction temperature. The operation of the total transducer is dependent upon the correct operation of both of these separate transducers. In order for the output to be related to the sensing junction temperature the compensator must provide the correct voltage to be added. For these reasons the testing of the transducer is divided into two sections, the testing of the compensation circuitry and the testing of the overall transducer.

The temperature-output voltage relationship of the compensation circuitry was first tested. To do so the thermocouple probe assembly was submerged in a water bath and allowed to reach temperature equilibrium with the water bath. The bath temperature and the output voltage of the compensator were measured and recorded. A thermometer accurate to within 0.1°C was used to measure the water bath temperature. The transducer was calibrated according to the procedure outlined in Section 3.2 on day 1 (February 12, 1985). The output of the compensator was measured on day 2, day 3, and day 14.

The results of the three trials are shown in Table 3.3.1. The temperature corresponding to the measured output voltage is compared with the measured water bath temperature.

From the error values it is apparent that the reference junction compensator voltage-reference junction temperature relationship is valid. The average errors and standard deviations are much less than 1.0% in all three cases. Also the maximum error for any measurement is 0.83%. These results not only show the compensator is accurate but also stable due to the time span between calibration and data collection of trial 3.

Table 3.3.1 The calculated water bath temperature, measured bath temperature, and the associated error versus output voltage of the compensator for three trials.

(a) Trial 1, Day 2

Measured Voltage (V)	Calculated bath temp. ($^{\circ}\text{C}$)	Measured input temp. ($^{\circ}\text{C}$)	Error of measured temp. from ideal
-3.500	19.99	20.0	0.06%
-3.363	20.39	20.4	0.07%
-2.762	22.13	22.2	0.34%
-2.467	22.98	23.0	0.09%
-2.229	23.67	23.7	0.13%
-2.143	23.92	24.0	0.34%
-1.839	24.80	25.0	0.81%

Average error: 0.26%
Standard deviation 0.27%

(b) Trial 2, Day 3

Measured Voltage (V)	Calculated bath temp. ($^{\circ}\text{C}$)	Measured input temp. ($^{\circ}\text{C}$)	Error of measured temp. from ideal
-3.589	19.73	19.7	-0.15%
-3.136	21.04	21.1	0.27%
-2.816	21.97	22.1	0.60%
-2.619	22.54	22.6	0.27%
-2.426	23.10	23.1	0.01%
-2.203	23.74	23.8	0.23%
-1.880	24.68	24.8	0.49%

Average error: 0.24%
Standard deviation 0.26%

(c) Trial 3, Day 14

Measured Voltage (V)	Calculated bath temp. ($^{\circ}\text{C}$)	Measured input temp. ($^{\circ}\text{C}$)	Error of measured temp. from ideal
-3.602	19.69	19.7	0.04%
-3.310	20.54	20.6	0.30%
-3.077	21.21	21.3	0.41%
-2.798	22.02	22.1	0.36%
-2.563	22.70	22.7	-0.01%
-2.320	23.41	23.6	0.83%
-1.853	24.76	24.9	0.57%

Average error: 0.36%
Standard deviation 0.29%

With the compensator working satisfactorily the total transducer output may be tested. The temperature probe (the thermocouple sensing junction) was placed in a water bath. The bath temperature and the transducer output voltage were measured and recorded. Three trials were performed. The calibration of the transducer used for testing the reference junction compensator was also used for these trials. The trials were taken on day 20, day 21, and day 22 (day 1 being the date the transducer was calibrated, February 12, 1985).

The results are shown in Table 3.3.2. The temperatures corresponding

to the measured voltages are calculated and compared with the measured bath temperatures. From the error values the transducer is shown to be operating satisfactorily. However, it is hoped to have the transducer error of less than 1.0%. While this is true in the average there are several values with an error of larger than 1.0% and one value larger than 2.0%.

Table 3.3.2 The calculated water bath temperature, measured bath temperature, and the associated error versus output voltage of the temperature transducer for three trials.

(a) Trial 1, Day 20

Measured Voltage (V)	Calculated bath temp. (°C)	Measured input temp. (°C)	Error of measured temp. from ideal
-3.51	19.97	20.1	0.65%
-3.33	20.49	20.7	1.01%
-3.04	21.33	21.3	-0.15%
-2.56	22.72	22.8	0.35%
-2.27	23.56	23.9	1.45%
-1.76	25.03	25.1	0.29%
-1.32	26.29	26.4	0.41%
-1.16	26.75	27.2	1.67%
-0.88	27.56	27.7	0.52%
-0.48	28.70	29.0	1.04%
-0.04	29.96	29.9	-0.20%
0.28	30.87	30.9	0.08%
0.64	31.90	31.8	-0.32%
0.94	32.76	32.8	0.14%
1.27	33.69	33.8	0.32%
1.58	34.57	34.7	0.36%
2.04	35.88	35.9	0.06%
2.44	37.01	36.8	-0.57%
2.61	37.49	37.8	0.82%
2.61	37.49	37.8	0.82%
3.49	39.97	40.1	0.32%

Average Error: 0.43%

Standard Deviation: 0.56%

(b) Trial 2, Day 21

Measured Voltage (V)	Calculated bath temp. (°C)	Measured input temp. (°C)	Error of measured temp from ideal
-3.30	20.58	20.7	0.59%
-3.08	21.22	21.6	1.81%
-2.65	22.46	22.8	1.51%
-2.35	23.33	23.8	2.03%
-1.79	24.94	25.0	0.24%
-1.33	26.26	26.6	1.28%
-0.88	27.56	27.8	0.89%
-0.56	28.47	28.7	0.80%
-0.24	29.39	29.8	1.40%
0.19	30.62	30.6	-0.06%
0.36	31.10	31.2	0.31%
0.64	31.90	32.0	0.31%
0.97	32.84	32.8	-0.12%
1.15	33.35	33.4	0.14%
1.48	34.29	34.3	0.03%
1.86	35.37	35.3	-0.19%
2.15	36.19	36.1	-0.25%
2.67	37.66	37.4	-0.69%
2.82	38.08	38.2	0.30%
3.15	39.01	39.1	0.22%
3.45	39.86	39.9	0.10%

Average Error: 0.51%
Standard Deviation: 0.73%

(c) Trial 3, Day 22

Measured Voltage (V)	Calculated bath temp. (°C)	Measured input temp. (°C)	Error of measured temp from ideal
-3.49	20.03	20.3	1.35%
-3.12	21.10	21.2	0.47%
-2.95	21.59	21.9	1.42%
-2.56	22.72	23.1	1.67%
-2.25	23.62	24.0	1.63%
-1.87	24.71	25.1	1.58%
-1.52	25.72	26.0	1.10%
-1.17	26.72	27.2	1.78%
-0.75	27.93	28.1	0.61%
-0.47	28.73	28.9	0.59%
-0.06	29.90	29.9	-0.01%
0.25	30.79	31.0	0.69%
0.75	32.21	32.2	-0.04%
0.94	32.76	32.9	0.44%
1.27	33.69	34.1	1.21%
1.73	35.00	35.1	0.29%
2.14	36.16	36.2	0.11%
2.49	37.15	37.3	0.40%
2.74	37.86	37.9	0.11%
3.07	38.79	38.9	0.29%
3.54	40.11	39.9	-0.53%

Average Error: 0.69%
Standard Deviation: 0.67%

This goal of 1% error in the determination of the flow temperature may be over ambitious and unnecessary. To illustrate this a preliminary estimate of the sensitivity of the calculation of the STPD flow on the flow temperature is investigated. The calculation of the respiratory flow is developed in Chapter IV and Appendix III. There are two terms in the calculation of the flow that are dependent on temperature, the relative viscosity and the

I \dot{T} P (Instantaneous Temperature and Pressure) to STPD conversion factor as is evident in the equation for flow

$$\dot{V}(\text{STPD}) = (\Delta P / \mu) K(P_b, F_{H_2O}, T) \quad A3.12$$

where μ is the viscosity. The equation for gas viscosity is developed in Chapter IV and is equal to

$$\mu = Fw_{O_2} \mu'_{O_2} + Fw_{CO_2} \mu'_{CO_2} + Fw_{N_2} \mu'_{N_2} + F_{H_2O} \mu'_{H_2O} \quad 4.5$$

Fw_x - the fractional content of gas x in the flow gas including the volume of water vapor in the gas.

μ'_x - the modified viscosity of gas x at the given temperature. The functions of temperature are given in Table 4.3 of Chapter IV.

The term $K(P_b, F_{H_2O}, T)$ is the ITP to STPD conversion factor and defined as

$$K(P_b, F_{H_2O}, T) = [1 - F_{H_2O}] [273.15 / (273.15 + T)] [P_b / 760]$$

T - the gas temperature

P_b - the barometric pressure

F_{H_2O} - the fractional content of water vapor in the gas.

It is not important to have a firm understanding of the calculation of the STPD flow at this time. The development of these equations are presented in Chapter IV and Appendix III.

The sensitivity of the STPD flow on temperature is

$$(d\dot{V}/dT)/\dot{V} = (1/\dot{V}) (d/dT) [(\Delta P/\mu) K(P_b, F_{H_2O}, T)]$$

which is equal to

$$(d\dot{V}/dT)/\dot{V} = [dK(P_b, F_{H_2O}, T)/dT] / K(P_b, F_{H_2O}, T) - (d\mu/dT)/\mu \quad 3.3.1$$

That is the sensitivity of the flow calculation to flow temperature is equal to the temperature sensitivity of the ITP to STPD correction factor minus the temperature sensitivity of the viscosity calculation. The sensitivity of the viscosity to temperature errors is (from Equation 4.5 and Table 4.3)

$$(d\mu/dT)/\mu = (1/\mu) [0.606 Fw_{O_2} + 0.612 Fw_{CO_2} + 0.451 Fw_{N_2} + 0.506 F_{H_2O}]$$

The derivative is taken assuming that the concentration of the water vapor is independent of temperature. This assumption is valid for small variations in temperature. Using concentrations in between the inspiratory and expiratory

values the sensitivity of the gas viscosity to errors in temperature is

$$\begin{aligned} (d\mu/dT)/\mu &= \left[1/(168.23 + 0.482T) \right] \left[\begin{array}{l} (0.606)(0.16) + (0.612)(0.03) \\ + (0.451)(0.78) + (0.506)(0.03) \end{array} \right] \\ (d\mu/dT)/\mu &= 0.482/(168.23 + 0.482T) \end{aligned} \quad 3.3.2$$

The sensitivity of the ITP to STPD correction factor on temperature (again assuming the water vapor concentration is temperature independent) is

$$(dK(P_b, F_{H_2O}, T)/dT)/K(P_b, F_{H_2O}, T) = -1/(273.15 + T) \quad 3.3.3$$

The sensitivity of flow on respiratory temperature is then

$$(d\dot{V}/dT)/\dot{V} = -1/(273.15 + T) - 0.482/(168.23 + 0.482T) \quad 3.3.4$$

The errors in the flow calculation as a function of temperature error are shown in Table 3.3.9 for several values of temperature. It is readily apparent that the sensitivity of flow to small errors in temperature is insignificant. To obtain a flow error of 1.0% due to an error in the temperature at 30°C requires an error of -5.6%, or -1.7°C. For these reasons it is apparent that the measured error of the temperature transducer is well within tolerable limits.

Table 3.3.9 Calculated flow sensitivity to Temperature error. Error in flow calculation due to errors in the flow temperature verse the flow temperature.

Temp.	Error in flow temperature				
	1.0%	2.0%	3.0%	4.0%	5.0%
20.0	-0.122%	-0.245%	-0.367%	-0.490%	-0.612%
25.0	-0.151%	-0.301%	-0.452%	-0.603%	-0.753%
30.0	-0.178%	-0.356%	-0.534%	-0.712%	-0.891%
40.0	-0.231%	-0.461%	-0.692%	-0.922%	-1.153%

Chapter IV. CALCULATION OF RESPIRATORY VOLUMES

For the successful program implementation of the respiratory volume calculations (Appendix III) it is necessary to have a thorough understanding of the signals being transduced, the signal transducer outputs, and the calibration methods. The respiratory signals of interest are discussed in Chapter II. The temperature transducer is discussed in Chapter III and the GMS is discussed in Appendix II. The calibration methods are discussed in Chapter V and Appendix V. The calculation of gas volumes from the monitored signals is derived in Appendix III.

In a brief summary to Appendix III, these calculations allow for the computation of gas volumes using the PTG differential pressure, the temperature, the dry fractional oxygen concentration, the dry fractional carbon dioxide concentration signals, and the ambient conditions. From the PTG differential pressure signal and the calculated gas viscosity a flow signal is obtained. The flow signal is converted to STPD conditions using the flow temperature signal and the ambient conditions, resulting in a STPD flow. This flow is integrated over each inspiration and expiration to obtain the respective STPD tidal volumes which are then scaled to BTPS conditions. The individual STPD gas flow signals are obtained from the STPD flow and the dry fractional gas concentration signals. These gas flows are integrated to obtain inspiratory and expiratory gas volumes and the difference taken to obtain STPD volumes of O_2 consumed and CO_2 produced. These calculated data and the inspiratory and expiratory times are used to compute the breath-by-breath values. Simplifications and the program implementation of the volume calculations are presented in this chapter.

Consider the volume calculations developed in Appendix III

$$V(STPD) = \int \dot{V} \cdot K(P_b, F_{H_2O}, T) \cdot dt$$

where $V(STPD)$ is the STPD (Standard Temperature and Pressure; Dry) volume in liters, \dot{V} is the flow in liters per second. The unitless factor $K(P_b, F_{H_2O}, T)$ is used to convert the ITP (Instantaneous Temperature and Pressure) flow to STPD conditions. This factor is defined as:

$$K(P_b, F_{H_2O}, T) = [1 - F_{H_2O}] \cdot \frac{273.15}{273.15 + T_i} \cdot \frac{P_b}{760}$$

where P_b - the ambient barometric pressure (torr)
 F_{H_2O} - the fractional content of water vapor in the flow gas
 T - the temperature of the gas ($^{\circ}\text{C}$).

The volume calculation in terms of the differential pressure is equal to

$$V(\text{STPD}) = \int \frac{k\pi r^4}{81\mu} \cdot \Delta P \cdot K(P_b, F_{H_2O}, T) \cdot dt$$

where

ΔP - differential pressure obtained from the PTM (torr)
 μ - viscosity of the gas (μP)
 l - effective length of the PTM (cm)
 r - effective radius of the PTM (cm)
 k - 7.5062 (10^{-6}) ((dyne/cm²)/torr)

The viscosity, length, radius, differential pressure, and the ITP to STPD conversion factor vary throughout the respiratory cycle. From the work of Turney et. al. [19] the radius and length of a no. 1 Fleisch PTM vary less than 0.1% over the respiratory temperature range, 20 $^{\circ}\text{C}$ - 40 $^{\circ}\text{C}$. Assuming this is also the case with the larger no. 2 Fleisch PTM used in this study, these variables can be considered constant and pulled outside the integral to obtain

$$V(\text{STPD}) = \frac{k\pi r^4}{81} \int \frac{\Delta P}{\mu} \cdot K(P_b, F_{H_2O}, T) \cdot dt \quad 4.1$$

Wilke's equation can be used to calculate the overall viscosity of mixtures of these gases [8,9,20]. The general form of Wilke's equation is given by:

$$\mu_g = \frac{\sum_{i=1}^4 \frac{F_{w_i} \cdot \mu_i(T)}{\sum_{j=1}^4 F_{w_j} \cdot \beta_{ij}}}{\sum_{j=1}^4 F_{w_j} \cdot \beta_{ij}} \quad 4.2$$

where

μ_g - the overall gas viscosity (μP)
 μ_i - the viscosity of gas i (μP) at the temperature T
 F_{w_i} - the fractional concentration of gas i in the wet gas
 M_i - the molecular weight of gas i
 β_{ij} - a dimensionless constant developed by Wilke [20] as

$$\beta_{ij} = \frac{[1 + (\mu_i/\mu_j)^{(1/2)}(M_j/M_i)^{(1/4)}]^2}{[8 \cdot (1 + M_i/M_j)]^{(1/2)}} \quad 4.3$$

Over the respiratory temperature range the individual gas viscosities of O_2 , CO_2 , N_2 , and H_2O are linearly related to gas temperature. These linear approximations are shown in Table 4.1

Table 4.1 Linear approximation of pure gas viscosities between 20°C - 40°C

$$\mu_{O_2} = 191.0 + 0.616 T \quad [10]$$

$$\mu_{CO_2} = 137.6 + 0.450 T \quad [10]$$

$$\mu_{N_2} = 166.6 + 0.454 T \quad [10]$$

$$\mu_{H_2O} = 132.6 + 0.570 T \quad [19]$$

where

μ_x - the viscosity of gas x (μP)

T - the gas temperature ($^{\circ}C$)

These viscosity calculations are rather complex and, considering they are executed for each sample require a great deal of computer time. Wilke's Equations, 4.2 and 4.3, are the most complex and time consuming of these calculations. The iterative calculation of the denominator term in Equation 4.2 would require the largest amount of computer time. If this equation could be reduced to the linear combination of the individual viscosities a large amount of computation time would be saved. Turney et. al. [19] assumed mixtures of the four gases to have an overall viscosity equal to the linear combination of the viscosities of the components multiplied by their respective concentrations. However, this does not account for the complex interaction between the various gas components. This interaction is quantified with the β_{ij} term. In order to account for this interaction and maintain the simplicity of the linear combination, Equation 4.4 is considered

$$\mu_g = \frac{Fw_{O_2}\mu_{O_2}}{\lambda_{O_2}} + \frac{Fw_{CO_2}\mu_{CO_2}}{\lambda_{CO_2}} + \frac{Fw_{N_2}\mu_{N_2}}{\lambda_{N_2}} + \frac{Fw_{H_2O}\mu_{H_2O}}{\lambda_{H_2O}} \quad 4.4$$

where the λ s are constants which account for the gas interactions. To determine if this is a valid approximation of Equation 4.2 for the normal respiratory concentrations the amount of variation of the denominator terms are investigated.

Shown in Figure 4.1 are plots of the four denominator terms of Wilke's equation plotted against the flow of a single respiratory cycle. This cycle has respiratory signals similar to those of Figure 2.1.2. The curve is

traced as the gas composition and gas temperature varies throughout the respiratory cycle. The average value and standard deviation of these denominator terms over several normal respiratory cycles are listed in Table 4.2.

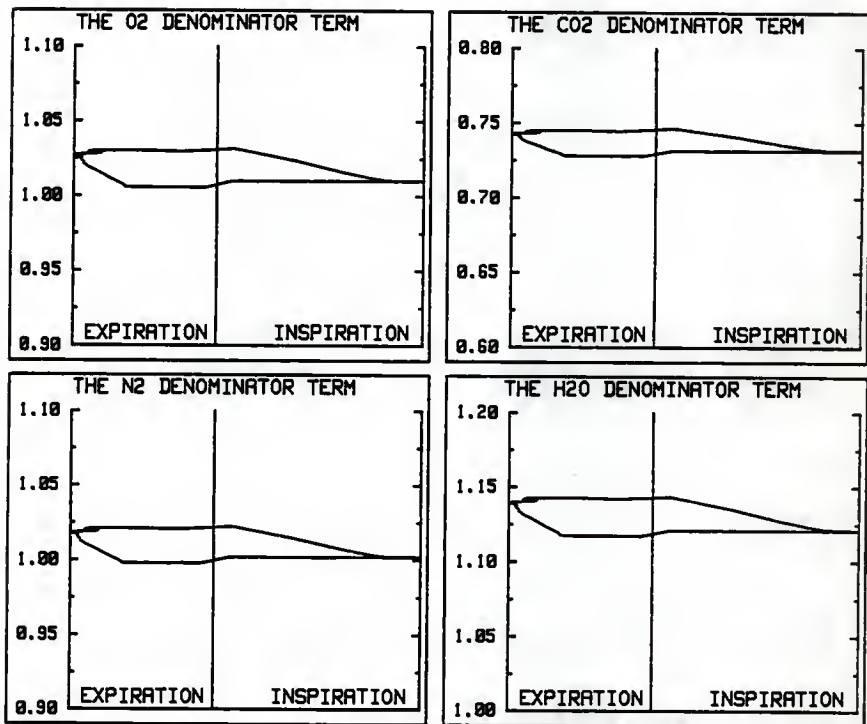


Figure 4.1 The denominator terms of Wilke's equation versus respiratory flow.

Table 4.2 Average values of the denominator terms of Wilke's equation

Gas	Average \pm 1 Standard Deviation
Oxygen	1.0157 \pm 0.0089
Carbon Dioxide	0.7353 \pm 0.0060
Nitrogen	1.0074 \pm 0.0084
Water Vapor	1.1274 \pm 0.0094

From Figure 4.1 and the standard deviation (less than 1%) it is apparent that these denominator terms are nearly constant. Therefore, a near linear relationship exists making the approximation of Equation 4.4 valid.

The constant λ values are equated to the averages of the denominator values. By incorporating these constants into the viscosity calculations of Table 4.1 the number of calculations may be reduced even farther. These modified viscosity equations are shown in Table 4.3.

Table 4.3
Modified linear approximations for pure
gas viscosities (20°C-40°C)

$$\begin{aligned}\mu'_{O_2} &= 188.0 + 0.606 T \\ \mu'_{CO_2} &= 187.1 + 0.612 T \\ \mu'_{N_2} &= 165.4 + 0.451 T \\ \mu'_{H_2O} &= 117.6 + 0.506 T \\ \mu'_x &= \text{the modified viscosity of gas } x \text{ (}\mu\text{P)}\end{aligned}$$

The overall viscosity can be found as the linear combination of the individual modified viscosities multiplied by their respective fractional concentrations.

$$\mu_g = Fw_{O_2}\mu'_{O_2} + Fw_{CO_2}\mu'_{CO_2} + Fw_{N_2}\mu'_{N_2} + Fw_{H_2O}\mu'_{H_2O} \quad 4.5$$

Using this linear approximation to calculate gas viscosity over several normal respiratory cycles results in an average error of 0.5% from the viscosity calculated with Wilke's equation.

A relative viscosity is defined as the viscosity of the gas relative to room air under STPD conditions. The value of relative viscosity is approximately equal to one. This allows the calibration factors calculated using viscosity and temperature corrections to be nearly equal to those calculated assuming the flow is directly proportional to the differential pressure.

$$\mu_r = \frac{\mu_g}{\mu_{STPD}} \quad 4.6$$

Applying these last few developments to Equation 4.1 results in the volume calculation of

$$V(STPD) = \frac{k\pi r^4}{8l\mu_{STPD}} \int \frac{\Delta P}{\mu_r} \cdot K(P_b, F_{H_2O}, T) \cdot dt \quad 4.7$$

The trapezoidal numerical integration technique is used to perform all integration operations.

Chapter V. SYSTEM CALIBRATION

Calibration factors must be determined in order to determine the respiratory signals in terms of their correct units. These factors relate the unitless binary sampled data, BCD data, to the physical phenomena being measured. Calibration of the gas mass spectrometer as presented by Creel [4] and Riblett [13] has not been altered and is not discussed here. The temperature transducer calibration procedure and an alternate scheme for calibration of the pneumotachograph (PTG) are presented. The new PTG calibration scheme uses viscosity and temperature corrections.

5.1 Temperature Calibration

The thermocouple based temperature transducer produces an output voltage related to the temperature at the thermocouple tip. Material presented in Appendix IV indicates that this temperature-voltage relationship is nonlinear. For the chromel-constantan thermocouple the temperature-voltage and, since the BCD sample is linearly related to the transducer voltage, the temperature-sampled voltage relationships may be modeled by second order polynomials over the respiratory temperature range ($20^{\circ}\text{C} - 40^{\circ}\text{C}$). To determine the relationship between the temperature and the sampled voltage, three temperature-BCD data points are taken. From these three points the second order relationship is generated.

The temperature calibration setup is shown in Figure 5.1.1. Three water baths are used to provide three input temperatures to the temperature transducer. Each water bath is heated with a separate aquarium heater. Each heater is controlled with a temperature controller in order to maintain the bath temperature at a constant level. The temperatures of the three water baths, 22°C , 30°C , and 39°C , are referred to as T_{low} , T_{mid} , and T_{high} respectively. The normal respiratory temperature range is spanned by these temperatures.

The tip of the thermocouple is placed into a water bath and the bath temperature is measured with a calibrated thermometer. The thermometer reading is entered into the computer. The computer program contains the thermometer's calibration factors so that the true temperature may be determined. The computer collects and averages 500 samples of the transducer output voltage. This step is performed for all three baths.

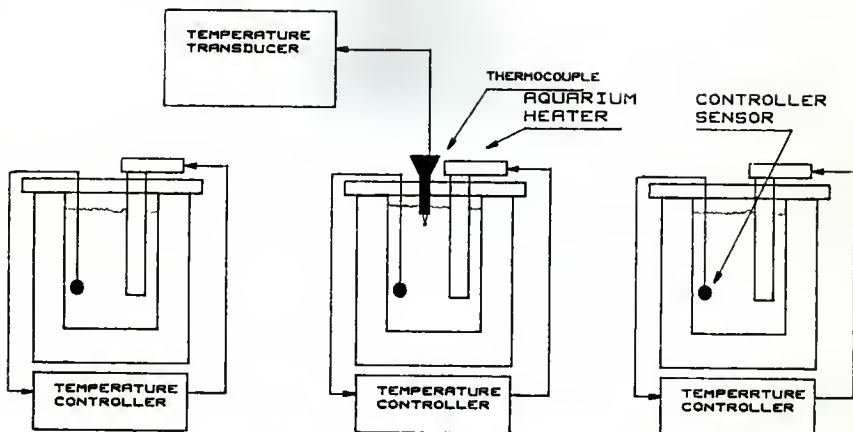


Figure 5.1.1 The equipment setup for the calibration of the temperature transducer.

The three calibration points $[T_{low}, B_{T1}]$, $[T_{mid}, B_{T2}]$, and $[T_{high}, B_{T3}]$ are used to generate the second order polynomial:

$$T = T_c + T_b \cdot B_T + T_a \cdot (B_T)^2 \quad 5.1.1$$

From the three calibration points, the equation:

$$\begin{bmatrix} T_{low} \\ T_{mid} \\ T_{high} \end{bmatrix} = \begin{bmatrix} 1 & B_{T1} & (B_{T1})^2 \\ 1 & B_{T2} & (B_{T2})^2 \\ 1 & B_{T3} & (B_{T3})^2 \end{bmatrix} \begin{bmatrix} T_c \\ T_b \\ T_a \end{bmatrix} \quad 5.1.2$$

is generated, where

- T - the temperature corresponding to the binary value B_T ($^{\circ}\text{C}$)
- B_T - the binary value corresponding to the TC transducer output
- T_c - the zero order calibration coefficient ($^{\circ}\text{C}$)
- T_b - the first order calibration coefficient ($^{\circ}\text{C}$)
- T_a - the second order calibration coefficient ($^{\circ}\text{C}$)
- B_{T1} - the binary value corresponding to the TC transducer output for a temperature of T_{low}
- B_{T2} - the binary value corresponding to the TC transducer output for a temperature of T_{mid}
- B_{T3} - the binary value corresponding to the TC transducer output for a temperature of T_{high}

Equation 5.1.2 is then solved for the calibration coefficients T_a , T_b , and T_c . These temperature calibration coefficients are used during flow cali-

bration and are stored for later use by the analysis routine.

5.2 Flow Calibration

The flow calibration of Creel [4] and Riblett [13] assumes that calibration and exercise data collection occur under the same temperature and water vapor conditions. It is hoped that by heating the PTM the temperature is nearly the same during calibration and data collection. However, it has been observed that with the #2 Fleisch PTM the temperature signal has an average temperature during calibration of 23°C and deviates about 2°C while during data collection it is approximately 10°C warmer. In addition, both inspiratory and expiratory water vapor content during calibration is that of room air which is usually less than 1% and seldom greater than 2%. During data collection the expiratory water vapor content can be as high as 6%. Also, Creel and Riblett neglected changes in the gas viscosity in order to assume the PTG differential pressure signal to be directly proportional to the flow. While this assumption is valid for constant gas composition, it is not valid when the gas composition varies. The amount of variance of the gas viscosity during respiration can be seen in Figure 5.2.1. The relative viscosity is plotted versus F_{CO_2} in the top figure and versus flow in the bottom figure. The constant conditions and constant viscosity assumptions used by Creel and Riblett lead to the possibility of errors in calculating volumes.

As discussed in Chapter IV, the gas viscosity can be calculated and used to convert the AP signal to a flow signal. Therefore, the PTG signal which is directly proportional to the AP signal can be converted to a signal that is directly proportional to the flow. The temperature signal may be used to convert this flow to any given temperature, pressure, and water vapor condition. This allows for the integration of a flow which is under constant conditions. For convenience the flow is converted to and integrated under STPD conditions. A scheme is presented which uses the flow gas temperature and the gas viscosity to calibrate the PTG.

The sampled binary value, B_p , of the PTG output is a linear function of the differential pressure, ΔP .

$$B_p = m \cdot \Delta P + b \quad 5.2.1$$

Ideally, two values of differential pressure, ΔP , and the corresponding

sampled values, the B_p values, can be used to solve for the two unknowns, the slope m and the y intercept b . A zero differential pressure is easily generated but it is difficult to generate a calibrated differential pressure across the screen of the PTM.

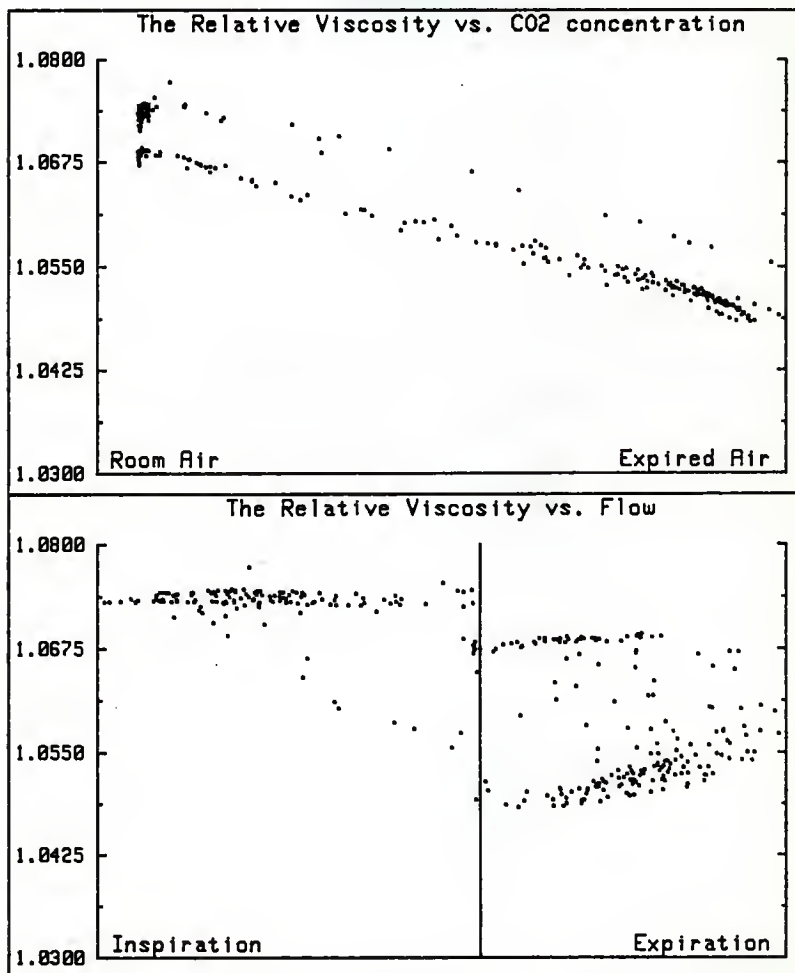


Figure 5.2.1 The variation of the relative viscosity throughout the respirator cycle.

The zero order term, b , is equal to the binary sample corresponding to zero differential pressure. Zero differential pressure is easily generated

by isolating the PTM from all air flow. This is accomplished by simply placing the PTM in a box. With the PTM isolated, 500 binary samples of the PTG output are collected and averaged. This average is then equated to the zero order term.

The scheme to complete the relationship of the sampled data to the differential pressure involves five steps. These steps are

1. Cycle a known volume through the PTM. A Harvard respirator is used to cycle a volume through the PTM.
2. Convert the PTG signal to a signal that is linearly related to the STPD flow using the gas viscosity and the conversion to STPD conditions.
3. Integrate the resultant signal over each inspiratory and each expiratory cycle of the respirator to obtain a volume that is directly proportional to the STPD respirator volume.
4. Average the individual inspiratory volumes and expiratory volumes.
5. Compute the proportionality constant by dividing the known respirator volume by the average values.

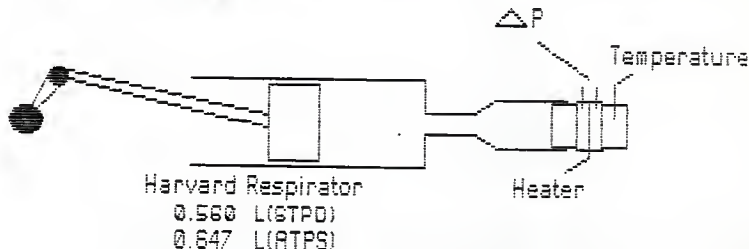


Figure 5.2.2 Equipment setup for the calibration of the PTG.

The calibration setup is shown in Figure 5.2.2. This, with the exception of the temperature transducer, is the same setup used by Creel [4] and by Riblett [13]. Separate inspiratory and expiratory calibration factors for inspiratory flows and expiratory flows are calculated. The use of separate inspiratory and expiratory flow calibration factors is suggested by Turney et al. [19] to account for the asymmetry of the PTM. The details of generating the calibration factors are presented here. Craal's scheme [4], also used by Riblett [13] is maintained with the present system.

Consider the volume calculations developed in Chapter IV and Appendix III.

$$V(\text{STPD}) = \int \dot{V} \cdot K(P_b, F_{\text{H}_2\text{O}}, T) \cdot dt$$

which in terms of the differential pressure is equal to

$$V(\text{STPD}) = \frac{k\pi r^4}{81\mu_{\text{STPD}}} \int \frac{\Delta P}{\mu_r} \cdot K(P_b, F_{\text{H}_2\text{O}}, T) \cdot dt$$

Rearranging Equation 5.2.1 so that the sampled data may be used to compute this volume yields

$$V(\text{STPD}) = \frac{k\pi r^4}{81\mu_{\text{STPD}}} \int \frac{(B_{\Delta P} - b)}{\mu_r} \cdot K(P_b, F_{\text{H}_2\text{O}}, T) \cdot dt$$

where b is the zero order term which corresponds to zero flow (zero ΔP). The constant term multiplying the integral is combined into a single factor known as the flow calibration factor. There are two calibration factors, one for inspiratory flow, \dot{V}_{Ical} , and one for expiratory flow, \dot{V}_{Ecal} (Note: these calibration values are related to but not equal to the first order coefficient, m , of Equation 5.2.1). The inspiratory and expiratory volumes are calculated by the integrals:

$$V_{\text{I}}(\text{STPD}) = \dot{V}_{\text{Ical}} \int_{\text{I}} \frac{(B_{\Delta P} - b)}{\mu_r} \cdot K(P_b, F_{\text{H}_2\text{O}}, T) \cdot dt \quad 5.2.3$$

$$V_{\text{E}}(\text{STPD}) = \dot{V}_{\text{Ecal}} \int_{\text{E}} \frac{(B_{\Delta P} - b)}{\mu_r} \cdot K(P_b, F_{\text{H}_2\text{O}}, T) \cdot dt \quad 5.2.4$$

The dry gas concentrations of O_2 , CO_2 , and N_2 needed in the calculation of relative viscosity are assumed to be that of room air ($F_{\text{O}_2} = 20.93\%$, $F_{\text{CO}_2} = 0.04\%$, and $F_{\text{N}_2} = 78.06\%$). The temperature is continually monitored during calibration in order to calculate the viscosity and to convert the computed flow to STPD conditions. The computations require the relative humidity, room temperature, and the barometric pressure.

The respirator cycles at 60 cycles per minute in order to create flows close to those of a subject. The determination of the ATPS respirator volume is outlined by Creel [4]. The respirator is connected to a spirometer. As the respirator slowly cycles (5 cycles/min), the spirometer displacement is recorded on chart paper. From the spirometer displacement the stroke volume may be computed. This volume is under ATPS conditions since the system is

equilibrated to ambient temperature and the gas is over water; therefore, is saturated with water vapor. By measuring the temperature of the water in the spirometer and barometric pressure the respirator volume can be converted to STPD conditions.

The respirator flow is sampled for 80 seconds generating approximately 80 respirator cycles. The value of the integrals (neglecting the calibration constants) in Equations 5.2.3 and 5.2.4 are calculated for each cycle and then averaged. The known STPD volume of the respirator is then divided by these averages to obtain the calibration factors:

$$\dot{V}_{I_{cal}} = \frac{\text{STPD respirator volume}}{\frac{1}{N} \sum_{i=1}^N \int_{I_i} \frac{(B_{AP} - b)}{\mu_r} \cdot K(P_b, F_{H_2O}, T) \cdot dt} \quad 5.2.6(a)$$

$$\dot{V}_{E_{cal}} = \frac{\text{STPD respirator volume}}{\frac{1}{N} \sum_{i=1}^N \int_{E_i} \frac{(B_{AP} - b)}{\mu_r} \cdot K(P_b, F_{H_2O}, T) \cdot dt} \quad 5.2.6(b)$$

With the method used by Creel and Riblett the volume of the respirator is determined under ATPS conditions and the integrand does not contain the viscosity term nor the ITP to STPD conversion factor. The integrals of Equations 5.2.3 and 5.2.4 simplify to

$$V_I = \dot{V}_{I_{cal}} \int_I (B_{AP} - b) \cdot dt \quad 5.2.7$$

$$V_E = \dot{V}_{E_{cal}} \int_E (B_{AP} - b) \cdot dt \quad 5.2.8$$

The calibration factors are then calculated by dividing the ATPS volume of the respirator by the average of the respirator cycles.

$$\dot{V}_{I_{cal}} = \frac{\text{ATPS respirator volume}}{\frac{1}{N} \sum_{i=1}^N \int_{I_i} (B_{AP} - b) \cdot dt} \quad 5.2.9(a)$$

$$\dot{V}_{E_{cal}} = \frac{\text{ATPS respirator volume}}{\frac{1}{N} \sum_{i=1}^N \int_{E_i} (B_{AP} - b) \cdot dt} \quad 5.2.9(b)$$

The use of the respirator volume under ATPS conditions by Creel [4] and Riblett [13] has the potential of leading to errors in volume calculations.

These errors arise because the PTG is calibrated under conditions other than ATPS. The goal of heating the PTM head is to bring its temperature to near body temperature. Assuming this is accomplished, the non-corrected calibration factors are computed by comparing the respirator volume under ATPS conditions ($T = 21^{\circ}\text{C}$, $F_{\text{H}_2\text{O}} = 2.6\% = 18.6/730$) to a volume computed at a temperature of 36°C and a water vapor concentration of less than one (room $F_{\text{H}_2\text{O}} = 30\%(18.6/730) = .7\%$). This leads to erroneous inspiratory and expiratory flow calibration factors. Also, during data collection the expiratory water vapor content is near 6% as compared to less than 1% during calibration. With this method the calibration volume is calculated under one temperature and pressure condition, the PTG calibrated under different conditions, and the expiratory volumes calculated under still another condition. By computing all volumes under STPD conditions these potentials for errors are reduced.

Chapter VI. SYSTEM SOFTWARE

The CBRMS system software developed by Creel [4] and modified by Riblett [13] for execution on the HP9826 system has been enhanced with volume calculations which use the temperature signal and the water vapor and viscosity calculations described in Chapter IV. Also, display of the breath-by-breath results using two breath combination (averaging) techniques has been integrated into the CBRMS. The plotting of the respiratory data, the printing of the breath-by-breath respiratory volumes, and the printing of the mean values have been maintained.

The external design of the software, as described by Riblett, has not been changed (with the exception of a few additional user inputs). Therefore, file compatibility and computer peripheral requirements remain the same. The calibration and respiratory data are collected using programs written in Pascal. The calibration and data collection routines store the data in temporary files using the same format (ASCII format). The ASCII format is necessary since it is the only file format which is compatible with both Basic and Pascal. The data are passed to the analysis routine in the same manner; via the ASCII files. However, the temporary ASCII data are optionally stored on the HP9895A 8-inch flexible disk, platter 1 of the HP9134A hard disk, or platter 2 of the hard disk (the medium used by Riblett). The ASCII data are converted to the numeric format of the Basic operating system and stored for a permanent record of the respiratory data using routines written in Basic. The data are analyzed using an enhanced analysis routine written in Basic.

While the external design of the software has not been changed from Riblett's version [13] the internal structure has. In order to take full advantage of the system languages, Hewlett-Packard's Basic and Pascal much of the code was converted to a structured format. Structured code consists of only three types of instructions; sequential, conditional, and iterative [15]. This reorganization resulted in code that is more compact, readable, and understandable.

The operation of the system software is outlined in Figure 6.1 and detailed operator instructions are given in Appendix V. Flowcharts for the various sections are presented in the latter portion of this Chapter and the actual program listings appear in the Appendix VI and Appendix VII.

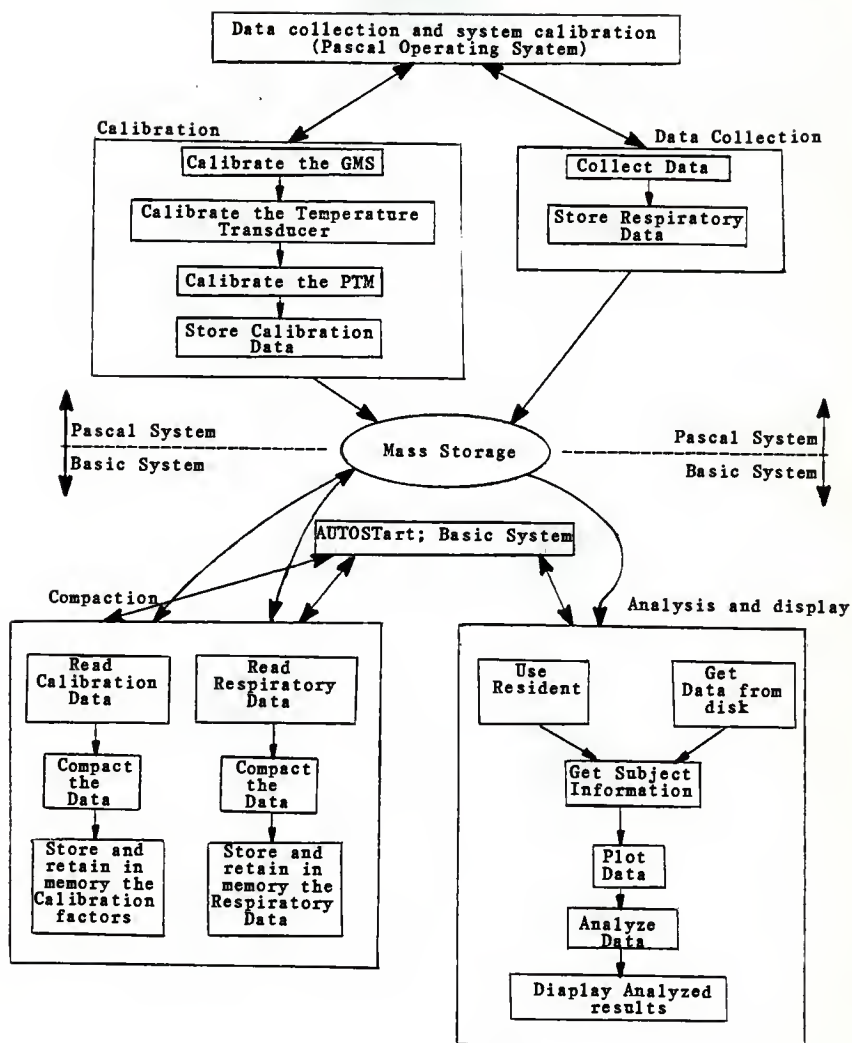


Figure 6.1 Organization of the CBRMS software

The calibration and respiratory data are collected with software written in Pascal. Pascal is required because of the need of assembly code to control the DAM in the collection of the data [13]. Calculation of the calibration factors for the system is accomplished with the Pascal program CAP2.CODE. The respiratory data are collected with the Pascal program DAP2.CODE. As mentioned, both Pascal programs store their data on disk in ASCII format. The Basic programs DAPCRUNCH and CAPCRUNCH convert this ASCII data to the more compact numeric format of the Basic system. The compacted data are stored on disk for a permanent record. These data are then used by the Basic program ANALYSIS to compute and display the various respiratory parameters.

6.1 CAP2.CODE: A Pascal Routine for System Calibration

CAP2.CODE (Calibration Program, version 2) determines calibration factors which are used to relate the sampled transducer outputs to the respiratory signals. Computation of the GMS calibration factors was developed by Creel [4] and the computation of the temperature transducer and flow transducer calibration factors is discussed in Chapter V. The flowchart of the calibration program is shown in Figure 6.1.1. The operator's instructions for CAP2 are given in Appendix V, Section A5.4.1, and the Pascal source code is documented in Appendix VI, Section A6.1.

When the program begins execution the sampling frequency is entered. This sampling frequency, generally 50 Hz, is used when the calibration points are being sampled. The GMS is the first device to be calibrated. The calibration of the GMS may be skipped, the same is true for the flow and temperature transducers. (Skipping any one of the calibration sections usually occurs only if a test is being conducted on a particular transducer or particular section of the calibration program.) The temperature transducer is calibrated next.

The PTG is the final transducer to be calibrated. If temperature and viscosity corrections are to be used the ambient temperature, humidity, and pressure are entered. A flow chart of the flow calibration scheme is presented in Figure 6.1.2 and is discussed shortly. Use of the temperature and viscosity calculations with the flow calibration may be optionally omitted.

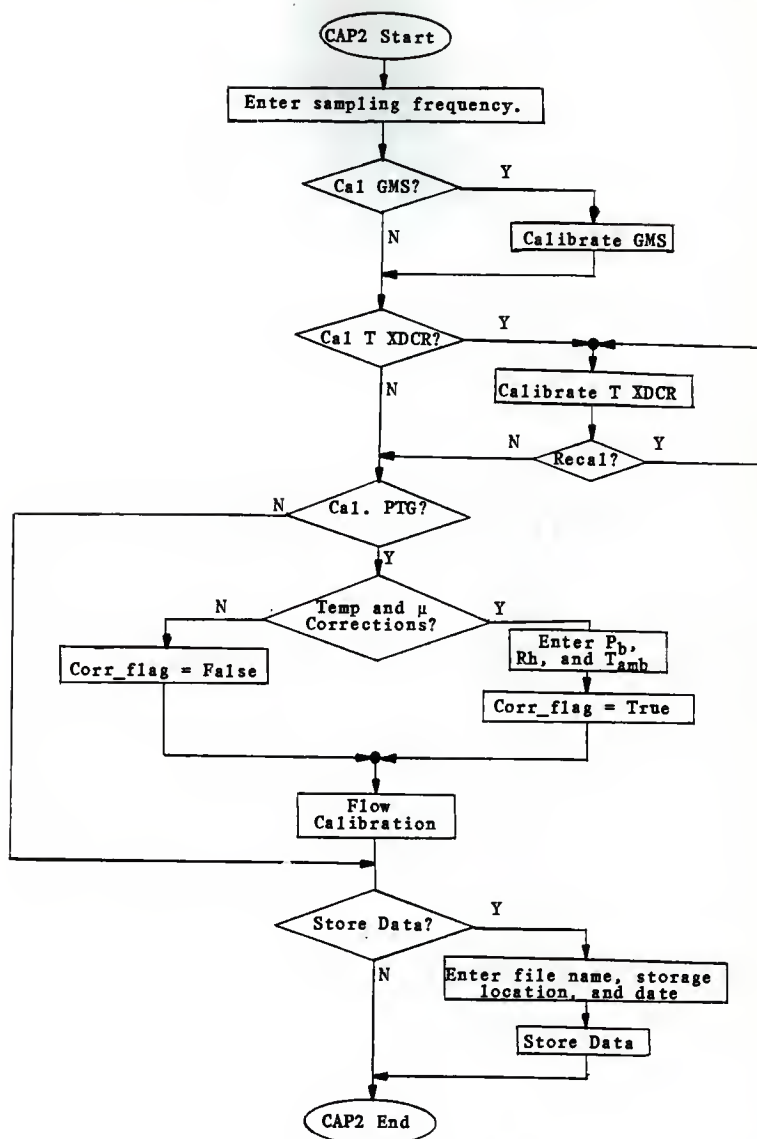


Figure 6.1.1 Calibration program, CAP2

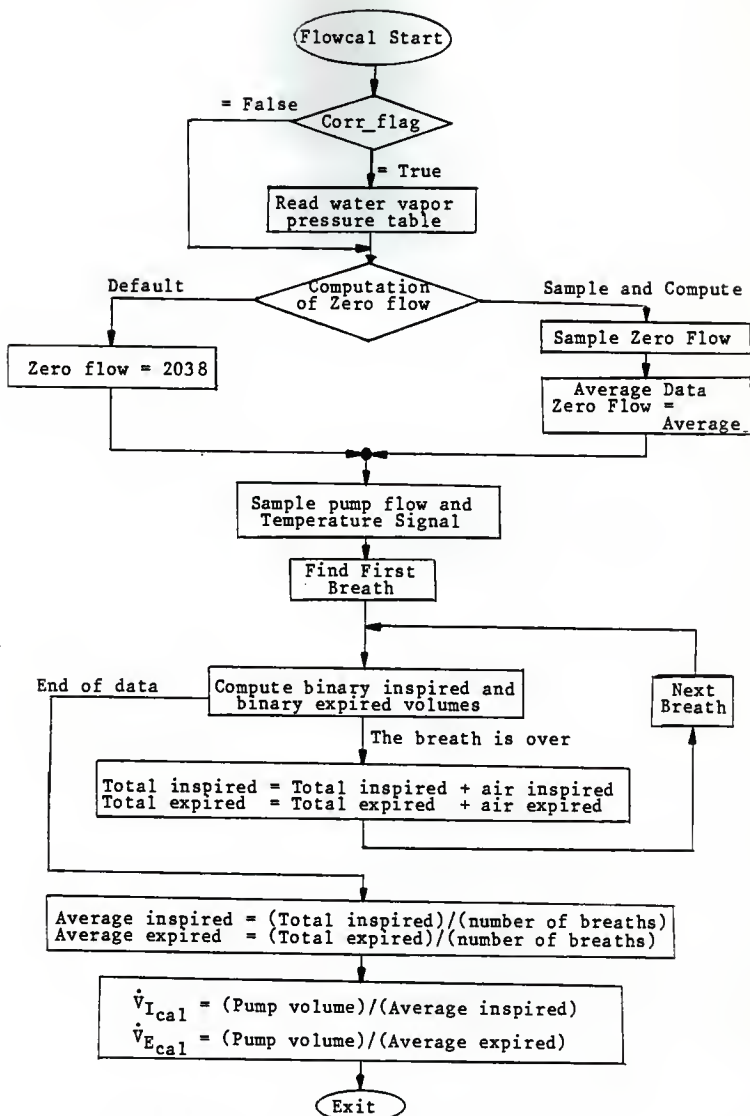


Figure 6.1.2 Flow calibration procedure

Finally the calibration data are stored along with the date. Program execution stops, and the computer operation returns to the Main Command Level of the Pascal operating system.

The flow chart of the flow calibration is outlined in Figure 6.1.2. First the binary value corresponding to zero flow is found. A default value of 2038 can be used for the binary value corresponding to zero flow (nearly all calculated zero flow values are equal to 2038).

The pump flow is then sampled for 4000 points. The binary inspiratory and expiratory volumes of the pump are computed (the computation of the binary volumes is presented in Section 6.5) for each cycle of the respiratory signal. During calibration two sets of the binary volumes are computed; one set uses temperature and viscosity corrections and the other uses no corrections. The binary volumes of each respiratory cycle are averaged. The inspiratory calibration factors are found by dividing the pump volume by the average inspiratory binary volumes. The same steps are performed with the corresponding expiratory volumes to determine the expiratory calibration factors. The routine then returns to the main calibration routine CAP2.CODE.

Below is a list of the major revisions to the original calibration program, CAP.CODE, described by Riblett [13].

1. Calibration of the temperature transducer can be repeated upon the user's request.
2. The PTG can optionally be calibrated using temperature and viscosity corrections in addition to the method used by Riblett.
3. The calibration data may be stored on one of three disk drives; platters 1 or 2 of the hard disk or the 8-inch floppy disk.
4. When data are being collected the number of samples and the length of time required to collect the samples are displayed.
5. The operator is prompted with an audible beep for all input data, just as occurs with the Basic routines.

6.2 DAP2.CODE: A Pascal Routine to Collect Respiratory Data

DAP2.CODE (Data Acquisition Program, Version 2) collects the respiratory data from the subject and stores the data on disk using ASCII format. Version one of this program was written by Riblett [13] and only minor

modifications were made for version 2. The flowchart for DAP2 is shown in Figure 6.2.1. The operator's instructions for DAP2 are given in Appendix V, Section A5.4.2 and the Pascal source code is documented in Appendix VI, Section A6.2.

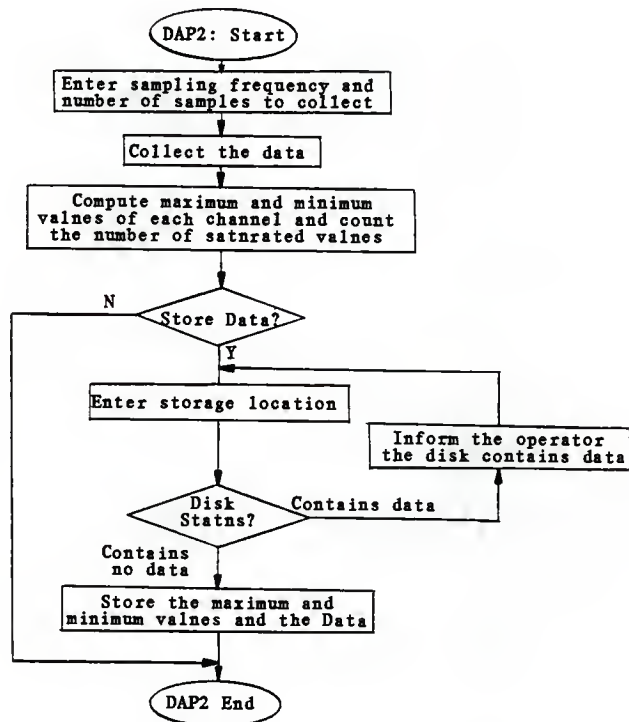


Figure 6.2.1 Data acquisition program, DAP2

The modifications to version 1 of the data acquisition program are listed below.

1. The respiratory data may be stored on one of three disk drives; platters 1 or 2 of the hard disk or the 8-inch floppy disk.
2. The ASCII data are protected from accidentally being overwritten.

3. When the data are being collected the number of samples and the length of time required to collect the samples are displayed.
3. The number of data points equal to the positive saturation value of the A/D, 4095, and the number equal to the negative saturation value of the A/D, 0, are counted and displayed for each channel.
4. The operator is prompted with an audible beep for all input data, just as occurs with the Basic routines.

6.3 AUTOST, CAPCRUNCH, and DAPCRUNCH: Auto-start and File Compaction Routines

The auto-start program, AUTOST, serves as a link between the various routines written in Basic. CAPCRUNCH and DAPCRUNCH are Basic programs which convert the data stored on disk in ASCII format by the Pascal programs CAP2.CODE and DAP2.CODE to the more compact numeric formats of the Hewlett-Packard Basic. This compaction greatly reduces the amount of storage space required for the data and the length of time to retrieve the data from disk. The operator's instructions for AUTOST, CAPCRUNCH, and DAPCRUNCH are given in Appendix V, Section A5.5, and the Basic programs are documented in Appendix VII, Sections A7.3, A7.4, and A7.5.

The flowchart of Figure 6.3.1 is a combination of three separate programs. The auto-start program, AUTOST, serves as a link between the three CBRMS programs; DAPCRUNCH, CAPCRUNCH, and ANALYSIS; by allowing them to be executed with the press of a key. Another Basic program, STOREHR (Store Heart Rate) can be loaded from AUTOST. AUTOST also allows several other useful operations; CATALOGING of disks, setting the default mass storage device, and loading other programs.

CAPCRUNCH, converts (crunches) the calibration factors computed and stored (in ASCII format) by the Pascal program CAP2.CODE from the ASCII format to the more compact numeric format of the Hewlett-Packard's 9826 Basic. DAPCRUNCH does the same for the respiratory data collected and stored by Pascal program DAP2.CODE. Below is a list of the revisions made to these programs.

1. A common area of memory has been set up so that the data read by the CAPCRUNCH and DAPCRUNCH programs remain in memory to be used by the ANALYSIS program.

2. The ASCII data can be read with the crunching programs from either platter 1 or platter 2 of the hard disk or the 8-inch disk drive.
3. The file names of the respiratory data are entered at the beginning of the DAPCRUNCH program. This allows the names to be entered all at once and then the data from all four channels are read in and converted and finally stored without the need for further operator input.

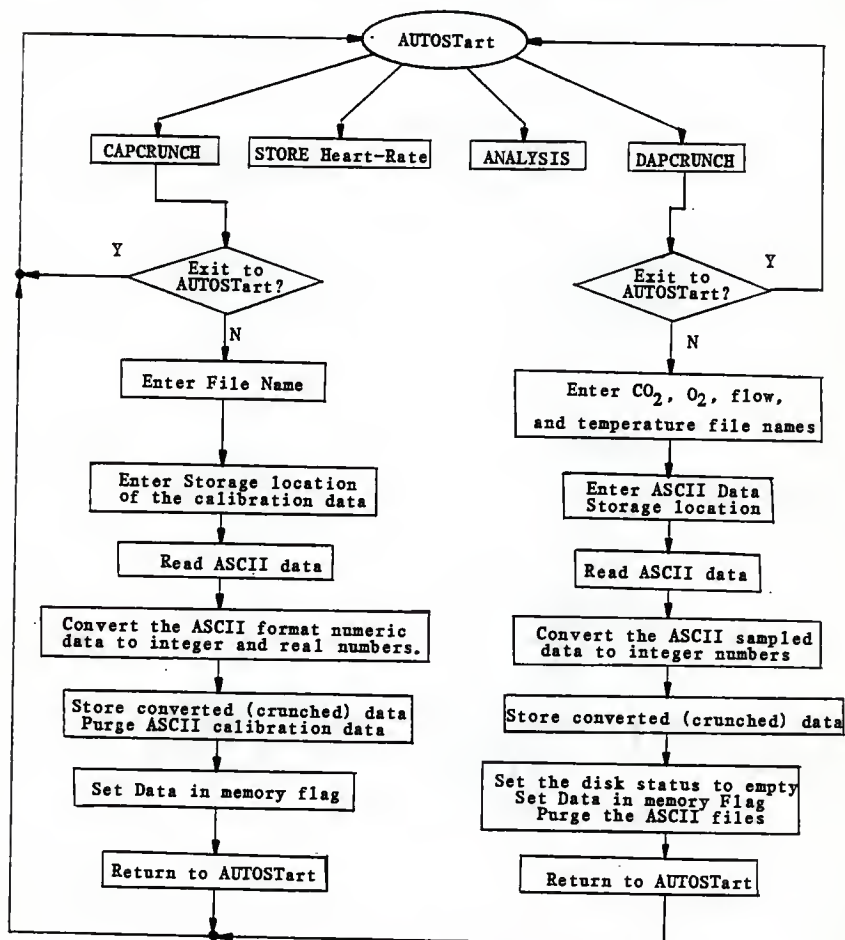


Figure 6.3.1 AUTOST, CAPCRUNCH, and DAPCRUNCH programs

6.4 ANALYSIS: A Basic Routine to Calculate the Respiratory Parameters

ANALYSIS is the analysis routine which performs the computations necessary to yield the respiratory parameters described in Chapter IV. These parameters may be displayed in a variety of formats. The operator's instructions for ANALYSIS are given in Appendix V, Section A5.6, and the Basic program documentation is in Appendix VII, Section A7.6.

Figure 6.4.1 shows the flowchart of ANALYSIS. The analysis program is called from the AUTOSTart program, as shown in the flowchart of the AUTOSTart program (Figure 6.3.1). System operation can also return from the analysis program to the AUTOSTart program. The first section of the analysis program obtains the necessary subject information, the subject's respiratory data, and the calibration data. The respiratory and calibration data may be resident in memory due to the execution of the data compaction programs, CAPCRUNCH and DAPCRUNCH, or previous execution of the analysis program. These data may be used by the analysis program or new data may be read from disk.

The operator selects the type of GMS time delay [13], breath-by-breath or fixed, and whether temperature and viscosity calculations are to be used in computing respiratory flow. The operator may plot the raw respiratory data. The window of data points for which the respiratory parameters are to be calculated is selected and the calculation of the respiratory parameters for that window begins.

The GMS time delay for the breath being analyzed is determined first. The time delay is either a fixed value or a computed value. The algorithm for the computation of the breath-by-breath time delay was presented by Riblett [13]. The binary volumes of air, oxygen, and carbon dioxide are computed. The computation of the binary volumes is described in Section 6.5 (this is the same flowchart used by the calibration program; CAP2.CODE, Section 6.1; to compute the binary pump volumes). The flow calibration factors are used to convert the binary volumes to the various respiratory volumes having the units of liters. The respiratory volumes may be printed for each breath being analyzed; however, most information can be attained from the later display. These respiratory volumes and the duration of the respiratory cycle are used to compute the other respiratory parameters; minute values, respiratory quotient, and respiratory frequency. All respiratory parameters are retained for later display. After all data in the

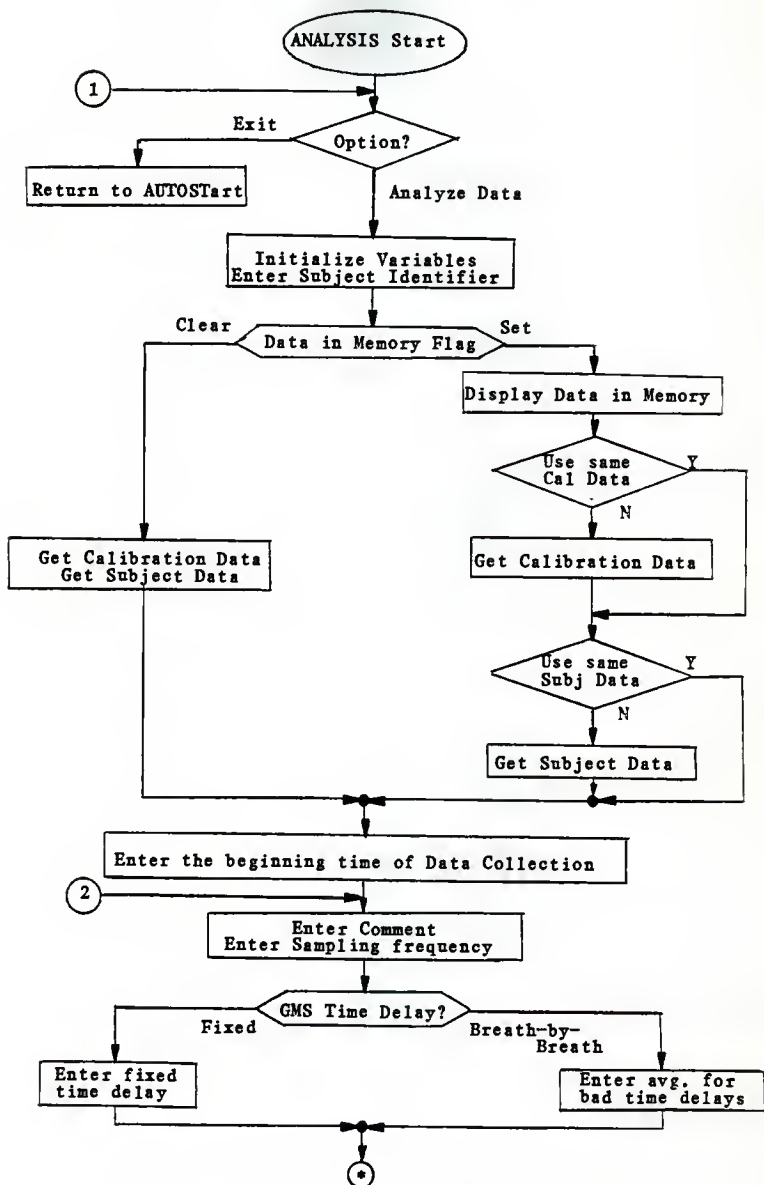


Figure 6.4.1 Data analysis program, ANALYSIS

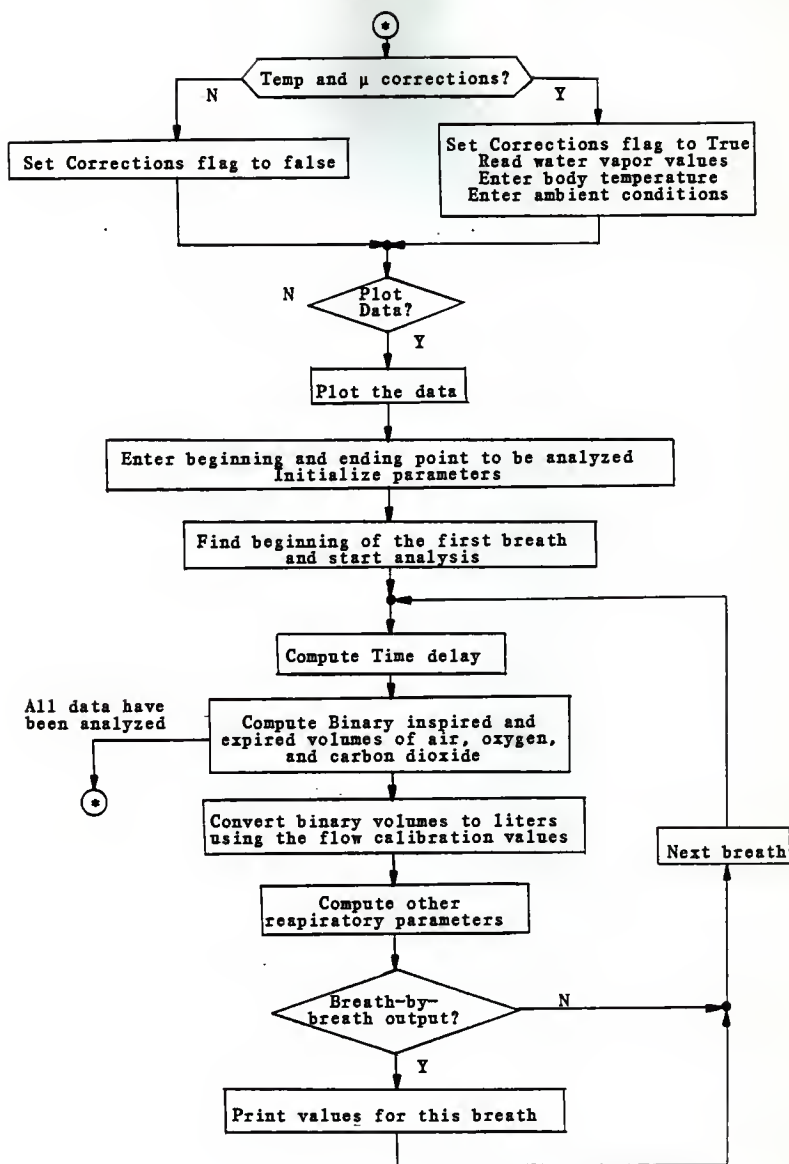


Figure 6.4.1 (continued)

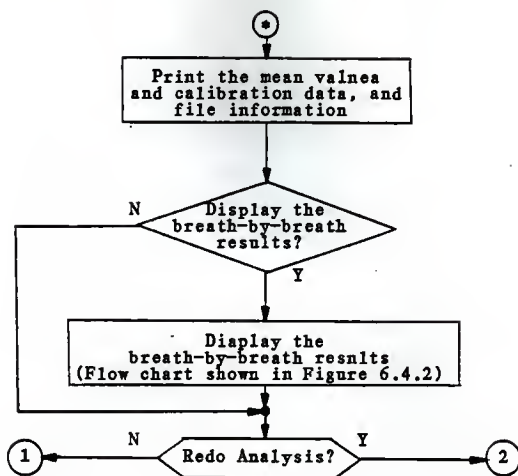


Figure 6.4.1 (continued.)

specified window have been analyzed the mean respiratory parameters for that window are computed and printed.

Following the printing of the mean values the computed breath-by-breath respiratory parameters may be displayed. The flowchart for the display of the breath-by-breath data is shown in Figure 6.4.2. Successive breath-by-breath values may be combined by one of two techniques; breath averaging, flowchart shown in Figure 6.4.3, or window averaging, flowchart shown in Figure 6.4.4. All of the respiratory parameters may be printed or any two parameters may be plotted. After the parameters have been displayed, control may be passed back to the main portion of the analysis program or additional parameters may be displayed.

The first of the breath combination techniques is breath averaging, Figure 6.4.3. The specified number of breath-by-breath values are summed. A breath is not included in the sum if it is considered a bad breath and the operator specifies that the bad breaths are to be omitted. A bad breath is defined as a breath that has an inspiratory tidal volume or an expiratory tidal volume of less than or equal to 400mL. The summing continues until the specified number of breaths have been averaged or no more breath-by-breath data are available. The average is computed. The routine then returns the average value, the time value that is midway between the first breath and the

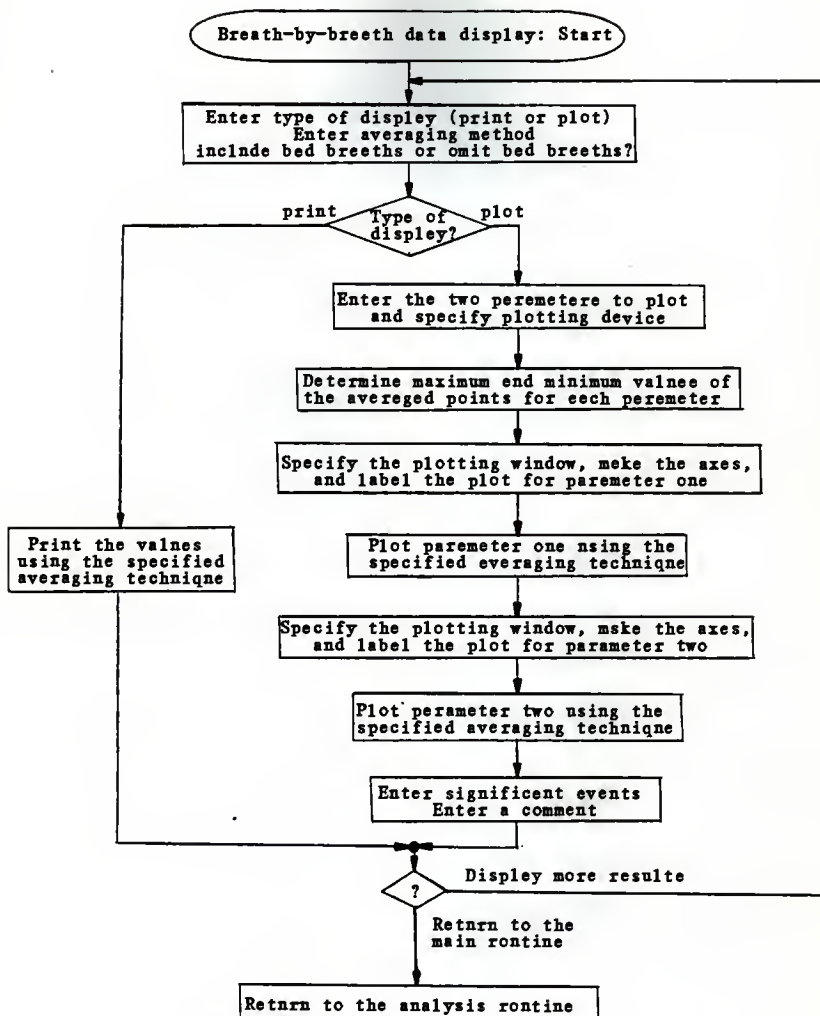


Figure 6.4.2 Display of the breath-by-breath data

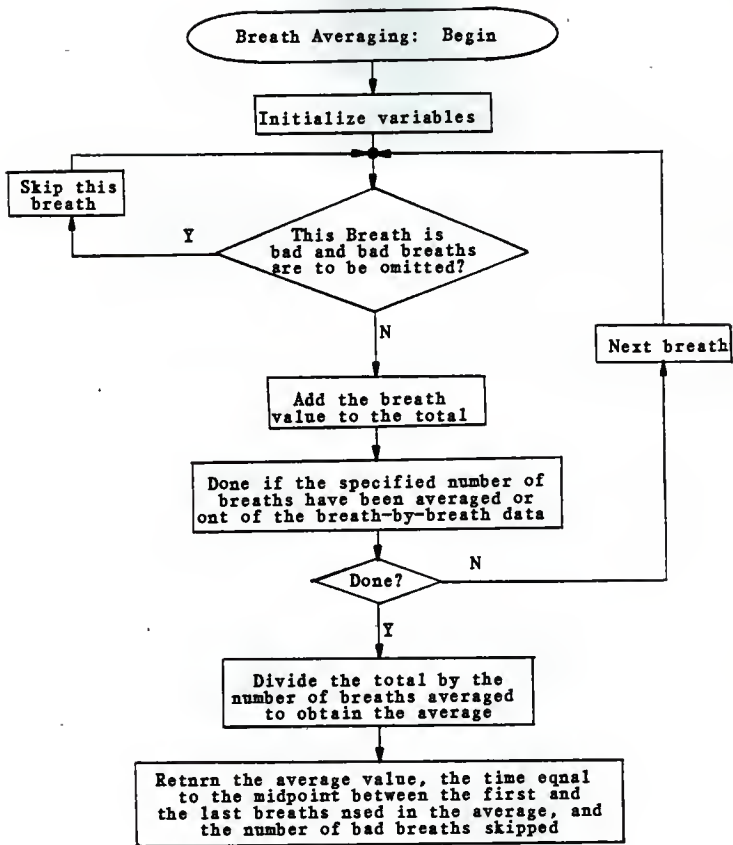


Figure 6.4.3 The breath averaging procedure

last breath averaged, and the number of bad breaths that are skipped.

The flowchart for the window averaging technique is shown in Figure 6.4.4. The goal of the window averaging technique is to look at a window in time and average all the breath values in that window. This is illustrated in Figure 2.2.3 for two windows.

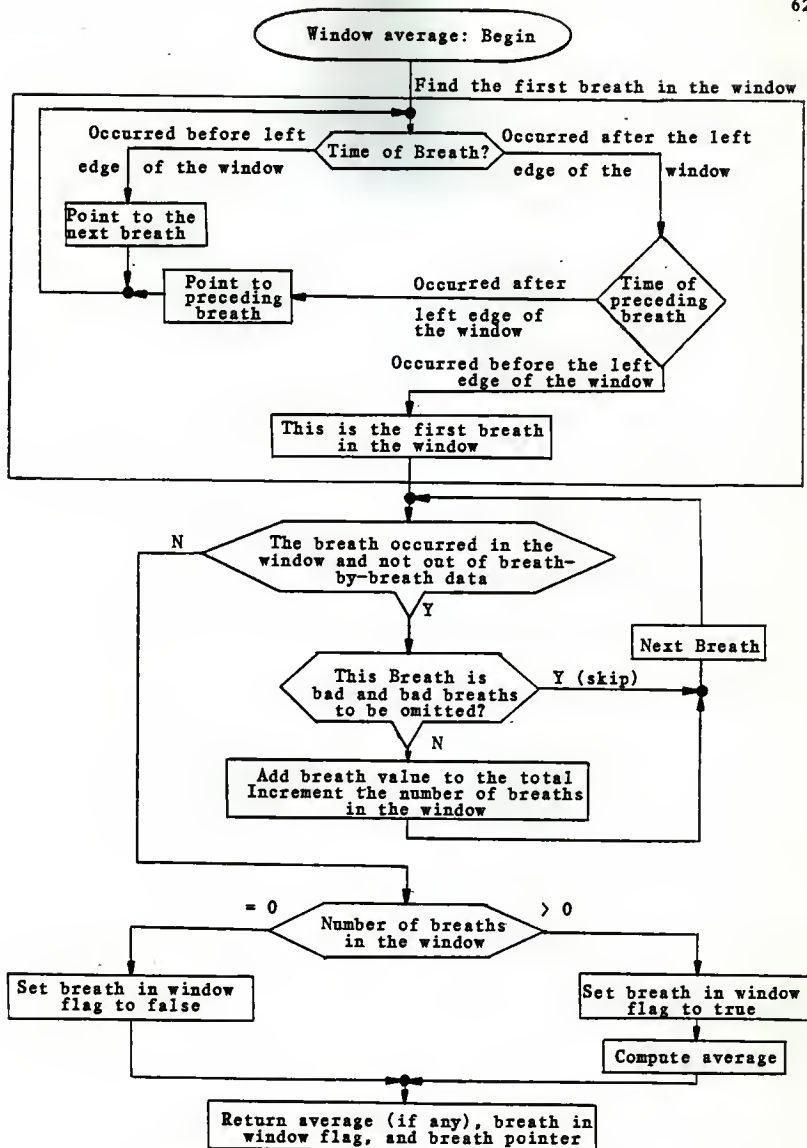


Figure 6.4.4 The window averaging procedure

The first thing the window average routine does is to find the first breath that occurred in the window. The time of a breath is checked. If the time of this breath precedes the left edge of the window then the next breath is tested. If the time of the breath occurs after or at the same time as the left edge of the window then the preceding breath is checked. If the time of the preceding breath precedes the left edge of the window then the breath being checked is the first breath in the window. If the time of the preceding breath is to the right of the left edge of the window then the breath being checked is not the first breath in the window and the preceding breath is checked.

Once the first breath in the window is found the remaining breaths in the window are averaged. This is done by summing the breath values for each breath in the window. If a breath is bad and the bad breaths are to be omitted then it is not included in the sum. Once the time of a breath is to the right of the window the summing stops. The sum is divided by the number of breaths included in the sum to obtain the average. If the window did not contain any breaths then a flag is set and the average is not computed.

Below is a summary of the major additions to the ANALYSIS routine.

1. The respiratory data and calibration data are retained in memory from the previous execution of the crunching routines or analysis routine. This bypasses the need to read data from disk for each execution of the analysis routine.
2. The printed output of the breath-by-breath volumes may be omitted. This increases the execution speed of the analysis program.
3. The breath-by-breath results may be plotted or printed. The individual values may be displayed or groups of the breath-by-breath values may be combined.

6.5 Computation of the Binary Volumes

The trapezoidal rule is used to implement the computation of the binary volumes of the various respiratory gases. The computations are developed in Appendix III and Chapter 4. The flowchart implementation of this scheme is shown in Figure 6.5.1.

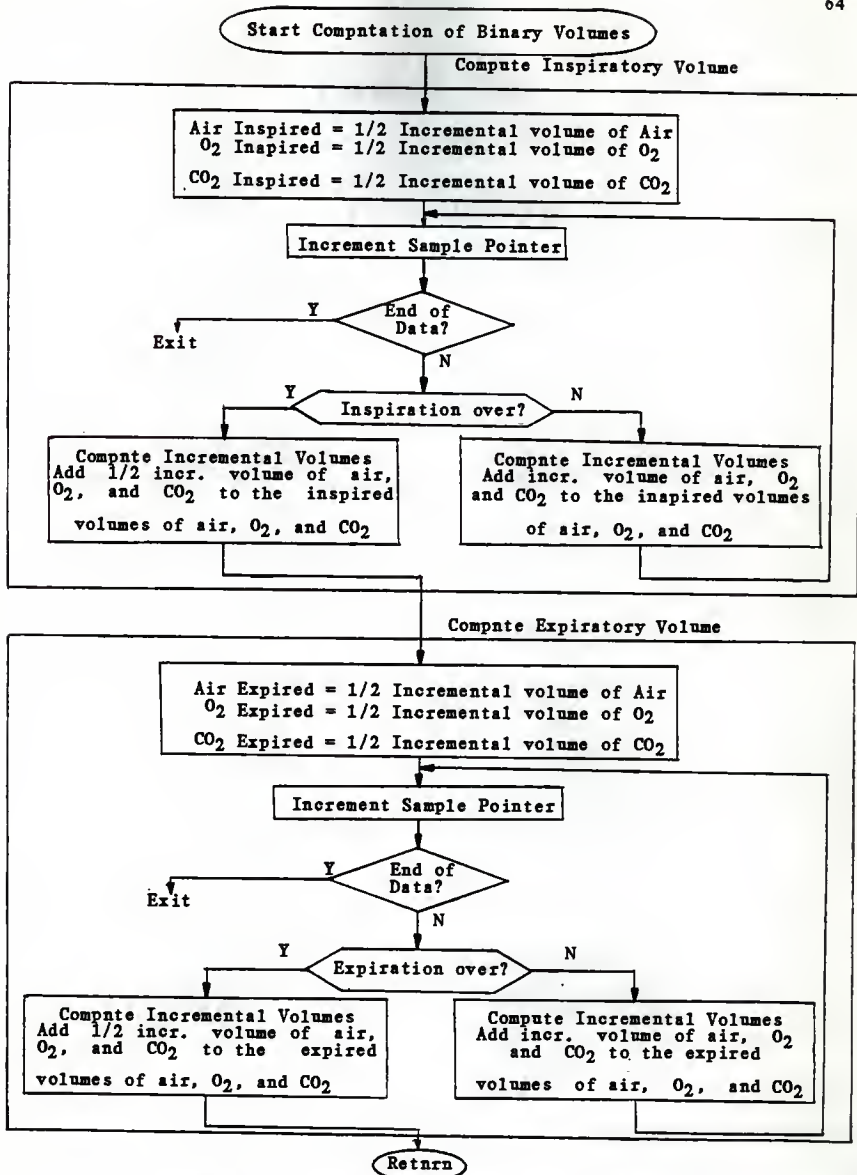


Figure 6.5.1 Computation of the binary volumes.

Half of the incremental volumes corresponding to the first inspiratory point is set equal to the accumulated inspired volumes. The incremental volumes of all inspiratory flows are then added to the accumulated inspiratory volumes until the inspiratory/expiratory transition is found. Half of the incremental volumes of the various respiratory gases corresponding to this transition are added to the accumulated inspiratory volumes while the other halves are used to initialize the accumulated expiratory volumes. The incremental volumes during expiration are added to the accumulated volumes until the expiratory/inspiratory transition is found. Half of the respiratory gases corresponding to this transition are added to the expiratory volumes. This transitory point is then the beginning point of inspiration for the next respiratory cycle.

6.6 STOREHR: A Basic Routine to Store the Heart Rate Values

STOREHR is a simple Basic program which allows the operator to enter the heart rate values and also store the values in a format compatible with Sprick's general purpose plotting program [16]. The flowchart for the program is shown in Figure 6.6.1. Sprick's plotting routine may be loaded, if so desired, which would allow the heart rate values previously stored to be plotted. When using Sprick's plotting routines enter TIME for the X-axis variable, MIN for X-axis units, and 2 (2 samples/min) for the sampling frequency. The operator's instructions for STOREHR are given in Appendix V, Section A5.7 and the Basic program documentation is in Appendix VII, Section A7.7.

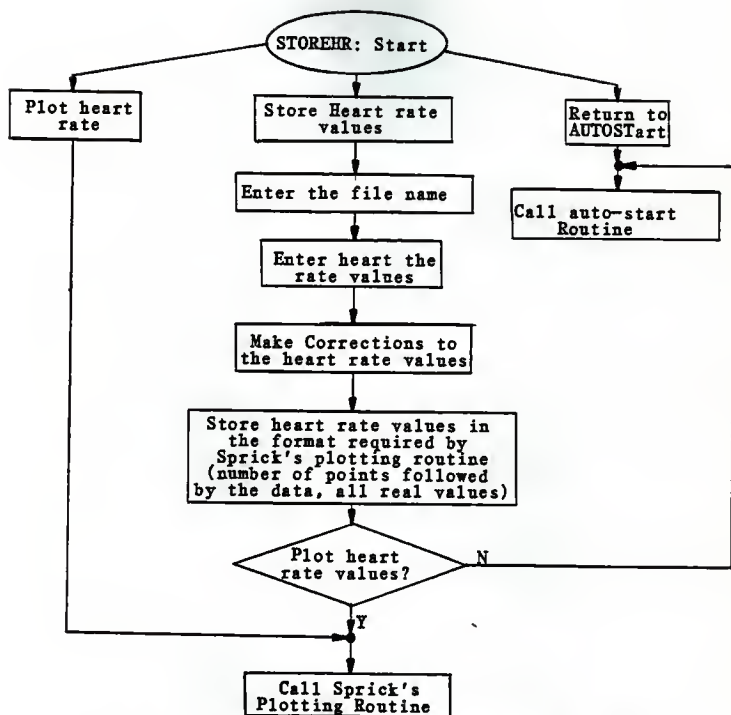


Figure 6.6.1 The heart rate storage program, STOREHR

Chapter VII. EXPERIMENTAL VERIFICATION OF THE SYSTEM

The computation of the various breath-by-breath respiratory parameters is based on two basic principles; the computation of respiratory cycle time and the computation of the respiratory volumes. The computation of the cycle time is a trivial task for the computer system provided the data acquisition system is functioning properly. The computer simply counts the number of samples involved with the respiratory cycle and divides this number by the sampling rate. The computation of the respiratory volumes on the other hand is a very complex matter. This is readily apparent from the development of Chapters IV and V and Appendix III. The calculations for the respiratory volumes are repeated below.

Inspiratory (Expiratory) tidal volumes

$$V_{I(E)}(\text{BTPS}) = \int_{I(E)} \dot{V}_{\text{STPD}} dt \cdot \frac{273.15 + T_b}{273.15} \cdot \frac{760}{P_b - P_{H_2O}(T_b)}$$

Volumes of O_2 consumed and CO_2 produced

$$\begin{aligned} V_{O_2} &= \int_I F_{O_2} \cdot \dot{V}_{\text{STPD}} dt - \int_E F_{O_2} \cdot \dot{V}_{\text{STPD}} dt \\ V_{CO_2} &= \int_E F_{CO_2} \cdot \dot{V}_{\text{STPD}} dt - \int_I F_{CO_2} \cdot \dot{V}_{\text{STPD}} dt \end{aligned}$$

From these equations the dependency of the volume calculations on a variety of variables is apparent. Essential to these volume calculations is the ability to obtain a valid flow signal under a known pressure, temperature, and water vapor condition. In this case the flow is under STPD conditions. In addition to the dependency on the valid flow signal, the calculations of V_{O_2} and V_{CO_2} are dependent on knowing the fractional O_2 and CO_2 composition signals. The Perkin-Elmer GMS provides very accurate fractional content signals. The method for calculation of the GMS delay time provides the necessary time alignment of the fractional composition signals with the flow signal [13].

The respiratory signals are slowly varying relative to the 50 Hz sampling frequency. The trapezoidal numerical integration technique is sufficient for integrating slowly varying signals. Therefore, the final critical link in the calculation of the respiratory volumes is the attainment of a valid flow signal.

The STPD flow, \dot{V}_{STPD} , is given by

$$\dot{V}_{\text{STPD}} = [\Delta P / \mu] K(P_b, F_{\text{H}_2\text{O}}, T)$$

where the factor $K(P_b, F_{\text{H}_2\text{O}}, T)$ is the ITP to STPD conversion factor

$$K(P_b, F_{\text{H}_2\text{O}}, T) = [1 - F_{\text{H}_2\text{O}}] \cdot \frac{273.15}{273.15 + T} \cdot \frac{P_b}{760}$$

In terms of the sampled data the flow is equal to

$$\dot{V}_{\text{STPD}} = \dot{V}_{\text{I(E)}}_{\text{cal}} [(P_b - b) / \mu_r] K(P_b, F_{\text{H}_2\text{O}}, T)$$

The possible errors in the calculation of the STPD flow can be seen from these equations and are summarized here:

1. The determination of the calibration factors, $\dot{V}_{\text{I(E)}}_{\text{cal}}$.
2. The determination of the binary sampled value corresponding to zero flow through the PTM, b .
3. The determination of the relative gas viscosity, μ_r .
4. The determination of the barometric pressure, P_b .
5. The determination of the $F_{\text{H}_2\text{O}}$ value throughout the respiratory cycle.
6. The measurement of the respiratory flow temperature signal, T .

The barometric pressure is constant over a short period of time and is easily measured. The value corresponding to zero flow is also easily determined. Therefore, these two sources of error can be immediately discounted.

It was shown in Chapter III that the temperature transducer could measure temperature with sufficient accuracy. The determination of the fractional content of water (inspiratory $F_{\text{H}_2\text{O}}$ is equal to that of room air and expiratory $F_{\text{H}_2\text{O}}$ is equal to the saturated value) appears to be accurate and consistent with the methods of other researchers. An alternative to determining the temperature and water vapor content is to maintain them at constant, known value. The PTM may be heated in an attempt to maintain a constant flow temperature but the success of this procedure is suspect. The water content of the flow signal can not be maintained constant. The water content in the inspiratory air is equal to the water content of room air (generally less than 1%) while during expiration the water content is much higher (5% - 6%). Therefore, the temperature and water vapor content should

be monitored. The final two possibilities which could lead to errors in the flow signal are the determination of the calibration factors and the determination of the relative gas viscosity.

To investigate the validity of the methods used to calculate the respiratory volumes a Harvard respirometer is used to cycle a known volume through the PTM. The resultant flow signal is integrated and the calculated volume compared with the known pump volume. The gas content and the temperature are altered to determine the effect on the volume calculations. These alterations assess the relative viscosity and the temperature of the gas to vary from the conditions of calibration. The premise of this testing is to show that the CBRMS can compute the pump volume accurately; therefore, showing that the calculated flow signal and integration technique are valid. With a valid STPD flow signal the O_2 and CO_2 volumes are accurate since the fractional content signals with the associated GMS time delay provide an accurate fractional content of the dry gas.

It should be pointed out that a nonconversion of the flow signal to STPD conditions causes an error in the calculation of the O_2 and CO_2 gas volumes. This is because a flow which contains water vapor is multiplied by the F_{O_2} and F_{CO_2} signals which are the fractional content of O_2 and CO_2 in the flow neglecting the volume of water vapor. Therefore, the computed gas volumes are over estimated, especially the expiratory volumes which are saturated with water vapor.

In addition to this test, the respiratory measurements taken from two healthy male subjects are presented and discussed.

7.1 Experimental Methods

The experimental apparatus shown in Figure 7.1.1 is used to cycle a volume of gas equal to the pump volume through the pneumotachometer. Data are collected with the CBRMS under three conditions:

1. with the Douglas bag disconnected (the same conditions that the PTM is calibrated under),
2. with the Douglas bag containing room air,
3. and with the Douglas bag containing a gas mixture of approximately 6% CO_2 and 14% O_2 with the balance of N_2 .

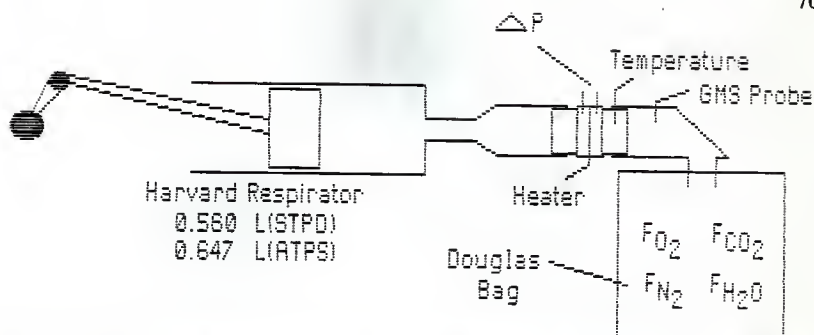


Figure 7.1.1 Experimental setup used to cycle a known volume of gas under known conditions through the PTM.

The temperature transducer is used to monitor the flow temperature and the GMS is used to monitor the fractional content of O_2 and CO_2 in the gas. The system is calibrated and data are collected using the normal procedures, Appendix V, Section A5.4. The data are analyzed using a modified version of the ANALYSIS program. The modifications to the ANALYSIS program are listed below.

1. Two sets of inspiratory and expiratory volumes are calculated. One set of the inspiratory and expiratory volumes use the temperature and viscosity calculations (referred to as method A) to determine the flow prior to integration. The other set of inspiratory and expiratory volumes are calculated using Riblett's method (referred to as method B). That is, the flow is linearly related to the PTG differential pressure signal and is under constant temperature and water vapor conditions.
2. The inspiratory and expiratory volumes calculated using the viscosity calculations are not scaled to BTPS conditions. This allows for direct comparison between the computed STPD volume and the STPD pump volume.
3. The average viscosity, average fractional O_2 and CO_2 content, and average temperature of the gas mixture are calculated.
4. The fractional content of water vapor in the flow air is a constant value.

7.2 Experimental Results and Conclusions

The experimental results are shown in Table 7.2.1, Table 7.2.2, and Figure 7.2.1. The average conditions of the flow gas for the various trials are given in Table 7.2.1. The computed average inspiratory and expiratory pump volumes are listed in Table 7.2.2. Shown in Figure 7.2.1 are the typical signals recorded with the CBRMS.

The error values of the first trial with the PTM connected to the Douglas bag, Table 7.2.2 (b) and Table 7.2.2 (c), are extremely large. This large error is due to a poor connection between the pump and the PTM which allows air to escape. The reason the errors are small with the bag disconnected is because the same amount of air escaped during calibration as during data collection; therefore, the calibration factors are also in error. These two errors cancel. However, with the bag connected to the PTM the resistance to flow is altered so that the amount of air passing out the leak is also altered. This air leak is not present with the data collected for the remaining trials.

Table 7.2.1 The average conditions of the flow gas. (a) The flow air is room air. (b) The flow air is room air with an elevated temperature. (c) The flow air was a mixture of approximately 6% CO₂, 14% O₂, and a balance of N₂.

Table 7.2.1 (a)

Trial	Date	Average Temp.	Average O ₂ conc.	Average CO ₂ conc.	Average Viscosity
1	2/25/85	23.7	21.00%	0.00%	184.65
2	2/26/85	24.4	21.00%	0.00%	185.13
3	2/28/85	24.6	21.09%	0.00%	185.22
4	3/1/85	24.6	20.09%	0.00%	185.22

Table 7.2.1 (b)

Trial	Date	Average Temp.	Average O ₂ conc.	Average CO ₂ conc.	Average Viscosity
1	2/25/85	38.8	21.05%	0.02%	189.92
2	2/26/85	29.3	21.02%	0.04%	187.57
3	2/28/85	38.1	20.09%	0.03%	189.01
4	3/1/85	35.7	21.00%	0.01%	190.66
5	3/4/85	37.5	20.09%	0.04%	187.40
6	3/4/85	37.9	21.00%	0.02%	188.37

Table 7.2.1 (c)

Trial	Date	Average Temp.	Average O ₂ conc.	Average CO ₂ conc.	Average Viscosity
1	2/25/85	35.2	13.37%	6.51%	190.38
2	2/26/85	31.3	15.17%	5.11%	188.62
3	2/28/85	29.2	15.32%	4.94%	187.58
4	3/1/85	36.2	13.50%	6.41%	189.98
5	3/4/85	37.0	13.62%	6.32%	190.27
6	3/4/85	38.6	13.24%	6.70%	190.69

Table 7.2.2 Experimental results which compare the calculation of a known volume with and without temperature and viscosity corrections. The errors are with respect to a volume of 560 mL (STPD) and 647 mL (ATPS). (a) The flow air is room air. (b) The flow air is room air with an elevated temperature. (c) The flow air was a mixture of approximately 6% CO₂, 14% O₂, and a balance of N₂.

Table 7.2.2 (a)

Trial	Volumes computed with the corrections (STPD)				Volumes computed without the corrections (ATPS)			
	Insp. (mL)	Insp. error	Expr. (mL)	Expr. error	Insp. (mL)	Insp. error	Expr. (mL)	Expr. error
1	560.3	-0.1%	561.8	-0.3%	647.8	-0.1%	648.5	-0.2%
2	557.9	0.4%	556.9	0.6%	642.4	0.7%	643.1	0.6%
3	562.2	-0.4%	565.7	-1.0%	656.5	-1.5%	657.6	-1.6%
4	563.1	-0.6%	565.4	-1.0%	652.1	-0.8%	653.3	-1.0%

Table 7.2.2 (b)

Trial	Volumes computed with the corrections (STPD)				Volumes computed without the corrections (ATPS)			
	Insp. (mL)	Insp. error	Expr. (mL)	Expr. error	Insp. (mL)	Insp. error	Expr. (mL)	Expr. error
1	610.8	-9.1%	625.4	-11.7%	753.2	-16.4%	756.0	-16.8%
2	568.0	-1.4%	570.8	-1.9%	672.6	-4.0%	678.3	-4.8%
3	576.0	-2.9%	588.4	-5.1%	719.0	-11.1%	727.0	-12.4%
4	577.5	-3.1%	590.7	-5.5%	722.6	-11.7%	728.3	-12.6%
5	562.1	-0.4%	565.2	-0.9%	680.0	-5.1%	686.2	-6.1%
6	568.4	-1.5%	572.6	-2.3%	675.0	-4.3%	675.4	-4.4%

Table 7.2.2 (c)

Trial	Volumes computed with the corrections (STPD)				Volumes computed without the corrections (ATPS)			
	Insp. (mL)	Insp. error	Expr. (mL)	Expr. error	Insp. (mL)	Insp. error	Expr. (mL)	Expr. error
1	655.0	-17.0%	608.1	-8.6%	805.2	-24.5%	737.0	-13.9%
2	582.8	-4.1%	570.5	-1.9%	709.0	-9.6%	686.0	-6.0%
3	581.2	-3.8%	565.6	-1.0%	685.3	-5.9%	668.0	-3.2%
4	560.2	-0.0%	565.6	-1.0%	680.4	-5.2%	670.3	-3.6%
5	570.2	-1.8%	568.0	-1.4%	669.0	-3.4%	669.5	-3.5%
6	562.9	-0.5%	561.2	-0.2%	669.9	-3.5%	668.5	-3.3%

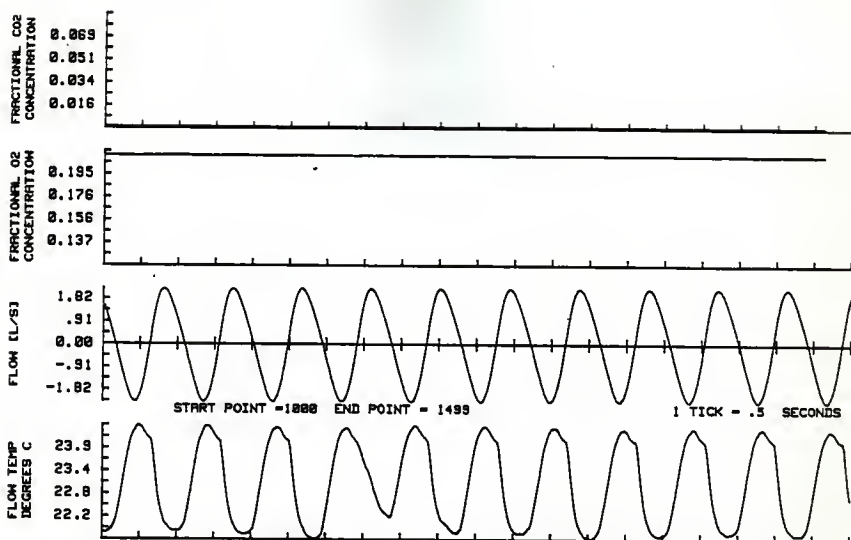


Figure 7.2.1 Typical CBRMS signals obtained from the Harvard respirator (room air cycling through the PTM).

With both method A and method B the errors generated using room air as the flow gas are minimal. With the exception of two of the error values of method B, all error values are less than or equal to 1%. This indicates that the volume calculations of both methods are accurate under flow conditions which are the same for both data collection and PTM calibration.

The errors increase when the flow gas is altered from the conditions of calibration. However, the increase is much less with method A than with method B. In all cases the error associated with method A is significantly less, 1.6% to 8.6% less with an average 4.1% less, than the error of method B. These results show that method A is better for calculating volumes where the flow gas conditions are different during data collection than during calibration, as is the case with expiratory gases.

In summary, both method A and method B provide accurate volume calculations when the flow conditions are the same during data collection as during calibration. However, once the flow conditions change from those of calibration method A provides more accurate volume calculations. This increased accuracy is due to the correction of the flow to constant conditions prior to integration. Method A provides the means for accurate calculation of volumes

under varying flow conditions.

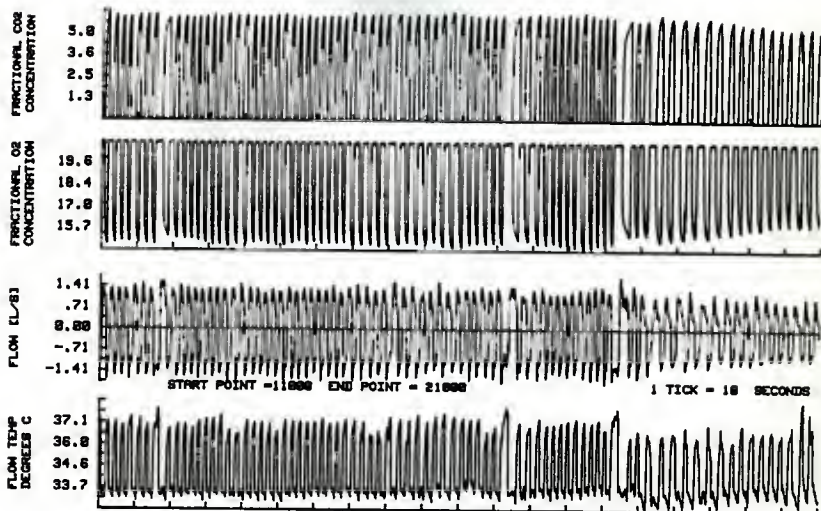
7.3 Subject Exercise Data

Two healthy male subjects performed exercise on a bicycle ergometer. The CBRMS collected data from these subjects and the results are discussed here. The features of the system are pointed out and steady-state exercise measurements discussed. The discussion is qualitative in nature as no respiratory measurements from another measurement system are available to make a quantitative comparison.

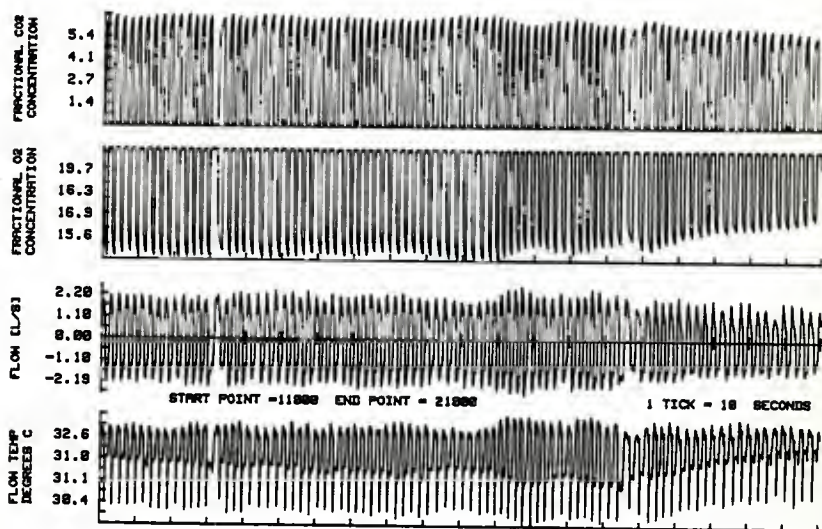
The subjects performed exercise at four work levels: (1) 50 Watts, (2) 100 Watts, (3) 125 Watts, and (4) 175 Watts. The subjects exercised at each work level four times (on different days) for a total of sixteen experiments. The first experiment at each level was to allow the subject to become accustomed to the system. The data collection regimen is outlined here (refer to the block diagram of the CBRMS, Figure 2.2.1).

1. The subject was fitted with the mask and placed on the ergometer.
2. Monitoring of the subject's heart rate began 1 minute prior to the collection of data with the Amerrec 150 belt telemetry system.
3. At the 60 second mark the CBRMS began collecting samples of the respiratory data.
4. Exercise began at the 100 second mark and continued to the 420 second mark for the 50, 100, and 125 Watt exercise levels and to the 360 second mark for the 175 Watt exercise level.
5. The CBRMS continued collecting data until the 540 second mark (a total of 8 minutes of respiratory data).
6. The heart rate was monitored to the 660 second mark.

Shown in Figures 7.3.1 thru 7.3.5 are examples of the output of the CBRMS. An example of the average output is shown in Figure 2.2.2 (page 10). Example respiratory signals for each of the work loads are shown in Figure 7.3.1. This window covers the time frame from 280 seconds to 480 seconds and includes the steady-state exercise and the off-transient exercise data.

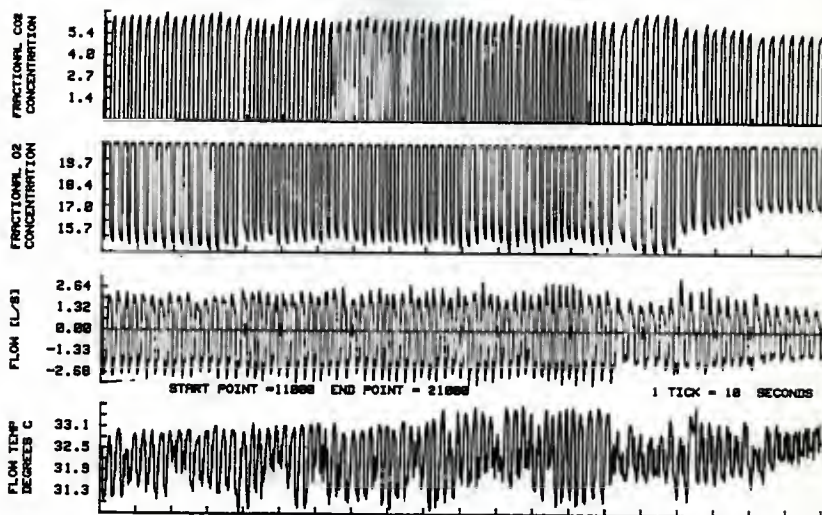


(a) 50 Watt exercise

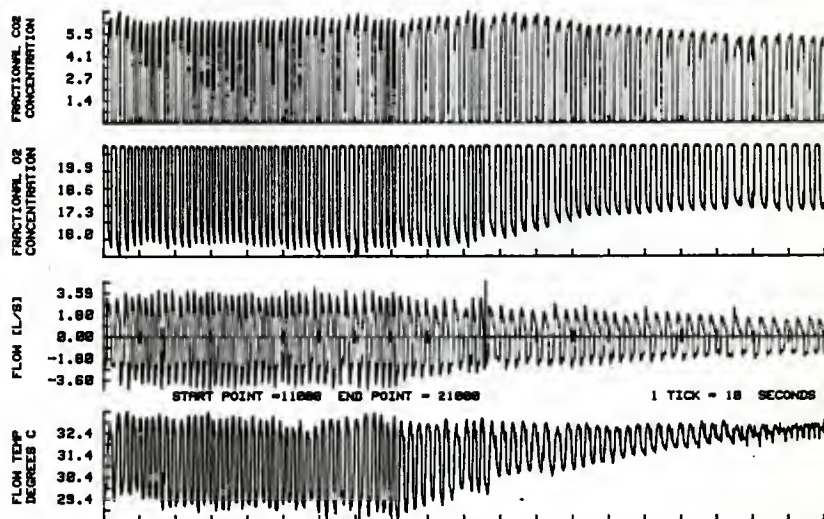


(b) 100 Watt exercise

Figure 7.3.1 Example respiratory signals.

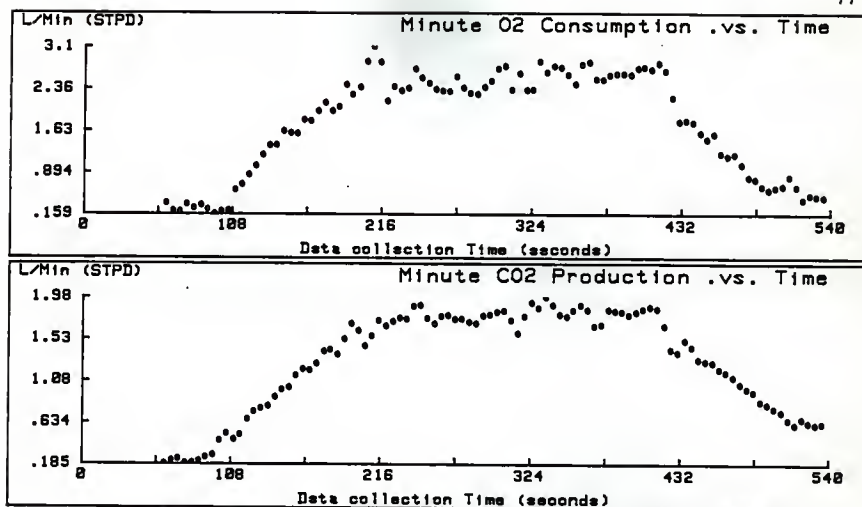


(c) 125 Watt exercise



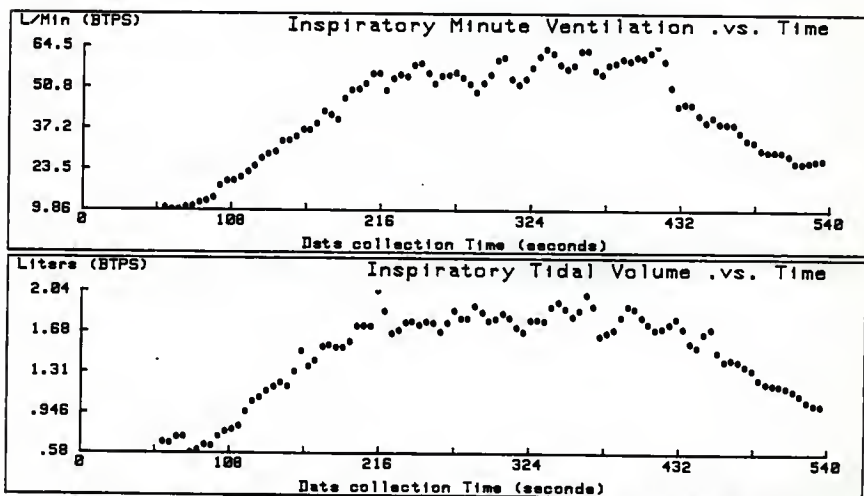
(d) 175 Watt exercise

Figure 7.3.1 (continued)



5 s Window period; 10 s Window width; Bad breaths omitted
 100 Seconds: Exercise Began
 420 Seconds: Exercise Ended

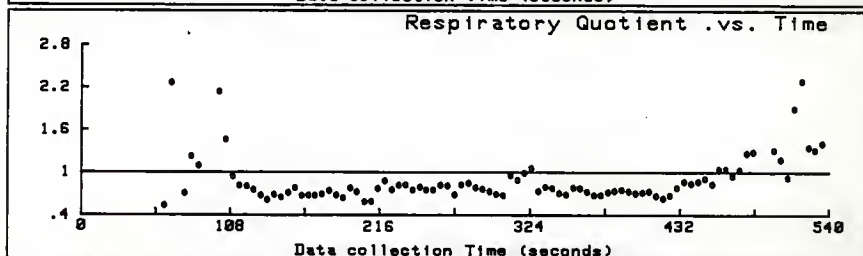
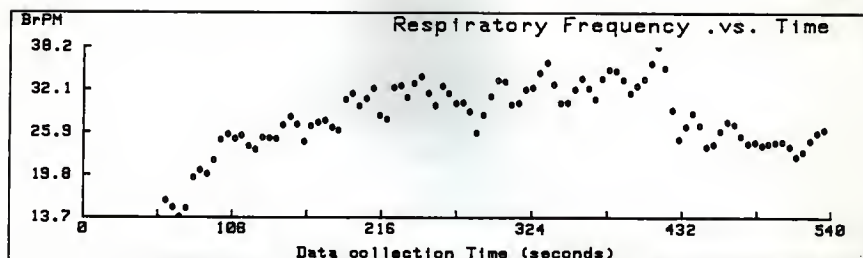
(a) Subject B; 125 Watt Exercise



5 s Window period; 10 s Window width; Bad breaths omitted
 100 Seconds: Exercise Began
 420 Seconds: Exercise Ended

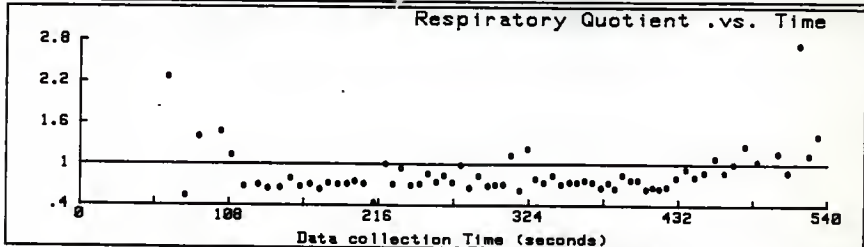
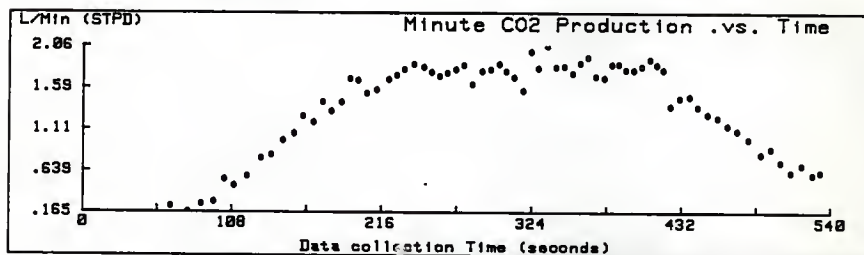
(b) Subject B; 125 Watt Exercise

Figure 7.3.2 Graphical display of the respiratory parameters.



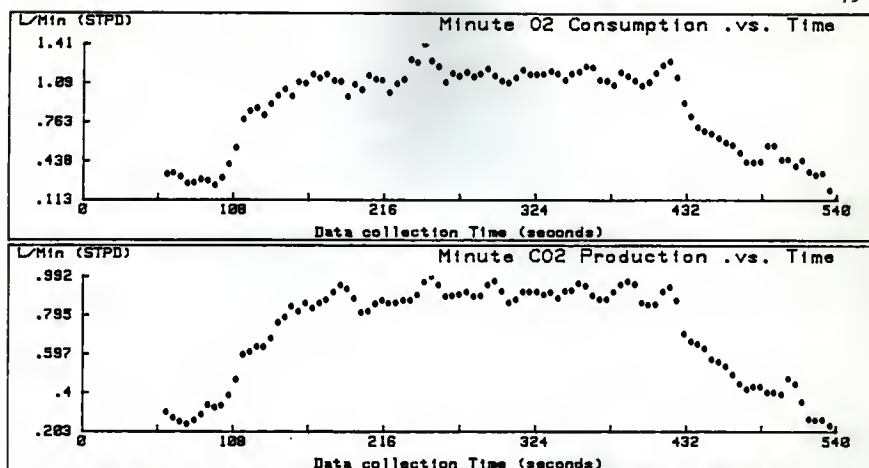
5 s Window period; 10 s Window width; Bad breaths omitted
 100 Seconds: Exercise Began
 420 Seconds: Exercise Ended

(c) Subject B; 125 Watt Exercise



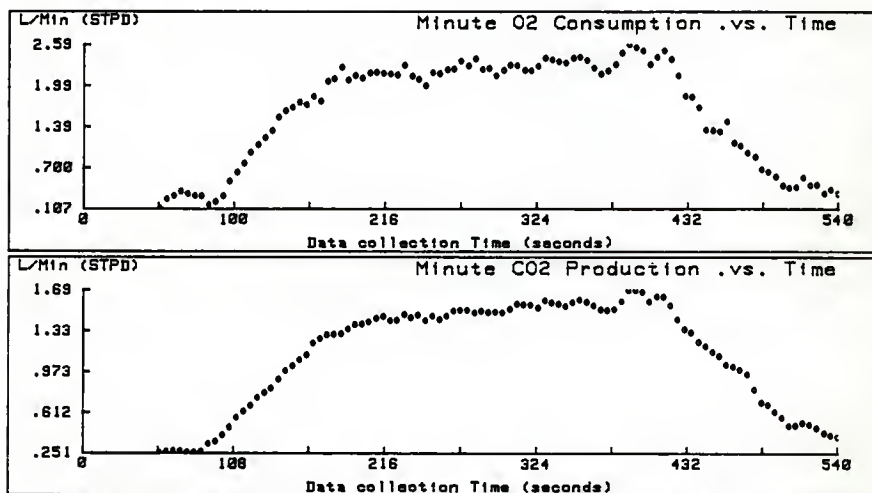
3 Breath(s)/point; Bad breaths omitted
 100 Seconds: Exercise Began
 420 Seconds: Exercise Ended

(d) Subject B; 125 Watt Exercise



5 s Window period; 15 s Window width; Bad breaths omitted
 100 Seconds: Exercise Began
 420 Seconds: Exercise Ended

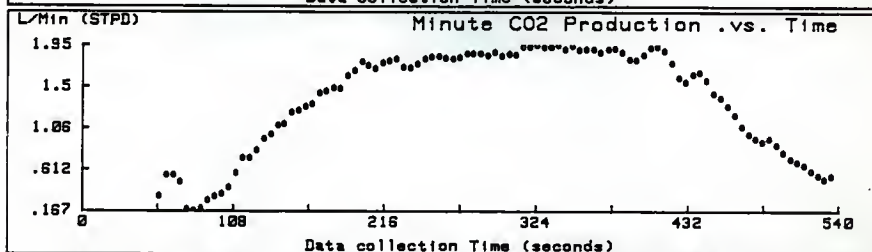
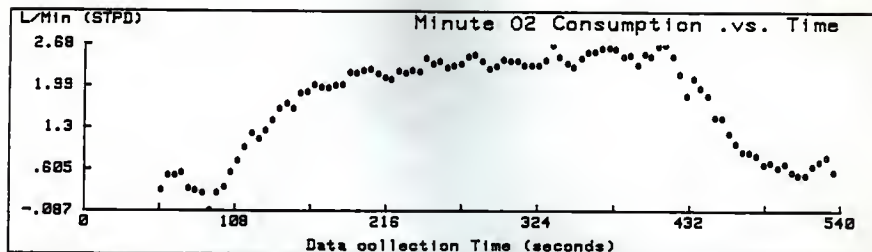
(a) Subject A; 50 Watt Exercise



5 s Window period; 15 s Window width; Bad breaths omitted
 100 Seconds: Exercise Began
 420 Seconds: Exercise Ended

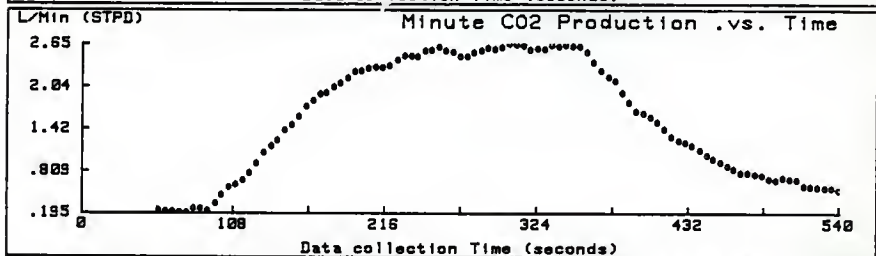
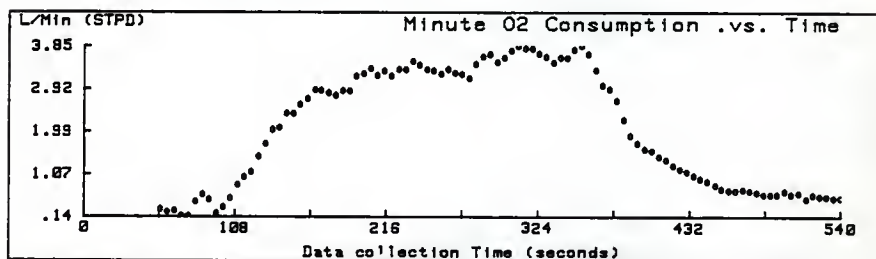
(b) Subject A; 100 Watt Exercise

Figure 7.3.3 \dot{V}_{O_2} and \dot{V}_{CO_2} responses.



5 s Window period; 15 s Window width; Bad breaths omitted
 100 Seconds: Exercise Began
 420 Seconds: Exercise Ended

(c) Subject A; 125 Watt Exercise



5 s Window period; 15 s Window width; Bad breaths omitted
 100 Seconds: Exercise Began
 360 Seconds: Exercise Ended

(d) Subject A; 175 Watt Exercise

Figure 7.3.3 (continued)

Comment: 125 Watt Exercise

Subject Identifier: Subject A

The window period is 10.0 seconds

The window width is 20.0 seconds

The starting time is 60 seconds

The ending time is 540 seconds

The breaths are combined by WINDOWING. The breaths occurring in a window 20 second(s) wide are averaged. The center of the window is moved 10 seconds between successive averages. The center of the first window is 60 seconds and the ending time is 540 seconds.

* BAD BREATHS OMITTED *

The bad breaths are not included in the averaging technique. Bad breaths are those breaths with an inspiratory volume or an expiratory volume of less than 0.4 Liters.

The R' value is equal to the averaged CO₂ produced value divided by the averaged O₂ consumed value. It is a better estimate of the true R value for the breaths averaged then the averages of the individual R values.

Time (sec)	O ₂ Consumed (L/min) (STPD)	CO ₂ Produced (L/min) (STPD)	Alveolar O ₂ Consumed (L/min) (STPD)	Alveolar CO ₂ Produced (L/min) (STPD)	Resp. Quotient	Averaged CO ₂ /O ₂ R'	Ventilation (L/min) (BTPS)	Insp. (L) (BTPS)	Exp. (L) (BTPS)	Tidal Volume (L) (BTPS)	Resp. Freq. (1/min)	Lung Vol. (L) (BTPS)
60.0	4.99	1.548	4.99	1.548	1.152	1.098	18.36	19.30	1.76	1.79	11.55	400
70.0	3.89	1.365	3.89	1.365	.927	.939	14.55	14.55	1.30	1.29	11.55	400
80.0	2.51	1.167	2.51	1.167	.766	.665	10.21	9.74	.78	.74	11.55	400
90.0	.073	1.278	.073	1.278	1.853	3.795	11.64	13.02	.72	.79	16.72	400
100.0	.284	1.416	.284	1.416	1.067	1.463	15.15	16.39	.75	.83	20.88	400
110.0	.821	1.535	.821	1.535	.930	.651	20.85	19.92	.93	.91	22.83	400
120.0	1.212	1.732	1.212	1.732	.641	.604	26.79	24.99	1.29	1.21	21.21	400
130.0	1.289	1.944	1.289	1.944	.793	.733	30.13	29.54	1.43	1.40	21.25	400
- - -												
310.0	2.406	1.843	2.406	1.843	.782	.766	53.51	49.83	2.32	2.15	23.35	400
320.0	2.404	1.927	2.404	1.927	.856	.802	56.95	53.55	2.29	2.15	22.30	400
330.0	2.358	1.936	2.358	1.936	.866	.821	57.49	54.43	2.18	2.06	22.34	400
340.0	2.475	1.925	2.475	1.925	.813	.778	57.50	53.60	2.31	2.15	25.05	400
- - -												
530.0	.783	.539	.783	.539	.799	.689	24.91	22.71	1.22	1.12	20.38	400
540.0	.546	.490	.546	.490	.897	.897	20.75	19.80	1.23	1.17	16.85	400

Figure 7.3.4 Example of the tabular output of the CBRMS using a 20 second window.

Date: NOV/02/1984

Comment: 125 Wett Exercise

Subject Identifier: Subject A

The window period is 30.0 seconds

The window width is 90.0 seconds

The starting time is 60 seconds

The ending time is 540 seconds

The breaths are combined by WINDOWING. The breathe occurring in a window 90 second(s) wide are averaged.
 The center of the window is moved 30 seconds between successive averages. The center of the first window is 60 seconds and the ending time is 540 seconds.

* BAD BREATHS OMITTED *

The bad breathe are not included in the averaging technique. Bad breathe are those breathe with an inspiratory volume or an expiratory volume of less than 0.4 Liters.

The R' value is equal to the averaged CO2 produced value divided by the averaged O2 consumed value. It is a better estimate of the true R value for the breathe averaged than the average of the individual R values.

Time (sec)	O2 Consumed (L/min) (STPD)	CO2 Produced (L/min) (STPD)	Alveolar O2 Consumed (L/min) (STPD)	Alveolar CO2 Produced (L/min) (STPD)	Resp. Quotient	Averaged CO2/O2 R'	Ventilation Insp. (L/min) (BTPS)	Ventilation Expr. (L/min) (BTPS)	Tidal Volume Insp. (L) (BTPS)	Tidal Volume Expr. (L) (BTPS)	Resp. Freq. (btr/min)	Lung Vol. (L) (BTPS)
60.0	.296	.303	.296	.303	.807	1.025	13.31	13.49	.91	.92	16.41	.400
90.0	.249	.523	.249	.523	.879	.805	19.25	19.12	1.07	1.06	18.73	.400
120.0	1.077	.784	1.077	.784	.812	.728	26.12	25.42	1.24	1.21	20.84	.400
150.0	1.625	1.684	1.625	1.684	.800	.719	35.95	34.42	1.62	1.56	22.33	.400
180.0	2.001	1.492	2.001	1.492	.757	.746	44.77	42.51	1.92	1.81	23.74	.400
210.0	2.189	1.672	2.189	1.672	.771	.764	49.51	46.61	2.06	1.94	24.39	.400
240.0	2.304	1.789	2.304	1.789	.786	.776	53.26	49.93	2.11	1.98	25.53	.400
270.0	2.340	1.810	2.340	1.810	.784	.773	53.40	49.89	2.14	2.00	25.18	.400
300.0	2.389	1.873	2.389	1.873	.811	.784	55.54	52.93	2.16	2.04	25.64	.400
330.0	2.436	1.894	2.436	1.894	.805	.777	56.51	52.93	2.22	2.08	26.78	.400
360.0	2.488	1.893	2.488	1.893	.796	.761	57.42	52.98	2.17	2.02	26.78	.400
390.0	2.466	1.833	2.466	1.833	.769	.743	56.27	52.98	2.15	2.00	26.36	.400
420.0	2.207	1.714	2.207	1.714	.830	.777	53.50	49.57	2.12	1.98	25.42	.400
450.0	1.640	1.424	1.640	1.424	1.003	.868	45.23	43.26	2.01	1.91	22.90	.400
480.0	1.011	1.067	1.011	1.067	1.216	1.055	36.98	35.21	1.70	1.65	22.08	.400
510.0	.700	.797	.700	.797	1.271	1.138	20.29	23.31	1.45	1.41	21.24	.400
540.0	.596	.643	.596	.643	1.248	1.080	26.36	26.19	1.24	1.21	21.77	.400

Figure 7.3.5 Example of the tubular output of the CBRMS using a 90 second window.

Shown in Figure 7.3.2 are graphical displays of several respiratory parameters. The first three figures show the window averaging technique and the final figure shows the averaging of three consecutive breaths. In all cases the 'Bad breaths', breaths having an inspiratory or an expiratory tidal volume of less than 0.4 L, have been omitted in the averaging technique. Typical \dot{V}_{O_2} and \dot{V}_{CO_2} responses are shown in Figure 7.3.3 for the four exercise levels. The window averaging technique was used.

Tabular outputs using window averaging are shown in Figures 7.3.4 and 7.3.5. The alveolar O_2 consumption, CO_2 production, and lung volume parameters in these figures are equal to the corresponding values measured at the mouth. These parameters contain no additional information but have been built into the display for future expansion [12].

The average results from a window of steady-state data (90 second window centered about 330 seconds) are shown in Table 7.3.1 and Figures 7.3.6 thru 7.3.10. These average values do not emphasize the most important advantage of the CBRMS over the expired gas collection technique, the ability to monitor transient respiratory responses. However, these values do allow comparison to those of other researchers and to those obtained using the expired collection technique.

The direct comparison of these data to the data from expired gas collection technique is not possible as such data were not collected from the subjects. However, the average ventilation values (\dot{V}_{O_2} , \dot{V}_{CO_2} , and \dot{V}) agree favorably to the values published by other researchers [6,13,14].

Table 7.3.1 Average respiratory parameters. Refer to the text for an explanation of these low respiratory quotient values and the difference between the inspiratory and expiratory ventilation.

(a) Subject A

Work Load (W)	O_2 Cons. (L/min) (STPD)	CO_2 Prod. (L/min) (STPD)	Resp. Quot.	Insp. Vent. (L/min) (BTSP)	Expr. Vent. (L/min) (BTSP)	Insp. Tid. Vol. (L) (BTSP)	Expr. Tid. Vol. (L) (BTSP)
50.0	1.16	0.93	0.80	32.2	31.0	1.37	1.32
50.0	1.16	0.91	0.78	31.7	30.5	1.21	1.16
50.0	1.12	0.85	0.76	30.2	28.9	1.26	1.2
100.0	2.01	1.57	0.78	47.4	44.8	1.97	1.87
100.0	2.06	1.41	0.68	48.4	45.0	1.57	1.46
100.0	2.27	1.35	0.68	47.5	43.2	1.79	1.63
125.0	2.43	1.88	0.77	55.0	51.4	2.33	2.18
125.0	2.44	1.89	0.78	56.5	52.8	2.22	2.08
125.0	2.71	1.84	0.68	57.6	52.6	1.91	1.74
175.0	3.64	2.67	0.73	88.4	80.6	2.53	2.32
175.0	3.84	2.85	0.74	93.6	85.6	2.64	2.42
175.0	3.62	2.56	0.71	78.8	71.3	2.63	2.38

Table 7.3.1 (b) Subject B

Work Load (W)	O ₂ Cons. (L/min) (STPD)	CO ₂ Prod. (L/min) (STPD)	Resp. Quot.	Insp. Vent. (L/min) (BTPS)	Expr. Vent. (L/min) (BTPS)	Insp. Tid. Vol. (L) (BTPS)	Expr. Tid. Vol. (L) (BTPS)
50.0	1.15	0.83	0.72	28.5	27.6	1.1	1.07
50.0	1.09	0.80	0.74	28.3	27.3	1.03	1
50.0	1.11	0.80	0.72	28.2	27.1	1.11	1.06
100.0	2.09	1.45	0.69	45.1	41.5	1.54	1.41
100.0	2.46	1.53	0.63	48.0	42.5	1.63	1.44
100.0	1.86	1.43	0.77	43.1	40.7	1.56	1.45
125.0	2.45	1.86	0.76	55.0	50.8	1.73	1.61
125.0	2.64	1.98	0.75	58.6	53.8	1.72	1.58
125.0	2.59	1.80	0.70	57.6	52.3	1.83	1.66
175.0	4.60	2.77	0.60	98.2	84.1	2.31	1.98
175.0	4.23	2.74	0.65	98.2	86.7	2.24	1.98
175.0	4.38	2.34	0.54	99.1	85.0	2.21	1.9

Of particular concern is the difference between the inspiratory volume and expiratory volume at the higher work levels. The inspiratory values are from 6% to 14% larger than the expiratory values. This is obviously not physically possible. The inspiratory and expiratory values should be nearly equal. These large errors lead to the possibility of the inspired O₂ being overestimated with respect to the expired O₂ causing the volume of O₂ exchanged to be overestimated. Also, the volume of CO₂ expired is possibly underestimated which would cause the volume of CO₂ exchanged to be underestimated. These two errors combined can cause the respiratory quotient, R, to be significantly underestimated. This is apparently the case as the R values should be nearly equal to unity.

The cause of this error can be attributed to the nonlinearity of the PTM differential pressure versus flow. While it was shown that the CBRMS could accurately calculate volumes from the PTM differential pressure, dependency of these calculations flow was not investigated. The flow rates of the subjects at the higher work loads are significantly higher than the flow rates generated by the Harvard respirator. This is apparent by comparing the flow signal of Figure 7.2.1 to those of Figure 7.3.1.

The ability of the Fleisch #2 PTM to be linear at the higher flow rates is suspect. In addition, the particular PTM used in this study had a defect in the screen, possibly causing additional nonlinearities. To correct this problem other PTMs should be investigated. Also the flow rate produced by the Harvard respirator should be increased by increasing the stroke volume.

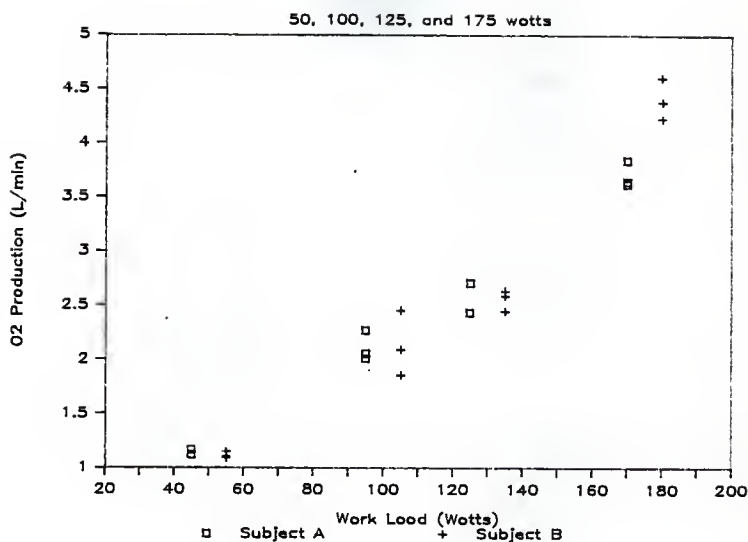


Figure 7.3.6 \dot{V}_{O_2} versus work load

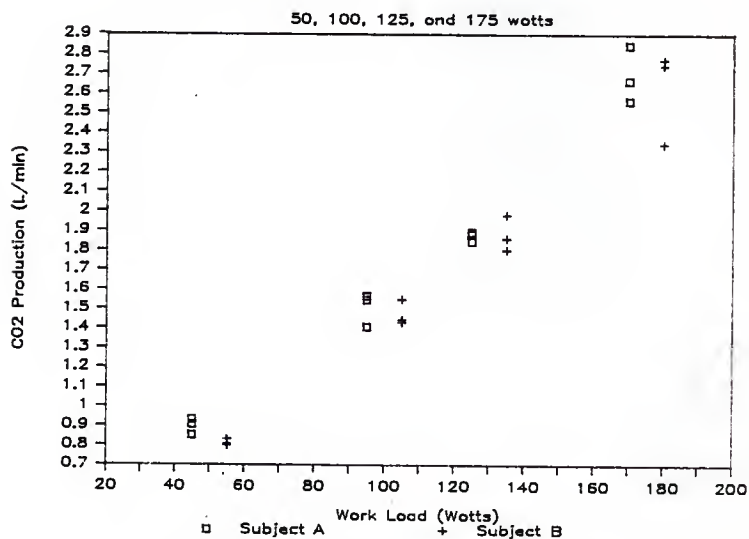


Figure 7.3.7 \dot{V}_{CO_2} versus work load

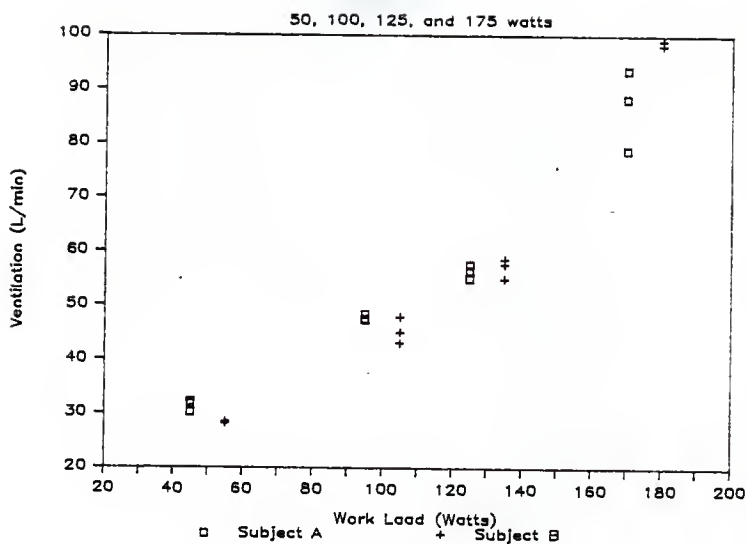


Figure 7.3.8 \dot{V}_I versus work load

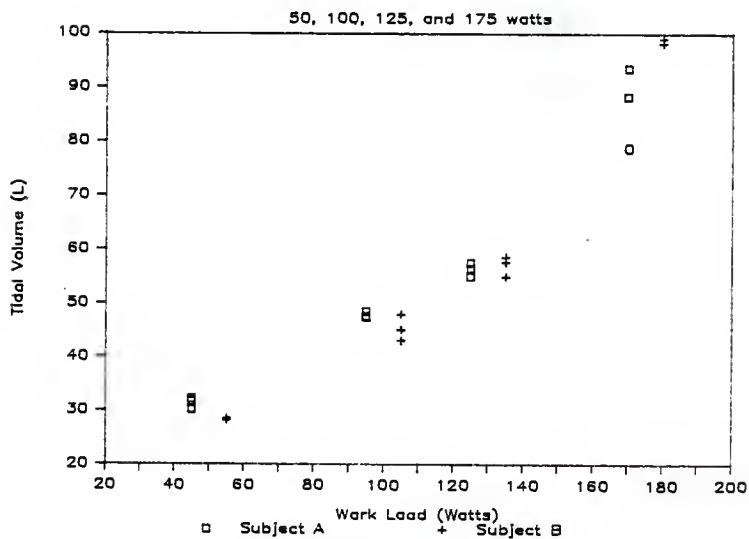


Figure 7.3.9 V_{TI} versus work load

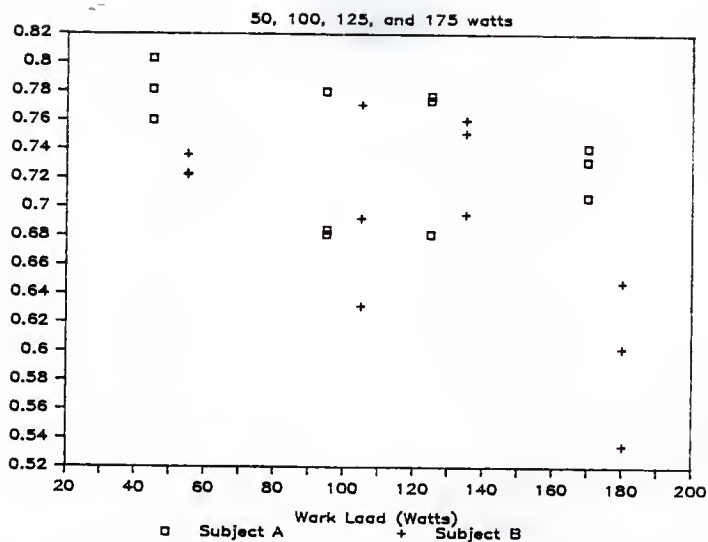


Figure 7.3.10 Respiratory Quotient, R , versus work load. Refer to the text for an explanation of these low respiratory quotient values.

Chapter VIII. CONCLUSIONS

Through the enhancement of the CBRMS first developed by Creel [4] and modified by Riblett [13] with a temperature and viscosity corrected flow and additional data display methods, the following conclusions have been reached.

1. A flow signal under STPD conditions can be computed from a PTM differential pressure signal, temperature signal, and fractional composition signals. The flow signal is calculated via Poiseuille's law from the measured signals and the appropriate assumptions. This flow signal can be converted to STPD conditions using the respiratory temperature signal and calculation of the water vapor content. The accuracy of volume calculations made with this flow signal are increased over those made assuming the flow directly proportional to the PTM differential pressure signal.
2. A temperature transducer based on 0.001 inch diameter thermocouple can be designed to produce a temperature signal with sufficient accuracy to be used in the calculation of STPD respiratory flow. The response time of this transducer is sufficient to monitor the respiratory flow temperature.
3. A limiting factor in the every day usefulness of the CBRMS is the relatively large amount of time required to compute the respiratory parameters from the recorded respiratory signals. This has been reduced with the addition of the averaging techniques so that the entire set of data need be analyzed one time only. From this analysis the response for windows of a specified time width for the entire run may be quickly attained. However, once new data have been read in or the computer has been turned off the breath-by-breath respiratory parameters are lost. Therefore, additional display of the results is not possible without the re-analysis of the data. The reduction of this problem is discussed in the Chapter IX, Suggested Areas for Future Development.
4. The addition of the breath averaging techniques and the display of the results enhances the ability of the researcher to quickly investigate transient responses. By increasing the size of the window steady-state responses may also be investigated without the time consuming task of re-analyzing the data.
5. The respiratory parameter calculations require accurate transducers.

The calculations are especially sensitive to errors in the flow signal. Possible errors in the flow are reduced with the addition of temperature and viscosity corrections. However, essential to these calculations is the attainment of a valid differential pressure signal. The linear relationship between the differential pressure and the flow (under constant flow gas conditions) for the particular Fleisch #2 PTM used in this study is suspect at the higher flow rates.

6. The application of structured programming techniques to the CBRMS programs enhances the readability and maintainability of the code. Structured programming allows large programs to be broken into functional units. This division of functions allows individual problems to be placed within one program block (procedure or subroutine).

Chapter IX. SUGGESTED AREAS FOR FUTURE DEVELOPMENT

The present CBRMS is a very usefml tool in assessing respiratory function bnt there are several additional improvements which would extend the system capabilities and rednce the time needed to obtain the analyzed results. The following improvements, most of which are software oriented, would enhance the system further and extend the ability of the researcher or clinician to interpret the results.

9.1 System Improvements

1. Apply the improvements of the Basic 2.0 Language Extensions. These extensions to the Basic 2.0 language (the language currently used by the Basic routines) provide a large number of additional commands. These improvements allow for snch things as snpport of the real time clock which would allow dates and times to be printed on all hard copy outpnt, vaatly improved editing featnres, the ability to send inpnt and outpnt through an internal memory bnffer (more on this improvement will be discssed in number 3), and many other featnres.
2. Obtain the CSUB (Compiled SUBroutine) preparation utility from Hewlett-Packard (part number 09800-10640). The preparation ntility allows snbroutines written in Pascal to be called from Basic. The CSUB snbroutines appear the same to the calling Basic routine as the standard SUB snbroutines. This featnre would allow Pascal programs to be called from Basic and the passing of parameters between Basic and Pascal. This would conceivably eliminate the time consuming problem of converting the ASCII format data collected with the Pascal system to the numeric format of the Basic system. In addition, the time consuming iterative portions of the Basic programs could be converted to the mnch faster Pascal snbroutines.

A prime example is the compntation of the breath-by-breath binary volumes. The compntation of the flow calibration factors involves integrating 4000 samples of flow and requires approximately 35 seconds to execnte. The same amount of data naing the Basic ANALYSIS program (the integration loops in the two programs are nearly identical) requires 100 seconds to execnte.

This featnre is briefly discssed in the Basic Language Reference manual [23] (under the CSUB command) bnt the potential is very evident. This featnre would allow the best of the two operating systems to be used; the

user and programmer friendliness of the Basic system and the speed and versatility of the Pascal system.

3. Upgrade the DECwriter II printer. There is an upgrade kit available for the DECwriter II which would increase the printing speed, increase the band rate, and provide a print buffer. However, other possibilities exist for reducing the time the computer is tied up with the printing of output. A print buffer could be designed and built or the TRANSFER buffer command available with the Basic 2.0 Language Extensions package could be used.

While the printer buffer would not increase the speed of the printer it could greatly reduce the amount of time the computer is tied up sending information to the printer. By increasing the band rate that the computer sends information to the DECwriter the computer would be tied up less and the operator could continue with other sections of the ANALYSIS program while the results are being printed. The buffer should also have the ability to simulate form feeds and skip over the perforations of the computer paper (accomplished by keeping track of the number of lines printed on the page) and a number of other useful characteristics available on more modern printers. The article by Bono, Build a Printer Buffer [3], should be referred to as a good starting point for the design and construction of such a buffer.

The Extensions package simulates the use of a printer buffer (allowing the computer to continue other operations while the relatively slow I/O operations occur simultaneously) with the TRANSFER command. The TRANSFER command provides the means for a variety of input/output operations to occur simultaneously with program execution. The Basic Interfacing Techniques reference [22] is a good guide for the use of the TRANSFER command. This command can also be applied to other I/O operations, such as reading and writing data files.

4. Purchase commercially available thermocouple assemblies. Omega Engineering Incorporated [24] has thermocouple probe assemblies available with the sensing junction exposed. These probes would be more mechanically rigorous.
5. Conduct studies on thermocouples of larger diameter to determine if the larger thermocouple has a fast enough response time to monitor the respi-

ratory temperature signal. The larger size would provide the obvious advantage of possessing a more rugged temperature probe. As pointed out in the conclusions of Chapter III, the sensitivity of the computed flow to small errors in temperature is very small. This would indicate that slower responding temperature sensors would not have a great detrimental effect on the calculation of the STPD flow.

6. Use a linear relationship between the sampled data and the temperature. The type E thermocouple has nearly a linear voltage-temperature relationship. The small errors in using a linear fit would not significantly effect the calculation of the STPD flow. Possibly more error is introduced by using three calibration points rather than two.

9.2 Storage and Extended Analysis of the Breath-by-Breath Results

This extension has been separated from the other system improvements because of the importance of being able to quickly and systematically analyze the breath-by-breath results of various subjects or various exercise levels. The goal of this improvement is to be able to obtain the average response of a subject, or a number of subjects, to a given exercise regimen. The foreseen steps to building a package to analyze sets of the breath-by-breath data are outlined below.

1. Alter the Display_results subroutine of the ANALYSIS program to store the breath-by-breath values, \dot{V}_{O_2} , \dot{V}_{CO_2} , \dot{V}_I , etc., which are stored in the two dimensional array Resp_var, (construction of the Resp_var array is discussed in Appendix VI, Section A6.5). This could be done by adding a 'Store Respiratory variables' option to the 'Plot Values' and 'Print Values' menu. This would allow many operations to be performed on the breath-by-breath results without the time consuming need to analyze the respiratory data every time. Care should be taken in defining a standard format for storing these breath-by-breath data!
2. Develop a routine which will average the average values obtained with the window averaging routine from several exercise runs or subjects (using data obtained from the same exercise regimens). This would allow average response and the standard deviation for a specific point in time. Note that the statistics of this technique may become a complex problem (or remain trivial) as different subjects may have a different number of breaths in a given window. This would give the two averaged values

different statistical significance. However, if the subjects have nearly identical respiratory frequencies and the window is wide enough this should not be a problem.

Shown in Figure 9.2.1 is a flowchart that could be used to implement this idea. One approach for storing the respiratory variables is to use an array similar to the respiratory variable array (Resp_var) described in Appendix VI, Section A6.5. However, the array would contain a third dimension representing the subject in addition to the two dimensions discussed; breath number and respiratory variable. The current window averaging routine could be used to accomplish the window averaging of a window of data. Slight modifications would be needed to handle the additional dimension.

Other operations could be substituted for the averaging of several subjects' values for a window in time. Such things as plotting the average value obtained from a window and the average value obtained from the same window of another run would allow a comparison of the response of two (or more) runs. Care should be taken and good program development techniques should be followed in the design of this routine so that future modifications can be easily implemented!

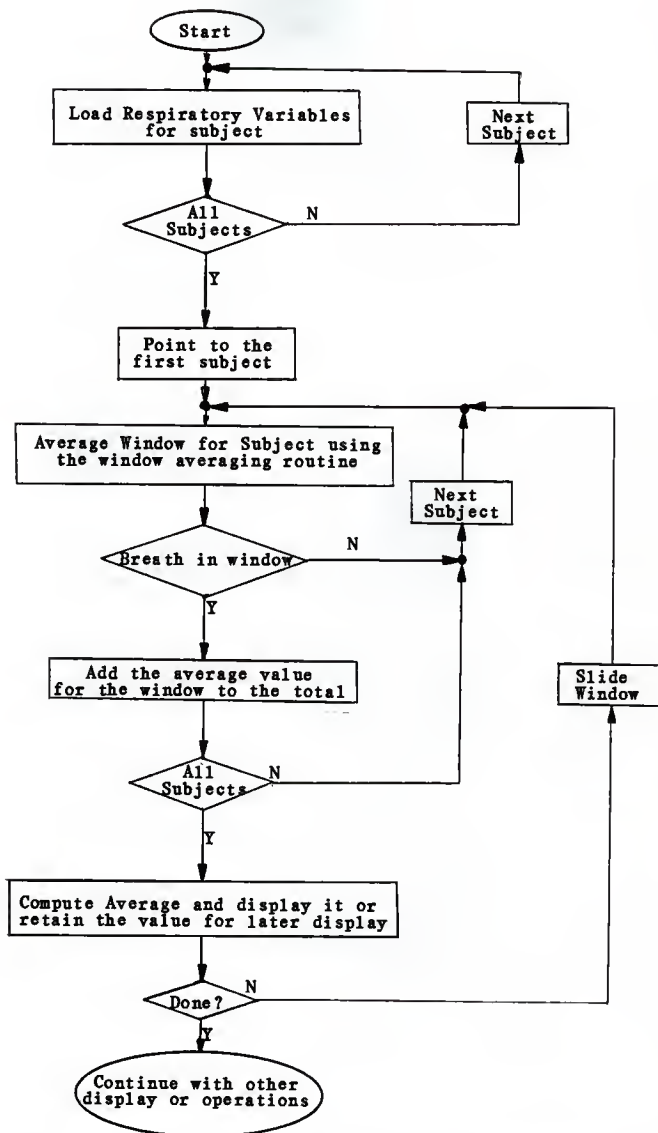


Figure 9.2.1 Flowchart for averaging the breath-by-breath results from several subjects or different runs of the same subject.

Chapter X. BIBLIOGRAPHY

1. Agnew, Jeanne and R.C. Knapp, Linear Algebra with Applications, Wadsworth Publishing Company, 1978
2. Beaver, William L., N. Lamarra, and K. Wasserman, Breath-by-breath measurement of true alveolar gas exchange, J. Appl. Physiol.: Respirat. Environ. Exercise Physiol., 51(6):1662-1675, 1981
3. Bono, John, Build a Printer Buffer, BYTE, 9(6):142, 1984
4. Creel, Earl E., Measurement of Breath-by-Breath Oxygen Consumption and Carbon Dioxide Production in Exercising Calves, Master's Thesis, Kansas State University, 1982
5. Gateno, Leon W., Design of a Versatile, Multi-Channelled, Data Acquisition Module, Master's Thesis, Kansas State University, 1980
6. Guyton, Arthur C., Textbook of Medical Physiology, sixth edition, W.B. Saunders Company, 1981
7. Horowitz, Paul, and W. Hill, The Art of Electronics, Cambridge University Press, 1980
8. Johns, D.P., J.J. Pretto, and J.A. Stretton, Measurement of gas viscosity with a Fleisch pneumotachograph, J. Appl. Physiol.: Respirat. Environ. Exercise Physiol., 53(1):290-293, 1977
9. Kestin, J., H.E. Khalifa, S.T. Ro, and W.A. Wakeham, The viscosity and diffusion coefficients of eighteen binary gaseous systems, Physica 88A: 242-260, 1977
10. Kestin, J., R. Dippio, Viscosity of Gases, Amer. Inst. of Phys. Handbook, Third edition, 2.232-2.248, McGraw-Hill Book Co, 1972
11. Minken, P. Yeh, R.M. Gardner, T.D. Adams, and F.F. Yanowitz, Computerized determination of pneumotachometer characteristics using a calibrated syringe, J. Appl. Physiol.: Respirat. Environ. Exercise Physiol., 53(1):280-285, 1982
12. Pieschl, Rick, The Application of FRC Corrections to Respiratory Gas Volumes Calculated Using Breath-by-breath Techniques, Personal Communication, 1984
13. Riblett, Loren E., A Computer-Based Instrumentation System for Measurement of Breath-by-Breath Oxygen Consumption and Carbon Dioxide Production in Exercising Humans, Master's Thesis, Kansas State University, 1984
14. Ruppell, Greg, Manual of Pulmonary Function Testing, second edition, The C.V. Mosby Co, 1979
15. Schneider, G. Michael, S.W. Weingart, D.M. Perlman, An Introduction to Programming and Problem Solving with Pascal, second edition, John Wiley and Sons, 1982

16. Sprick, Mark, Universal Plotting Routine, Personal Communication, 1984
17. Sue, Darryl Y., Personal Communication, 1981
18. Swanson, George D., I.E. Sodal, J.T. Reeves, Sensitivity of Breath-to-Breath Gas Exchange Measurements to Expiratory Flow Errors, IEEE Trans. Biomed. Eng., Vol. BME-28, No.11, 1984
19. Turney, S.Z., W. Blumenfeld, Heated Fleisch pneumotachometer: a calibration procedure, J. Appl. Physiol., 34(1):117-121, 1973
20. Wilke, C.R., A Viscosity Equation for Gas Mixtures, J. of Chem. Phys, 18:517-519, 1950
21. Application Note: How to Test Basic Operational Amplifier Parameters, Data Acquisition Data Book 1982, Analog Devices, 1982
22. Advanced Transfer Techniques. BASIC Interfacing Techniques with Extensions 2.0, Hewlett-Packard Co., 1982
23. BASIC Language Reference with Extensions 2.0, Hewlett-Packard Co., 1983
24. Temperature Measurement Handbook and Encyclopedia, Omega Engineering Incorporated, 1984

XI. ACKNOWLEDGMENTS

Without the support and help of a great number of people my education culminating in this thesis would not have been possible. I would like to thank my committee members Dr. Michael S. P. Lucas and Dr. Howard H. Erickson for their help and suggestions. A special thanks goes to my Major Professor Dr. Richard Gallagher for his support, guidance, and friendship. I would like to thank the Department of Electrical and Computer Engineering and the Department of Anatomy and Physiology for supplying financial support during my research.

A special thank you to Earl Creel. Thank you Mr. Creel for instilling in me the burning desire for the quest of knowledge through the applied sciences. You will never be forgotten.

To my parents, without you my education would not have been possible, thank you for everything; your love, your prayers, your patience, your example, and your inspiration.

This work is dedicated to my nieces and nephews, may their smiles last forever.

APPENDIX I. DEFINITION OF ACRONYMS

The acronyms used throughout this thesis are defined within this appendix.

ATPS	- Ambient Temperature and Pressnre; Saturated
BTPS	- Body Temperature and Pressure; Satnrated
CBRMS	- Compnter Based Respiratory Measurement System
DAM	- Data Acqnisation Module
F_x	- Frsctional concentration of gas x
GMS	- Gas Mass Spectrometer
ITP	- Instantaneons Temperatnre and Pressnre
$K(P_b, F_{H_2O}, T)$	- ITP to STPD conversion factor
PTG	- Pneumotachograph
PTM	- Pneumotachometer
P_b	- Bsrometric pressure
P_x	- Psrtial pressnre of gas x
STPD	- Standard Temperature and Pressnre; Dry
T	- Temperature or sampling period
T_j	- Sensing junction tempersture
T_{ref}	- Reference junction temperature
V	- Volume
V_{TC}	- Thermocouple voltage
V_{TE}	- Expiratory tidal volume
V_{TI}	- Inspiratory tidal volume
\dot{V}	- Flow rate
\dot{V}_{CO_2}	- CO_2 production rate
V_E	- Expiratory ventilation
\dot{V}_I	- Inspiratory ventilation
\dot{V}_{O_2}	- O_2 consumption rate
μ	- Viscosity
μ_r	- Relative viscosity
μ_x	- Viscosity of gas x
ΔP	- Differential pressnre

APPENDIX II. PRINCIPLES OF OPERATION OF THE
PERKIN-ELMER 1100 MEDICAL GAS ANALYZER

The Gas Mass Spectrometer used in these experiments is the Perkin-Elmer 1100 Medical Gas Analyzer. This GMS has a rapid response time and is configured to measure the percentage concentration of O_2 , CO_2 , and N_2 ; two features which make it ideal for monitoring normal respiratory gases. The principles of operation are explained very well in the Perkin-Elmer manual. A brief description of the GMS's signal processing circuitry is given in this appendix.

The Perkin-Elmer 1100 is a magnetic sector type of GMS. A magnetic sector GMS introduces a small sample of gas to an electron beam which causes a fraction of the gas molecules to lose one or more electrons and become positively charged ions. The ions are acted upon by a magnetic field at right angles to the direction of ion travel. This causes the ions of the various gases to bend in a circular arc with a radius proportional to their mass, thereby separating the ions. The individual ions then collide with individually located collectors. The collectors produce outputs that are proportional to the number of ions hitting them and therefore, proportional to the concentrations of the particular gases in the air sample.

A functional block diagram of the signal amplifiers is shown in Figure A2.1. The outputs of the collector circuits are applied to the calibration network. The calibration network adjusts the gain of the individual channels and cancels the interference between gases which occurs when a portion of one gas excites the collector of another gas. The calibration network outputs enter automatic gain amplifiers (AGC) with outputs connected to a summing junction. Also connected to the summing junction are two fixed signals which are set by the operator using external potentiometers. The fixed signals are the fractional content of the various gases in room air whose concentration remains a constant, and the fractional content of water vapor. The fractional content of water vapor switches between to set values, the fractional content of the inspirate gas and the fractional content of the expirate gas. The switching is triggered by the F_{CO_2} signal.

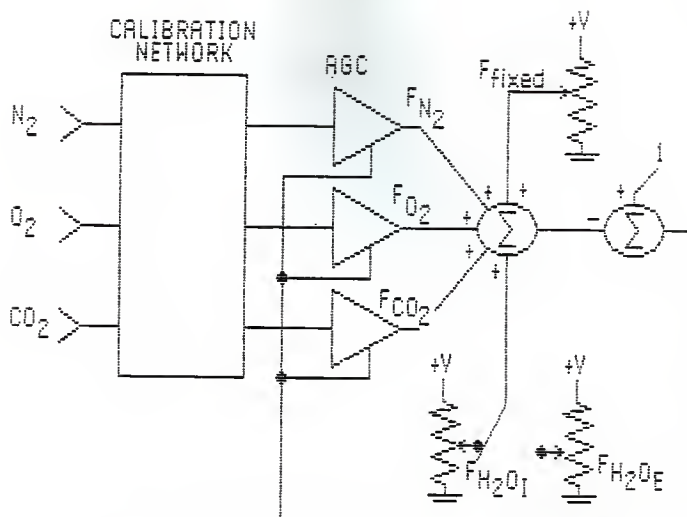


Figure A2.1 The AGC block diagram of the GMS.

The output of the summing junction is compared with the value of unity creating an error value. This error value controls equally the gain of the AGC blocks forcing the error value to zero. The output of the summing block is

$$F_{wN_2} + F_{wCO_2} + F_{wO_2} + F_{wH_2O(I)(E)} + F_{fixed} = 1 \quad A2.1$$

where F_{w_x} denotes the concentration of gas x in the wet gas (gas containing water vapor). Of particular interest is the fractional content of the various gases neglecting the volume of water in the gas, the dry gas concentrations. This can be found by dividing the volume of gas x by the volume of the gas without any water vapor, the dry gas volume. The volume of the dry gas is the total volume of the wet gas minus the volume of water vapor in the gas,

$$V_d = V_w - F_{wH_2O} V_w = V_w(1 - F_{wH_2O})$$

so that the dry fractional content of gas x is

$$F_x = \frac{V_{w_x}}{V_d} = \frac{F_{w_x} V_w}{V_w(1 - F_{wH_2O})} = \frac{F_{w_x}}{(1 - F_{wH_2O})}$$

$$F_x = \frac{F_{w_x}}{(1 - F_{w_{H_2O}})}$$

where

F_x - fractional content of gas x in the dry gas

F_{w_x} - fractional content of gas x in the wet gas

V_{w_x} - volume of gas x in the wet gas

V_w - volume the wet gas

V_d - volume the dry gas.

The GMS can be made to read directly the dry concentrations by adjusting the fractional water vapor content potentiometers to zero. This causes the gain on the various channels to increase (all gains increase the same amount) until the error value is zero. This gain increases by the factor $1/(1 - F_{H_2O})$ so that the outputs are equal to the dry gas concentrations. The wet gas concentrations may then be found from the inverse of Equation A2.2.

With the water vapor potentiometers set to zero it is necessary to only measure the outputs of two channels to obtain the value of all three, since the individual outputs are forced to sum to one. For instance, the F_{N_2} value may be found by measuring the F_{O_2} and F_{CO_2} values.

$$F_{N_2} = 1 - F_{O_2} - F_{CO_2} - F_{fixed}$$

Assuming the fixed value is approximately zero,

$$F_{N_2} = 1 - F_{O_2} - F_{CO_2}.$$

With the current studies the GMS is adjusted to read the dry fractional content values. The fractional content of nitrogen is found from the above equation and the fractional content of water vapor is found by other means, namely the temperature signal and ambient conditions.

APPENDIX III. DERIVATION OF THE RESPIRATORY PARAMETER CALCULATIONS

A derivation of the gas volume calculations is presented here. The calculations are based on the dry fractional concentration signals of oxygen and carbon dioxide, the flow temperature signal, and the PTM differential pressure signal.

The first step in calculating the breath-by-breath volumes is to convert the instantaneous differential pressure obtained from the PTM to the instantaneous flow. This conversion is accomplished with Poiseuille's law which describes laminar flow through a tube. The PTM can be modeled as a single tube so that Poiseuille's law holds. The law is stated thus:

$$\dot{V} = \frac{\Delta P}{R} \cdot \frac{k}{100 \text{ (L/cm}^3\text{)}} \quad \text{A3.1}$$

where

\dot{V} = flow through the tube (L/s)

ΔP = pressure difference between one end of the tube and the other end (torr)

R = effective resistance of the PTM (dyne-sec/cm⁵(10⁻⁶))

k = 7.5062 (10⁻⁶) ((dyne/cm²)/torr)

The resistance is given by:

$$R = \frac{\mu l}{\pi r^4} \quad \text{A3.2}$$

where

μ = viscosity of the gas (μP)

l = effective length of the PTM (cm)

r = effective radius of the PTM (cm)

The effective PTM length and the radius are considered constant and the gas viscosity is determined from the gas composition signals, the temperature signals, and the ambient conditions [19]. The linear approximations for the viscosity of individual gases over the respiratory temperature range are shown in Table A3.1. Wilke's equation can be used to calculate the overall viscosity of mixtures of these gases [8,9,20]. The general form of Wilke's equation is given by:

$$\mu_g = \sum_{i=1}^4 \frac{Fw_i \cdot \mu_i(T)}{\sum_{j=1}^4 Fw_j \cdot \beta_{ij}} \quad \text{A3.3}$$

where β_{ij} is a dimensionless constant defined by Wilke [20] as

$$\beta_{ij} = \frac{[1 + (\mu_i/\mu_j)^{1/2}(M_i/M_j)^{1/4}]^2}{[8 \cdot (1 + M_i/M_j)]^{1/2}} \quad A3.4$$

and

- μ_g - the overall gas viscosity (μP)
- $\mu_{i(j)}$ - the viscosity of gas $i(j)$ (μP) at the temperature T
- $F_{wi(j)}$ - the fractional concentration of gas $i(j)$ in the wet gas
- $M_{i(j)}$ - the molecular weight of gas $i(j)$.

Table A3.1. Linear approximation of pure gas viscosities between 20°C-40°C

μ_{N_2}	= 166.6 + 0.454 T	[10]
μ_{O_2}	= 191.0 + 0.616 T	[10]
μ_{CO_2}	= 137.6 + 0.450 T	[10]
μ_{H_2O}	= 132.6 + 0.570 T	[19]

where

- μ_x - the viscosity of gas x (μP)
- T - the gas temperature ($^{\circ}C$)

The fractional gas concentrations of the wet gas may be calculated from F_{H_2O} and the dry gas concentrations measured from the mass spectrometer. The fractional concentration of water vapor is given by

$$F_{H_2O} = P_{H_2O}/P_B$$

From Appendix II the wet gas concentrations are

$$F_{wO_2} = F_{O_2} (1 - F_{H_2O}) \quad A3.5$$

$$F_{wCO_2} = F_{CO_2} (1 - F_{H_2O}) \quad A3.6$$

$$F_{wN_2} = (1 - F_{O_2} - F_{CO_2}) (1 - F_{H_2O}) \quad A3.7$$

The flow obtained from Equation A3.1 using the calculated PTM resistance obtained from Equations A3.2 thru A3.7 and Table A3.1 is under ITP conditions. Consider the respiratory ITP flow, temperature, and F_{H_2O} signals of Figure A3.2. The flow is divided into subintervals of duration Δt with points t_i in the center of each subinterval. The rectangle of height $\dot{V}(t_i)$ has an ITP volume, in liters, of

$$V_i(ITP) = \dot{V}(t_i) \Delta t$$

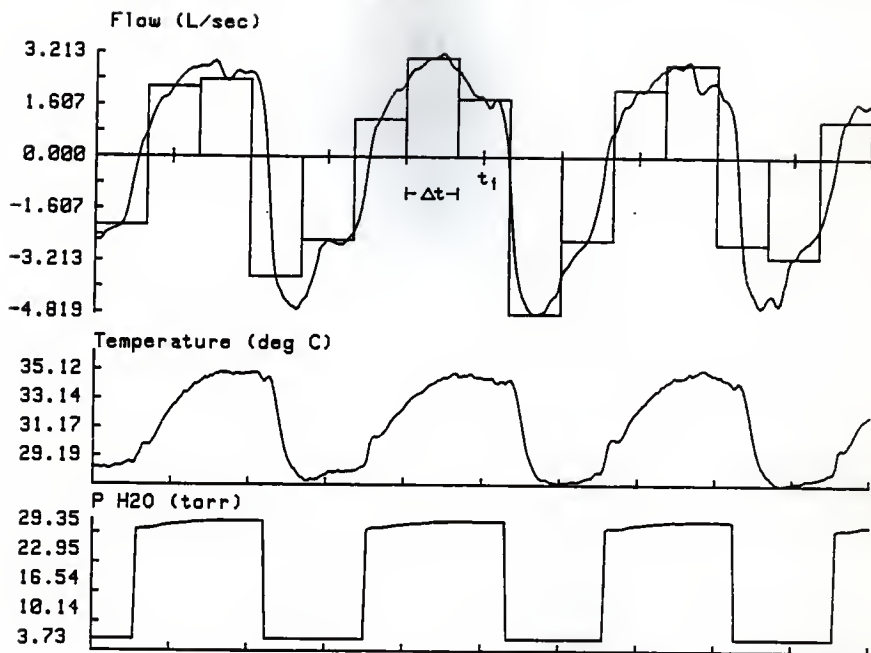


Figure A3.2 The \dot{V} , \dot{V} temperature, and F_{H_2O} signals.

If Δt is sufficiently small so that the temperature and F_{H_2O} over that interval are constant, then the volume of the dry gas is the total volume minus the volume of the water vapor and is given by

$$\text{dry volume} = V_i(\text{ITP}) - V_i(\text{ITP}) \cdot F_{H_2O} = V_i(\text{ITP}) \cdot [1 - F_{H_2O}]$$

Using the ideal gas law, this volume under STPD conditions is given by

$$V_i(\text{STPD}) = V_i(\text{ITP}) \cdot [1 - F_{H_2O}] \cdot \frac{273.15}{273.15 + T_i} \cdot \frac{P_b}{760}$$

This reduces to the familiar form of

$$V_i(\text{STPD}) = V_i(\text{ITP}) \cdot \frac{273.15}{273.15 + T_i} \cdot \frac{P_b - P_{H_2O}}{760} \quad \text{A3.8}$$

Since the individual volumes are under the same conditions, namely STPD conditions, they may be summed. Writing the Riemann sum of these individual STPD volumes over the inspiratory and the expiratory cycles and taking the

limit as Δt goes to zero results in:

$$\lim_{\Delta t \rightarrow 0} \sum_I \dot{V}(t_i) K(P_b, F_{H_2O}, T) \Delta t$$

$$\lim_{\Delta t \rightarrow 0} \sum_E \dot{V}(t_i) K(P_b, F_{H_2O}, T) \Delta t$$

These expressions become integrals in the limit. The values of these integrals are equal to the respective STPD inspiratory and expiratory tidal volumes. These integrals are

$$V_I(\text{STPD}) = \int_I \dot{V} K(P_b, F_{H_2O}, T) dt \quad \text{A3.9}$$

$$V_E(\text{STPD}) = \int_E \dot{V} K(P_b, F_{H_2O}, T) dt \quad \text{A3.10}$$

where the factor $K(P_b, F_{H_2O}, T)$ is defined as:

$$K(P_b, F_{H_2O}, T) = [1 - F_{H_2O}] \cdot \frac{273.15}{273.15 + T_i} \cdot \frac{P_b}{760} \quad \text{A3.11}$$

This factor is referred to as the ITP to STPD correction factor. From the form of Equations A3.9 and A3.10 a STPD flow is defined as:

$$\dot{V}_{\text{STPD}} = \dot{V} \cdot K(P_b, F_{H_2O}, T) \quad \text{A3.12}$$

The STPD tidal volumes are then:

$$V_I(\text{STPD}) = \int_I \dot{V}_{\text{STPD}} dt \quad \text{A3.13}$$

$$V_E(\text{STPD}) = \int_E \dot{V}_{\text{STPD}} dt \quad \text{A3.14}$$

These tidal volumes are then scaled to BTPS conditions and are given by:

$$V_I(\text{BTPS}) = V_I(\text{STPD}) \cdot \frac{273.15 + T_b}{273.15} \cdot \frac{760}{P_b - P_{H_2O}(T_b)} \quad \text{A3.15}$$

$$V_E(\text{BTPS}) = V_E(\text{STPD}) \cdot \frac{273.15 + T_b}{273.15} \cdot \frac{760}{P_b - P_{H_2O}(T_b)} \quad \text{A3.16}$$

Consumption of O_2 and production of CO_2 are determined by multiplying the STPD flow by the dry fractional gas signals. So that V_{O_2} and V_{CO_2} are given by:

$$V_{O_2} = \int_I F_{O_2} \cdot \dot{V}_{STPD} dt - \int_E F_{O_2} \cdot \dot{V}_{STPD} dt \quad A3.17$$

$$V_{CO_2} = \int_E F_{CO_2} \cdot \dot{V}_{STPD} dt - \int_I F_{CO_2} \cdot \dot{V}_{STPD} dt \quad A3.18$$

APPENDIX IV. A TUTORIAL OF THERMOCOUPLE PRINCIPLES

A thermocouple has the ability to convert thermal energy to electric energy. A thermocouple is made of two dissimilar conductors joined together at the point where temperature is to be measured, the sensing junction, and terminated at a point where both terminals are at the same temperature, the reference junction. Any conductor having different temperatures at its ends generates a voltage which is a function of the temperature difference. This effect can be modeled by a battery placed between the ends of the conductor. This model applied to a thermocouple is shown in Figure A4.1.

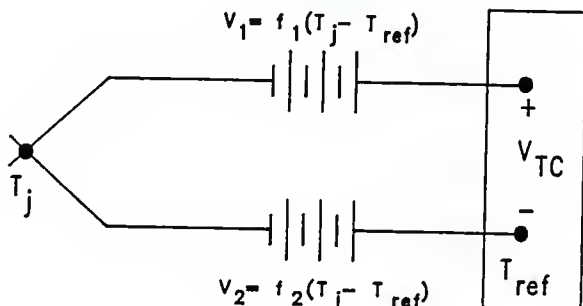


Figure A4.1. The basic thermocouple circuit

The terminal voltage, V_{TC} , is the algebraic sum of the two individual potentials, V_1 and V_2 . This sum yields a terminal voltage function of

$$V_{TC}(T_j, T_{ref}) = f_1(T_j - T_{ref}) - f_2(T_j - T_{ref})$$

If the two conductors are made of the same material the two voltage sources cancel out, $V_{TC} = 0$. However, thermocouples are made with the two leads of different metals such that one lead generates a positive voltage (positive lead) and the other lead a negative (negative lead).

The National Bureau of Standards (NBS) have specified voltage-temperature values for the most commonly used thermocouples. These values are specified with the junction temperature at zero degrees Centigrade, the ice-point. Table A4.1 contains the voltage-temperature values of type E thermocouples for temperatures from 16°C to 48°C in 4°C increments. This voltage-temperature relationship can be modeled with a second order polynomial,

$$V_{TC}(T_j, T_{ref} = 0) = F(T_j) = V_a \cdot T_j^2 + V_b \cdot T_j + V_c \quad A4.1$$

where

$V_{TC}(T_j, 0)$ = the thermocouple terminal voltage (mV)

T_j = the junction temperature ($^{\circ}\text{C}$).

The least squares method [1] is used to calculate the polynomial coefficients from the type E thermocouple voltage-temperature data [24] in 1°C increments from 0°C to 50°C . The polynomial coefficients are

$$V_a = 45.85(10)^{-6} \text{ (mV/} (^{\circ}\text{C})^2 \text{)}$$

$$V_b = 58.65(10)^{-3} \text{ (mV/} (^{\circ}\text{C}) \text{)}$$

$$V_c = 198.07(10)^{-6} \text{ (mV)}$$

Table A4.1 True thermocouple voltage, the second order thermocouple voltage estimate, and the associated error values versus sensing junction temperature (reference junction at 0°C).

Sensing junction Temperature (degrees C)	Terminal voltage (milli volts)	2nd order polynomial (milli volts)	2nd order error
16	0.950	0.950	-0.0276%
20	1.192	1.191	0.0465%
24	1.434	1.434	-0.0067%
28	1.678	1.678	-0.0128%
32	1.924	1.924	0.0104%
36	2.171	2.171	0.0069%
40	2.419	2.419	-0.0153%
44	2.669	2.669	-0.0133%
48	2.921	2.921	0.0066%

Average error: -0.0006%
Standard Deviation: 0.0191%

From the individual error values and their mean and standard deviation it is apparent that the type E thermocouple's voltage-temperature relationship can be modeled with the second order polynomial over the respiratory temperature range.

When the reference junction is at a temperature other than 0°C , the ice-point temperature, the terminal voltage is equal to

$$V_{TC}(T_j, T_{ref}) = V_{TC}(T_j, 0) - V_{TC}(T_{ref}, 0) = F(T_j) - F(T_{ref}) \quad A4.2$$

That is, the terminal voltage is equal to the the ice-point voltage corresponding to the sensing junction temperature minus the ice-point voltage corresponding to the reference junction temperature.

Temperature measurement using the thermocouple is based on determining the sensing junction temperature from the voltage measured at the reference terminals. Solving Equation A4.2 for the sensing junction temperature yields

$$T_j(V_{TC}) = F^{-1}[V_{TC}(T_j, T_{ref}) + F(T_{ref}, 0)] = F^{-1}[V_{TC}(T_j, T_{ref}) + V_{ref}] \quad A4.3$$

$$V_{ref} = V_{TC}(T_{ref}, 0)$$

That is, the sensing junction temperature is found by measuring the thermocouple terminal voltage, adding the reference junction temperature's ice-point voltage, and taking the inverse of Equation A4.1. There are two basic schemes used to accomplish the addition of the terminal voltage and the ice-point voltage corresponding to the reference junction's temperature.

- (1) Software compensation. The reference junction temperature, T_{ref} , is measured and used to determine the reference voltage, V_{ref} . This voltage is added to the measured terminal voltage, $V_{TC}(T_j, T_{ref})$, to obtain the voltage $V_{TC}(T_j, 0)$. In some implementations the reference junction is maintained constant at a known temperature, which is used to determine the reference voltage.
- (2) Hardware compensation. A temperature to voltage converter having a voltage-temperature relationship similar to the thermocouple is used to generate a voltage equal to V_{ref} . This voltage source is placed in series with the thermocouple so that the resulting voltage is equal to $V_{TC}(T_j, 0)$.

Software compensation, so named because the compensation voltage value is computed (rather than generated) and added to the measured terminal voltage, requires a separate transducer for monitoring the reference junction temperature or a heater to maintain the reference junction at a known temperature. This method requires a good deal of additional hardware and the transducer would not be one independent unit.

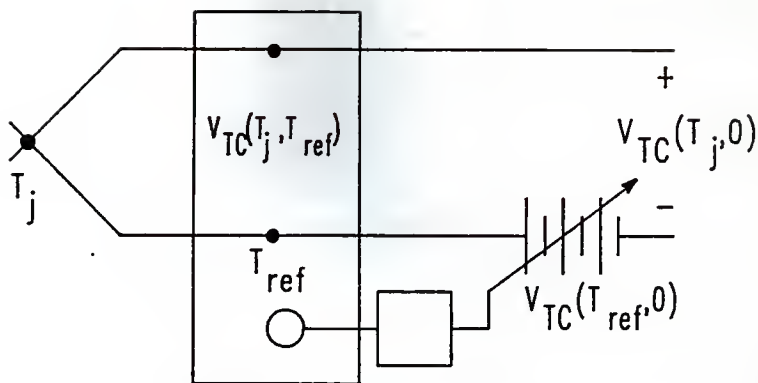


Figure A4.2. Hardware compensation of the reference junction temperature.

The basic scheme of hardware compensation is illustrated in Figure A4.2. The reference junction transducer is designed to have a temperature-voltage relationship, over the range of T_{ref} temperatures, similar to that of the thermocouple. The resultant terminal voltage is equal to the ice-point temperature specified by the NBS for the temperature T_j . This transducer functions independently so that only the output of the transducer need be measured.

APPENDIX V. OPERATION OF THE CBRMS

A description of the CBRMS from the viewpoint of a system operator follows in this appendix. This description will allow the operator, who is assumed to be familiar with the Hewlett-Packard 9826 computer system or other types of microcomputer equipment, the ability to calibrate the system, collect subject data, analyze the data and display the analyzed results. While this appendix is a 'cook-book' for the operation of the system, an understanding of what is occurring during the various phases is helpful.

The system layout is shown in Figure 2.2.1 with a detailed description given in Chapter II. A bicycle ergometer is used to exercise the subject at various work loads. The subject is fitted with a mask containing the three sensing elements of the four system transducers. The PTM senses flow, the thermocouple senses temperature, and the GMS probe samples the flow air for sensing fractional oxygen content and fractional carbon dioxide content. The four transducer outputs are connected to four channels of an eight-channel Data Acquisition Module (DAM). Under computer control the DAM samples these analog signals. The DAM passes the digital values to the computer. The computer can relate the digital data to the analog respiratory signals using the calibration parameters obtained from a computer controlled calibration routine. The sampled analog data are used to compute the various respiratory parameters. These parameters may be displayed in a variety of formats. An ECG telemetry unit is used to continuously monitor the heart rate and record the heart rate at 30 second intervals.

Two options are possible at power up: the data collection and system calibration operating system, Pascal, may be booted (a term synonymous with pulling up by the boot straps) or the analysis and file compaction operating system, Basic, may be booted. The transducers should be periodically calibrated according to their specified calibration procedures (these calibration procedures are different from the system calibration outlined in Section A5.3).

The collection of data and system calibration occur under computer control using programs written in Pascal. Following calibration of the system, the calibration data are stored in the system's mass

storage. The computer collects the respiratory data and stores it in the system's mass storage. The standard Pascal operating system routines are also available to the operator.

Data is passed from the calibration and data collection system, Pascal, to the analysis and data compaction routines using the mass storage devices. The calibration and respiratory data are stored in ASCII files (the ASCII format is the only compatible file format between the two systems). ASCII files require large storage space and considerable retrieval from storage time. In order to minimize storage space and retrieval time the ASCII files are converted to the more compact numeric format of the Basic operating system. The compaction routines read the ASCII data from the mass storage devices, compact it (convert the data to numeric format), and re-store the data in smaller numeric files.

The analysis procedure calculates the breath-by-breath respiratory parameters using the collected respiratory data. The respiratory data are related to the respiratory signals using the calibration factors. The respiratory data and calibration factors are retained in memory once they have been read from mass storage. This allows the data that have been compacted by the data compaction procedures (CAPCRUNCH and DAPCRUNCH) to remain available to the analysis and display routine without the need to read it from storage. The analysis procedure also displays the calculated respiratory parameters.

A5.1 The Computer System: An overview

The computer system is based on the Hewlett-Packard, series 200, 9826 computer with 1.34 MB of internal RAM, an internal 5.25" floppy disk drive with a 256 kB capacity, and two operating systems; a Basic system stored in ROM (Read Only Memory) and a Pascal system stored on floppy disks. The 9826 is connected to two other mass storage devices; a Hewlett-Packard HP9895A 8" floppy disk with 1 MB capacity and a Hewlett-Packard HP9134 4 MB hard disk system, of which 3 MB is available to the 9826 computer while 1 MB is reserved for another computer. The system uses three devices for hard copy output: a Digital Equipment Corporation DECwriter II printer, a Hewlett-Packard HP2673A printer, and a Hewlett-Packard HP9872C eight pen plotter. The computer system is interfaced into the remaining portion of the CBRMS with the DAM

which performs an analog-to-digital (A/D) conversion on the four analog respiratory signals.

The Basic operating system, version 2.0, will automatically boot up at power on. The first thing the system will do is check the internal 5.25" disk drive for a program titled AUTOST (an acronym for AUTOSTart) which, if found, is loaded into the computer memory and execution of the AUTOST program begins. The CBRMS uses such a program as will be described in Section A5.5.1.

If a great deal of programming is to be done, the program designer should become familiar with the Basic utility programs and the Basic 2.0 language extensions package, AP2.0. The utilities can backup disks, perform a program variable cross reference, unpurge files, indicate the remaining disk space, and repack disks to get rid of blank sectors between files (resulting in more room on the disk). The Basic language extensions are documented in the manuals of the Hewlett-Packard Computing Lab, Durland 293. The extensions provide extended editing features by allowing for the locating and/or the changing of program text, the moving or copying of several program lines, the automatic indentation of the structured levels, and a few other editing operations. Incorporation of the extensions into the Basic programs of the CBRMS would provide real time clock support (determination of date and time), matrix operations, maximum and minimum values of arrays, and a number of other useful extensions.

The Pascal system is a disk based system which is booted by placing the Pascal 2.1 System Boot Disk in the internal drive. This disk will load the Pascal system and Pascal's Editor, Filer, and Compiler into memory. The operator should become familiar with the Main Command Level of the operating system and program designers should become familiar with the Editor, Compiler, and Filer.

The Hewlett-Packard peripherals are tied to a common HP-IB interface bus, the DECwriter II is connected to a RS232 port, and the DAM is interfaced to a GPIO (General Purpose Input/Output) port. The GPIO has sixteen bits of input, sixteen bits of output (in parallel), and several control lines. Each peripheral device has a unique address that is represented differently in the two operating systems. The Basic operating system uses the specific addresses of the different

peripherals while the Pascal system assigns a logical unit number to each device. The Pascal system also recognizes the volume label of a disk in addition to the disk drive's unit number. The peripherals and their corresponding designation in the two systems are shown in Table A5.1.1.

Table A5.1.1 Computer system peripheral designations

Peripheral	Computer System Address	Basic Operating System Designation	Pascal Operating System Designation	Volume Label
8" drive HP9895A	700	:HP9895,700	#7	(see note 1)
Hard Disk HP9134A	702			
Platter 0	702,0	(see note 2)		
Platter 1	702,1	:HP9895,700,1	#12	HARD1:
Platter 2	702,2	:HP9895,700,2	#13	HARD2:
Platter 3	702,3	:HP9895,700,3	#14	HARD3:
DECwriter II	9	9	#6	PRINTER:
HP printer HP2673A	701	701	not recognized (see note 4)	(see note 3)
Plotter	705	705,HPGL	not recognized (see note 4)	
DAM	12	12	not recognized (see note 5)	
Internal		:INTERNAL	#3	(see note 1)

Note 1: The volume label depends upon the disk that is in the drive. Each disk has its own volume label. If the disk was initialized by Basic command INITIALIZE the volume label is B9826:. This label can be changed with the Filer in the Pascal system and also the Basic utility program INITIALIZE. Using the Filer is easier (refer to A5.3.2).

Note 2: Platter 0 has been initialized for the HP9835 computer system. This platter could be set up to work with the 9826 computer system.

Note 3: The DECwriter printer is assigned the volume label PRINTER by the Pascal operating system.

Note 3: These devices are not recognized by the Pascal system. In order for the system to recognize the peripherals the program TABLE.CODE must be altered. TABLE.CODE is automatically loaded during Pascal booting and its purpose is to check for peripherals, and assign the unit numbers. The source code for this program is CTABLE.TEXT and is located on the Pascal system disk titled CONFIG:. The most recent version is CTABLE2.0.TEXT which sets the priority of the internal disk drive higher than the other drives so that the AUTOSTART program is loaded from the internal drive. Revisions to this program would allow the system to recognize the other devices. However, such revisions may be difficult and should be left to the experienced program designer. Documentation of the TABLE is located in the technical reference, pages 442 to 457, of the Pascal 2.1 User's Manual.

Note 5: The DAM is not recognized by the system but it is still possible to access the device through program control.

A5.2 System Power up

Turning on the CBRMS involves two steps: (1) setting up of the instrumentation and system calibration equipment and (2) the power up of the computer system (if the operator is interested in the analysis of data only, the instrumentation need not be turned on). Prior to the system calibration and the collection of data the individual transducers must be calibrated and the gain and offsets of the DAM set. Calibration of the Perkin-Elmer Medical Gas Analyzer (referred to as the GMS, Gas Mass Spectrometer) and Godart pneumotachograph are spelled out in their respective manuals and calibration of the temperature transducer is described in Chapter III. DAM gain and offset adjustments are described in Appendix II of Riblett's work [13].

Following is a list of the instrumentation and calibration equipment which must be turned on.

Instrumentation Equipment

1. Perkin-Elmer Medical Gas Analyzer. The GMS is generally left in the standby mode. Simply press the GMS ON button. If power to the GMS has not been turned on the GMS must be 'pumped down'. The pump down procedure is outlined in the GMS owners manual and requires two to eight hours to accomplish.
2. The Godart pneumotachograph. The PTG should be left on during periods of frequent use or given ample time to warm up.
3. The Tektronics cabinet containing the temperature transducer.
4. The zero-suppression box. The zero-suppression box is used to alter the DC voltage level of the GMS O_2 and CO_2 outputs so that the signals are bipolar and centered about zero volts. The zero-suppression box should be left on during periods of frequent use or given ample time to warm up.
5. The Tektronics cabinet containing the DAM.
6. The cardiometer should be ready. The cardiometer is always on provided its batteries are good.

7. The fan for blowing the expired gases away from the subject should be ready.
8. A thermometer for measuring the subject's pre- and post-exercise body temperatures, a watch for monitoring experimental time, and a metronome for pacing the subject should be available and made ready.

Calibration Equipment

1. The temperature calibration bath heaters. The heaters should be turned on 3 hours prior to calibration to allow enough time for the water baths to warm up.
2. The GMS calibration gas should be ready but not on.
3. The Harvard respirator and the zero flow isolation box should be ready.
4. The PTM heater should be ready but not on.

The computer system must be powered up in three steps; the peripherals turned on, the necessary operating system loaded, and the program execution began. The Hewlett-Packard 9826 manuals specify that all computer peripherals must be turned on before the 9826 computer is turned on. The Pascal operating system needs to be loaded if the CBRMS system is to be calibrated or respiratory data are to be collected. The Basic operating system is used for analysis and compaction of the data.

Booting the Pascal 2.1 operating system

Below is a step by step procedure for booting the Pascal operating system.

1. Make certain that all computer system peripherals (DECwriter II printer, both external disk drives, HP2673A printer, and the plotter) are on.
2. Place the 5.25" disk titled Pascal 2.1 system Boot disk in the HP9826's internal disk drive.
3. Turn the HP9826 on.
4. Allow the system to boot (approximately 1 1/2 minutes).

5. The system will prompt you for the new system date. Enter the system date in the format DD<separator>MON<separator>YR; where DD is the date, MON is a three letter abbreviation for the month, YR is the last two digits of the year, and <separator> is any non-alphanumeric character (usually a period is easier as it is located on the numeric keypad) followed by depressing the ENTER key. The entire date is not necessary if the current month or current year is correct. If the current system date is to be used just press the ENTER key.
6. The system will prompt for the new system time. Enter the system time in the format HH<separator>MM<separator>SS; where HH is the hour (using the 24 hour clock), MM is the minutes, SS is the seconds, and <separator> is any non-alphanumeric character (usually a period is easier as it is located on the numeric keypad) followed by depressing the ENTER key. It is not necessary to enter the entire time. If the current system clock time is to be used just press the ENTER key.

Example of the setting the system date and time:

Screen display:

prompt line

System date is	19-Feb-85
System time is	13:20:22

Work Station	Rev. 2.1	1-Mar-83
--------------	----------	----------

Available global memory	51420 bytes
Total available memory	899894 bytes

Default volume:	HARD3:
System volume:	HARD3:

Copyright information

Response to the system date prompt line
Enter the new system date: 20.MAR.85

Response to the system time prompt line
Enter the new system clock time: 8.26

The displayed system data and time will be updated. Pressing the V key (V for the command Version) while in the Main Command Level will allow for the correction of mistakes.

The Pascal operating system is now loaded and the system is in the Main Command Level. Beginning operation of programs (as described in Section A5.4 for the data collection and calibration programs), the Editor, the Filer, etc. are possible from the Main Command Level.

Booting the Basic 2.0 operating system

The Basic operating system; version 2.0, is stored in ROM in the HP9826 and is automatically loaded as the operating system provided some other operating system is not present on the disk in the internal drive.

1. Make certain that all computer system peripherals (the DECwriter II printer, both external disk drives, the HP2673A printer, and the plotter) are on.
2. Place the 5.25" floppy disk titled "Michael's Analysis disk" in the internal disk drive.
3. Turn the HP9826 computer on.
4. Allow the system to boot and load the autostart program, AUTOST (approximately 15 seconds).
5. The AUTOST program will begin execution. The compaction programs (CAPCRUNCH and DAPCRUNCH), the analysis and display program (ANALYSIS), and the heart rate storage routine (STOREHR) can be called from AUTOST. The program can be exited to allow for editing or execution of other programs or any other Basic operation.
6. Load the Basic Extensions package, AP2.0. These extensions provide the programmer with many tools to aid the editing and development of programs (locating and/or changing of program text and variables, automatic indentation of the structure levels, and many other enhancements). Refer to the reference [23] for detailed information of the Extensions 2.0 refer. The extensions package does not need to be loaded unless program design or editing is to be done. To load the extensions package, exit the AUTOST program and execute the command SCRATCH A to clear all program memory. Execute the command LOAD BIN "AP2_0:HP9895,702,3" (the extensions are located on the hard

disk, platter 3). The extensions will take approximately 20 seconds to load.

A5.3 Configuration of the ASCII data disks

The calibration data generated by CAP2.CODE and the respiratory data collected by DAP2.CODE are stored in ASCII format. The respiratory data require a lot of disk space (24,000 data points require 750 kB, 768,000 bytes; i.e. 4 integers/datum point times 2 bytes/integer times 24,000 datum points per channel times 4 channels). Due to the large amount of required storage space for the ASCII data, the possible storage devices are limited to the 8" floppy disk and platters one and two of the hard disk.

The respiratory data collection program stores the four channels of data in files named MONSTER1.ASC thru MONSTER4.ASC for all data collection runs; the permanent naming of the respiratory data files occur during file compaction using the program DAPCRUNCH in the Basic operating system. The Pascal system does not protect existing files as does the Basic operating system so that it is possible to write to these files with new data, resulting in the old data being overwritten and lost. To solve this problem a separate file named DISK_STAT.ASC was created on each ASCII data disk which indicates the status of the disk: either a full status, the disk contains data that has not been crunched, or the empty status, no ASCII data exists on the disk. The data collection program, DAP2.CODE, checks this file to obtain the status of the disk and if it contains ASCII data the operator is prompted to choose another storage device or replace the disk. The original data collection program, DAP.CODE [13], does not check the disk status and all un-compacted data are not protected from being overwritten.

If the disk selected for storing the ASCII data does not contain the status file, as is the case with a newly initialized disk, the program will crash and the collected data will be lost. Therefore care should be taken to make certain that the following ASCII data disk configuration procedure is followed for a newly initialized ASCII data disk.

The Pascal system's Filer may be used to check a disk to deter-

mine if it contains the status file. Execute the Filer by pressing the F key (F for Filer) while in the Main Command Level. Once in the filer, press the L key (L for List a directory). Enter #7 (#7 is the unit number assigned to the 8" disk drive) in response to the 'List what directory?' prompt. This will list the files contained on the disk and the space remaining on the disk. The disk has been configured if it contains the file 'DISK_STAT.ASC' in its directory.

The procedure below can also be used to re-configure a disk so that it will except ASCII data. This is useful if a disk contains unwanted data which can occur during practice sessions with the respiratory data collection program or from an experimental collection in which a problem arose. Reconfiguration of a disk is accomplished by following steps three thru five of the procedure below.

A5.3.1 Procedure for setting the status of an ASCII data disks to empty

1. Select an 8" disk to contain the ASCII data. If the disk is new or contains un-wanted data and programs, the disk must be initialized (step 2). If the disk has already been initialized and contains enough room to store the ASCII data then proceed to step 3.

2. While in the Basic operating system execute the command

INITIALIZE ":HP9895,700".

This will start the initialization process of the ASCII data disk. The process requires approximately 10 minutes to complete.

3. Boot up the Pascal operating system as described in Section A5.2 of this appendix.
4. Run the Pascal program ASCII_CONF.CODE by pressing the R key (R for Run), type the program name, ASCII_CONF, and press the ENTER key. The program will begin execution and display the three disk drives which may be configured to except the ASCII respiratory data: the disk in the 8" drive and platters one and two of the hard disk.
5. Enter the number corresponding to the device that is to be configured and press the ENTER key (for the newly initialized 8" disks select option 3). The program will now create the status

file, set the status to empty. Execution then returns to the Main Command Level. The disk is now ready to except respiratory data collected by the data collection program DAP2.CODE.

A5.3.2 Changing the volume label of a disk

The volume label of a disk may be altered with the Pascal system's filer. This allows a meaningful volume label, the subject's name for example, to be placed on the disk. The volume labels on the hard disks are HARD1, HARD2, and HARD3, corresponding to platters one thru three and should not be altered. To change the label of the 8" disk, follow the procedure below. Refer to the Filer portion of the Pascal 2.1 User's Manual [1] for the details. Disks newly initialized using the Basic operating system and the INITIALIZE command will have the volume label 'B9826:'.

1. From the Main Command Level enter the Pascal system Filer by pressing the F key. The Filer will begin execution and the Filer Command Line will be displayed.
2. Press the C key (C for Change).
3. In response to the 'Change what file?' prompt, enter '#7:' followed by the ENTER key (the unit number of the 8" drive is #7).
4. In response to the 'Change to what?' prompt enter the new volume label (6 characters maximum) followed by a colon and press the ENTER key.
5. Press the V key (V for Volumes recognized by the Pascal system). The peripherals recognized by the Pascal system will be displayed. If the volume was successfully changed the new volume label will appear alongside the unit number 7.
6. The disk can now be referred to with the specified volume label.
7. Exit the filer and return to the Main Command Level by pressing the Q key (Q for Quit).

A5.4 Calibration and data collection

Calibration of the CBRMS and collection of data with the CBRMS are relatively simple procedures whose sequences are controlled by two Pascal programs, CAP2.CODE (Calibration Program, Version 2) and DAP2.CODE (Data Acquisition Program, Version 2). The program CAP2.CODE controls calibration of the system and DAP2.CODE controls collection of respiratory data. The programs prompt the operator with simple instructions which, in conjunction with this operator's guide, describe the tasks to be performed. The first section to be presented will provide an operator's guide to calibration of the CBRMS using the program CAP2.CODE and the second will provide an operator's guide to collection of respiratory data using the program DAP2.CODE. Operation of the data compaction routines and the data analysis and display routine is described in Section A5.5 of this appendix.

A5.4.1 Operator instructions for calibration of the CBRMS.

Following is a step-by-step procedure for the calibration of the Computer Based Respiratory Measurement System using the Pascal program CAP2.CODE. The calibration procedure is best accomplished with two operators working as a team; one operator handling the instrumentation and the other operating the computer system. However, one operator can easily accomplish the calibration procedure. The procedure can be completed in ten minutes by an experienced operator (or operator team), but the operator(s) should not be discouraged if a longer time is needed. Above all, do not rush through the procedure. A lot of operations are performed and must be performed carefully and accurately.

1. Power up the instrumentation system and the Pascal operating system as described in Section A5.2 of this appendix. (Remember to allow ample time for the water baths to heat up and for the Godart PTG and zero-suppression box to warm up and stabilize.)
2. Make certain that the disk to be used for storage of the ASCII data is ready.
3. Execute the calibration program by pressing the R key (R for Run). Type the program name, CAP2, followed by the ENTER key (it is not necessary to type CAP2.CODE, as the system will tack

on the .CODE part). Program execution will begin.

4. Enter the sampling frequency in response to the program prompt, 'ENTER THE SAMPLING FREQUENCY: '. Typically 50 (for 50 Hz) is used.

Note: As with all numeric input while running a Pascal program, make certain that only numeric keys, the '-' key, the '+' key, or the '.' key are pressed. Depression of any non-numeric key will cause the program to crash and all preceding data are lost.

Calibration of the GMS

5. Determine if the fractional gas signals are to be calibrated and respond to the prompt, 'CALIBRATE FRACTIONAL CONCENTRATION SIGNAL? (Y/N)'. If the fractional gas signals are not to be calibrated skip to step number 16.

Note: as with all yes or no questions enter 'Y' (or 'y') for yes or enter 'N' (or 'n') for no. Entering any key other than 'Y' or 'N' is not excepted and you will be prompted to re-enter your response.

6. Place the GMS probe in room air. The calibration program prompts the operator to do this by displaying 'CONNECT THE GMS PROBE TO ROOM AIR.'. While the room air signal is being sampled, in step 9 below, be careful not to breath on or near (within a few feet) the GMS probe as this will alter fractional content of the gas being sampled and cause erroneous fractional gas calibration factors.
7. Enter the percent composition of CO_2 in room air (0.04) in response to the prompt, 'ENTER ACTUAL PERCENT CO_2 CONCENTRATION.'. Enter the value as a percentage. Room air CO_2 concentration is 0.04%, enter this value rather than the GMS reading.
8. Enter the percent composition of O_2 in room air (20.93) in response to the prompt, 'ENTER ACTUAL PERCENT O_2 CONCENTRATION.'. Enter the value as a percentage. Room air O_2 concentration is 20.93%; enter this value rather than the GMS

reading.

Note: The GMS should be recalibrated if the displays indicate significantly different concentration values from those in the sampled gas (see the operator's manual).

9. Press the ENTER key, which is what the program instructs the operator to do, to sample the GMS outputs while the GMS probe is in room air. The program will display the length of time the system will take to sample the signal.
10. The average binary values of the sampled data for room air conditions are displayed.
11. Place the GMS probe in the calibration gas delivery port and open the main valve on the calibration gas cylinder. The calibration program prompts the operator to do this by displaying 'CONNECT THE GMS PROBE TO THE CALIBRATION GAS.'
12. Enter the percentage CO₂ concentration of the calibration gas in response to the prompt, 'ENTER THE ACTUAL PERCENT CO₂ CONCENTRATION.'. The present calibration gas contains 7.0% CO₂. If in doubt check the gas cylinder for the correct value.
13. Enter the percentage O₂ concentration of the calibration gas in response to the prompt, 'ENTER THE ACTUAL PERCENT O₂ CONCENTRATION.'. The present calibration gas contains 12.9% O₂. If in doubt check the gas cylinder for the correct value.
14. Press the ENTER key, which is what the program instructs the operator to do, to sample the GMS output while the GMS probe is in the calibration gas. The program will display the length of time the system will take to sample the signal.
15. The average binary values of the sampled data for the calibration gas are displayed followed by a display of the computed calibration factors for the fractional gas signals.

Calibration of the Temperature Transducer

16. Determine if the temperature transducer is to be calibrated and respond to the prompt, 'Do you wish to calibrate the temperature transducer? (Y/N)'. If the temperature transducer is not to be

calibrated then enter 'N' and continue with step 23.

17. Read the calibrated thermometer while it is placed in the lowest temperature bath, place the tip of the thermocouple in the bath, and enter the thermometer reading into the computer. The computer will sample the temperature channel and average the samples. The average of the samples is displayed.
18. Step 17 is repeated for the middle temperature bath and the high temperature bath.
19. The program will display the computed calibration factors.
20. Based on the calibration factors, determine if the temperature transducer is to be re-calibrated and answer the prompt, 'Do you wish to re-calibrate the temperature transducer? (Y/N)'. If the temperature transducer is not to be re-calibrated then continue to step 22.
21. Make certain you want to re-calibrate the temperature transducer. Respond to the prompt, 'You are going to re-calibrate the temperature transducer. Is that what you wish to do? (Y/N)'. If the transducer is to be re-calibrated, then return to step 17.

Calibration of the PTG flow transducer

23. Determine if the PTG flow transducer is to be calibrated and respond to the prompt, 'CALIBRATE THE FLOW TRANSDUCER? (Y/N)'. If the flow transducer is not to be calibrated then enter 'N' and continue with step 36.
24. Determine if the temperature and viscosity corrections are to be used in calibrating the PTG flow transducer and respond to the prompt, 'Do you wish to use gas temperature and gas viscosity calculations while calibrating the flow signal? (Y/N)'. If temperature and viscosity corrections are not to be used with the flow calibration then enter 'N' and continue with step 28.
25. Enter the ambient relative humidity in response to the prompt, 'Enter the percent relative humidity.'.

26. Enter the ambient temperature (degrees Fahrenheit) in response to the prompt, 'Enter the room temperature. (deg F)'.
27. Enter the barometric pressure (inches mercury) in response to the prompt, 'Enter the barometric pressure. (inches)'.
28. Determine if a default value of 2038 is to be used for the binary value corresponding to zero flow through the PTM and respond to the prompt, 'You can determine the binary zero flow or use a default value of 2038. Do you wish to determine binary zero flow? (Y/N)'. If you wish to use the default value then enter 'N' and continue to step 32.
29. The prompt, 'CONNECT ZERO FLOW TO THE PNEUMOTACHOMETER', will now be displayed. In addition to connecting zero flow to the PTM, the PTG must be zeroed. The PTG is zeroed by placing the PTG in the volume mode (set switch to 'V'). Blow into the PTM until the PTG needle is in the middle of the scale. Place the PTM in the zeroing box to isolate it from all air flow. Adjust the zeroing potentiometer until the PTG needle does not move.
30. Return the PTG to the flow mode (set the switch to flow).
31. Press the ENTER key when zero flow is attained (by leaving the PTM in the zeroing box). You are instructed to do so by the 'PRESS ENTER TO CONTINUE' prompt. The computer samples the zero flow signal and averages the samples to compute the binary value corresponding to zero flow. Once computed, the zero flow binary value is displayed to the operator.
32. If temperature and gas viscosity corrections are to be used, as selected in step 24, insert the temperature transducer into the PTM head.
33. Turn the PTM heater on. Connect the harvard respirator to the PTM. Turn the respirator on and allow the PTM temperature to stabilize (a few minutes).
34. Press the ENTER key when the PTM temperature has stabilized. You are instructed to do so by the 'PRESS ENTER TO CONTINUE' prompt. The computer samples the flow signal. Once the flow signal has been sampled the respirator may be turned off. At

this time, the subject may be placed on the ergometer and fitted with the instrumentation.

35. The computer integrates each inspiratory and expiratory cycle of the pump to attain a volume that is directly proportional to the respirator's volume. Two sets of volumes are computed, one set uses no temperature or viscosity corrections and the other does. If temperature and gas viscosity corrections were not to be used, as selected in step 24, the corrected values are set equal to the non-corrected values. The two sets of volumes are displayed on the screen for each cycle of the respirator. The individual inspiratory and expiratory volumes are averaged and the proportionality factors (the calibration factors) which relate the computed volume to the respirator volume are determined. These calibration factors are displayed on the CRT.

Storage of the Calibration Data

36. Determine if the calibration data are to be stored on disk and respond to the prompt, 'STORE CALIBRATION FACTORS ON DISK? (Y/N)'. If the calibration values are not to be stored enter 'N' and proceed to step 41.
37. Enter the calibration file name.
38. Specify which disk drive is to contain the calibration data.
39. Enter the current date.
40. The calibration data will be stored.
41. The calibration procedure is complete.

A5.4.2 Operator instructions for collection of respiratory data with the CBRMS

Following is a step-by-step procedure for the collection of respiratory data using the Computer Based Respiratory Measurement System (CBRMS). The data procedure is best accomplished with two operators working as a team; one operator monitoring the subject and handling the instrumentation and the other operating the computer system. However, one operator can easily accomplish the task.

1. If the system is not on then power up the instrumentation system and the Pascal operating system as described in Section A5.2 of this appendix. The system is generally powered up prior to data collection, as the system is usually calibrated prior to data collection.
2. Make certain that the disk to be used for storage of the ASCII data is ready and has been configured to accept the data from the data collection program (see Section A5.3). If the disk has not been configured to accept the data, the program will crash and all data will be lost when an attempt is made to write the data to disk in step 9.
3. Execute the data collection program by pressing the R key (R for Run). Type the program name, 'DAP2', (it is not necessary to type DAP2.CODE, the system will tack on the .CODE part) followed by the ENTER key. Program execution will begin.
4. Enter the sampling frequency in response to the program prompt, 'ENTER THE SAMPLING FREQUENCY: '. Typically 50 (for 50 Hz) is used.

Note: as with all numeric input while running a Pascal program, make certain that only numeric keys, the '-' key, the '+' key, or the '.' key is pressed since depression of any other key will cause the program to crash and all preceding data are lost.

5. Enter the number of samples to be collected in response to the program prompt, of 'ENTER NUMBER OF SAMPLES [24,000 MAX]:'. The number of samples must be in the range 1 to 24000 for the current system.
6. Make certain the subject is prepared, then press the 'ENTER' key to begin collection of the data. The number of samples and the length of time required to collect the samples will be displayed. The computer will sound an audible beep and display the message, 'DATA COLLECTION COMPLETE' when the data have been collected. The computer then calculates the maximum and minimum values of each channel and counts the number of data points equal to the saturation values (0 or 4095) for each channel. No operator input is required until all the data has been collected

and the maximum value, minimum value, and number of saturation points counted.

7. This is your last chance to make certain that the device to contain the ASCII data has been configured to hold ASCII data (see Section A5.3)
8. Select the mass storage device which will contain the ASCII data.
9. If the device presently contains ASCII data the computer will have you enter an alternate device. Otherwise, the data are stored.
10. The data collection procedure is complete.

A5.5 Compaction of the Calibration and Respiratory Data

Compaction of the calibration data and the respiratory data stored in ASCII format by the Pascal programs CAP2 and DAP2 to the numeric format of Basic will now be described. Compaction of the data is accomplished with two Basic programs: CAPCRUNCH for compaction of the calibration data and DAPCRUNCH for compaction of the respiratory data. The programs are simple to operate and require minimal operator input. Operator instructions for the compaction of the data will now be given. If only one type of compaction is necessary the other compaction operation may be bypassed.

The calibration and respiratory data will be stored on an 8" floppy disk. If the ASCII data are also stored on 8" floppy disk, the two disks will have to be switched during operation of the programs. The compaction programs will prompt the operator when the disks need to be exchanged.

1. Power up the Basic operating system as described in section A5.2 of this appendix. If the Basic operating system is powered up, execution of the AUTOSTart program may be accomplished by the command

LOAD "AUTOST:INTERNAL",1

2. Have an 8" disk prepared to accept the calibration data and

respiratory data. Continue with step 3 for the compaction of the calibration data or skip to step 11 for compaction of the respiratory data.

Compaction of the calibration data

3. With the AUTOSTart program executing, press the k_0 soft key which has the label "CCRUNCH". CAPCRUNCH will load and execution will begin.
4. Press the k_0 softkey labeled "CCRUNCH" again to continue with the compaction of the calibration data. CAPCRUNCH allows the return to the AUTOST program by pressing the k_9 softkey labeled "EXIT". This may be desired if the CCRUNCH key was accidentally pressed from the AUTOSTart program.
5. Enter the name of the calibration file.
6. Three mass storage devices will be displayed on the screen: platters 1 and 2 of the hard disk and the 8" disk. Enter the number corresponding to the mass storage location which contains the calibration data collected by CAP2.CODE.
7. If the ASCII data were stored on an 8" disk (as specified in step 6) then place the ASCII data disk in the 8" disk drive in accordance with the prompt displayed on the computer's screen. Press the CONTINUE key when this is accomplished. If the data were stored on the hard disk place the 8" disk which will contain the compacted data in the 8" disk drive and continue to step 10 (the ASCII data will be read, converted to numeric format, and stored; this will require several seconds).
8. The data will be read from the disk (a few seconds) and the operator prompted to place the 8" disk which will contain the compacted data in the 8" disk drive. Press the CONTINUE key when this is accomplished.
9. The data will be stored (several seconds) and the operator prompted to place the ASCII data disk in the 8" disk drive. Press the CONTINUE key when this is accomplished. The ASCII data will then be destroyed.
10. Program operation will return to the AUTOSTart program.

Compaction of the respiratory data

11. With the AUTOSTart program executing, press the k_1 soft key which has the label "DCRUNCH". DAPCRUNCH will load and execution will begin.
12. Press the k_1 softkey labeled "DCRUNCH" again to continue with the respiratory data compaction. DAPCRUNCH allows for the return to the AUTOST program by pressing the k_9 softkey labeled "EXIT". This may be desired if the DCRUNCH key was accidentally pressed from the AUTOSTart program.
14. Three mass storage devices will be displayed on the screen: platters 1 and 2 of the hard disk and the 8" disk. Enter the number corresponding to the mass storage location which contains the respiratory data collected by DAP2.CODE.
15. Enter the number of data points which were collected.
16. Enter the name of the CO_2 data file.
17. Enter the name of the O_2 data file. (If the O_2 file name begins with a O and the remaining portion of the file name is the same as the CO_2 file name, with the exception of the first letter, then simply press the CONTINUE key. Example: O_2 file name is O1106N175 and CO_2 file name is C1106N175).
18. Enter the name of the flow data file. (If the flow file name begins with a V and the remaining portion of the file name is the same as the CO_2 file name, with the exception of the first letter, then simply press the CONTINUE key. Example: flow file name is V1106N175 and CO_2 file name is C1106N175).
19. Enter the name of the temperature data file. (If the temperature file name begins with a T and the remaining portion of the file name is the same as the CO_2 file name with the exception of the first letter then simply press the CONTINUE key. Example: temperature file name is T1106N175 and CO_2 file name is C1106N175)
20. If the ASCII data were stored on an 8" disk (as specified in step 14) then place the ASCII data disk in the 8" disk drive in

accordance with the prompt displayed on the computer's screen. Press the CONTINUE key when this is accomplished. If the data were stored on the hard disk place the 8" disk which will contain the compacted data in the 8" drive and continue to step 24 (the ASCII data will be read, converted to numeric format, and stored; this will require a few minutes for a large number of data points).

21. The data will be read from the disk and converted from ASCII characters to numeric values, one data file at a time. This operation will take several minutes to accomplish for a large number of data points. The progress of the operation can be monitored on the bottom line of the CRT.
22. Place the data disk which will contain the numeric data in the 8" drive and press CONTINUE.
23. The data will be stored (several seconds) and you will be prompted to place the ASCII data disk in the 8" disk drive. Press the CONTINUE key when this is accomplished. The ASCII data will then be destroyed.
24. Program operation will return to the AUTOSTart program.

A5.6 Data Analysis and Display

The analysis and data display operations will now be described. The two operations are described in a single section since the present system uses the same routine to perform both analysis of the respiratory data and the display of the analyzed results.

1. Power up the Basic operating system as described in section A5.2 of this appendix. If the Basic operating system is powered up, execution of the AUTOSTart program may be accomplished by the command

LOAD "AUTOST:INTERNAL",1

2. Press the k_2 soft key labeled "ANALYSIS". This will cause the ANALYSIS program to be loaded.
3. Press the k_1 softkey labeled "ANALYSIS" again to continue with the analysis and display program. ANALYSIS allows the return to

the AUTOST program by pressing the k_9 softkey labeled "EXIT". This may be desired if the ANALYSIS key was accidentally pressed from the AUTOSTart program.

4. Enter the subject's name or the subject's identifier (25 characters maximum). This name (or identifier) will become a part of all hard copy output of the ANALYSIS routine.
5. Previous execution of the data compaction routines, CAPCRUNCH and DAPCRUNCH, or the analysis routine, ANALYSIS, will have placed the subject data in the 9826's memory. If this is the case, information about the data is displayed on the screen. With data in memory, perform steps 6 thru 14 otherwise proceed to step 15.
6. Determine if the calibration data currently in memory is to be used and respond to the prompt, 'DO YOU WISH TO USE THESE CALIBRATION DATA? (Y/N)'. If the current calibration data are to be used answer yes, 'Y', and proceed to step 8.
7. Enter the name of the calibration file in response to the prompt, 'ENTER THE CALIBRATION FILE FILENAME.'. The specified calibration file will be loaded.
8. Determine if the respiratory data currently in memory is to be used and respond to the prompt, 'DO YOU WISH TO USE THESE B_by_B DATA? (Y/N)'. If the current respiratory data are to be used answer yes, 'Y', and proceed to step 14.
9. Enter the number of data points which were collected in response to the prompt, 'ENTER THE TOTAL NUMBER OF POINTS TO BE ANALYZED'.
10. Enter the name of the CO₂ data file in response to the prompt, 'ENTER THE CO2 SIGNAL FILE NAME'.
11. Enter the name of the O₂ data file in response to the prompt, 'ENTER THE O2 SIGNAL FILE NAME'. (If the O₂ file name begins with a O and the remaining portion of the file name is the same as the CO₂ file name, with the exception of the first letter, then simply press the CONTINUE key. Example: O₂ file name is O1106N175 and CO₂ file name is C1106N175)

12. Enter the name of the flow data file in response to the prompt, 'ENTER THE FLOW SIGNAL FILE NAME'. (If the flow file name begins with a V and the remaining portion of the file name is the same as the CO₂ file name, with the exception of the first letter, then simply press the CONTINUE key. Example: flow file name is V1106N175 and CO₂ file name is C1106N175)
13. Enter the name of the temperature data file in response to the prompt, 'ENTER THE FLOW TEMPERATURE SIGNAL FILE NAME'. (If the temperature file name begins with a T and the remaining portion of the file name is the same as the CO₂ file name, with the exception of the first letter, then simply press the CONTINUE key. Example: temperature file name is T1106N175 and CO₂ file name is C1106N175)
14. Proceed to step 22.
15. Determine if the calibration data are to be loaded and respond to the prompt, 'LOAD CALIBRATION FACTORS FROM DISK? (Y/N)'. If calibration data are not to be loaded, then answer no, 'N', and proceed to step 17.
16. Enter the name of the calibration file in response to the prompt, 'ENTER THE CALIBRATION FILE FILENAME.'. The specified calibration file will be loaded.
17. Enter the number of data points which were collected in response to the prompt, 'ENTER THE TOTAL NUMBER OF POINTS TO BE ANALYZED'.
18. Enter the name of the CO₂ data file in response to the prompt, 'ENTER THE CO2 SIGNAL FILE NAME'.
19. Enter the name of the O₂ data file in response to the prompt, 'ENTER THE O2 SIGNAL FILE NAME'. (If the O₂ file name begins with a O and the remaining portion of the file name is the same as the CO₂ file name, with the exception of the first letter, then simply press the CONTINUE key. Example: O₂ file name is O1106N175 and CO₂ file name is C1106N175)
20. Enter the name of the flow data file in response to the prompt,

'ENTER THE FLOW SIGNAL FILE NAME'. (If the flow file name begins with a V and the remaining portion of the file name is the same as the CO₂ file name, with the exception of the first letter, then simply press the CONTINUE key. Example: flow file name is V1106N175 and CO₂ file name is C1106N175)

21. Enter the name of the temperature data file in response to the prompt, 'ENTER THE FLOW TEMPERATURE SIGNAL FILE NAME'. (If the temperature file name begins with a T and the remaining portion of the file name is the same as the CO₂ file name, with the exception of the first letter, then simply press the CONTINUE key. Example: temperature file name is T1106N175 and CO₂ file name is C1106N175)
22. Enter the experimental time corresponding to when respiratory data collection began (generally 60 seconds).
23. Enter a comment which will be printed on the hard copy output.
24. Determine the sampling frequency used to sample the respiratory data. If this sampling frequency is 50 Hz, then answer no, 'N', in response to the prompt, 'CHANGE SAMPLING FREQUENCY FROM 50 HZ? (Y/N)' and proceed to step 26.
25. Enter the sampling frequency used to sample the respiratory data.
26. Determine if the GMS time delay is to be computed on a breath-by-breath basis or a fixed value used and respond to the prompt, 'B-BY-B TIME DELAY OR FIXED TIME DELAY (B/F)?'. For a breath-by-breath time delay perform step 27 and for the fixed time delay perform steps 28 and 29.
27. Enter the average time delay to be used in case a valid breath-by-breath time delay can not be determined. Continue to step 30.
28. The current time delay is displayed on the screen. If this time delay is to be used then answer yes, 'Y', to the prompt, 'CHANGE TIME DELAY? (Y/N)' and proceed to step 30.
29. Enter the desired time delay.

30. Determine if the flow is to be calculated using temperature and viscosity corrections and respond to the prompt, 'USE TEMP. AND VISCOSITY CORRECTIONS? (Y/N)'. If the corrections are not to be used enter no, 'N', and proceed to step 35.
31. The ambient conditions currently in memory are displayed on the screen. If these ambient conditions are correct, enter yes, 'Y', in response to the prompt, 'Do you wish to use the ambient conditions above? (Y/N)' and proceed to step 35.
32. Enter the barometric pressure (inches of mercury).
33. Enter the percent relative humidity.
34. Enter the room temperature ($^{\circ}$ F).
35. Determine if alveolar ventilation values based on FRC corrections are desired and respond to the prompt, 'Do you wish to use FRC corrections? (Y/N)'. Respond negatively, 'N', to this question as the FRC calculations are not implemented in this version of the ANALYSIS program. Refer to the reference [12].

Plotting the respiratory data

36. Determine if a plot of the respiratory data is desired and respond to the prompt, 'WOULD YOU LIKE A PLOT OF THE RESPIRATORY DATA? (Y/N)'. If a plot is not desired, enter no, 'N', and continue to step 42.
37. Enter the first data point to plot.
38. Enter the last data point to plot. At this time the maximum and minimum values for the specified range are calculated.
39. Once the maximum and minimum values have been determined you have approximately 20 seconds to determine the plotting device. At the end of this time and if no plotting device was specified the plot will automatically be sent to the 9826's screen. If the plotter is to be used, press the space bar. Set up the plotter. Enter 'PLOTTER' (all capitals) in response to the prompt, 'OUTPUT ON THE PLOTTER OR CRT? (PLOTTER/CRT)'.

If the plot was sent to the screen there, are two options for

obtaining a printed copy. For a small copy, press the 'SHIFT' key and 'DUMP GRAPHICS' key simultaneously. To obtain an expanded copy, type the command 'CALL Expanded_dump' and press the 'EXECUTE' key.

40. Press the 'CONTINUE' key.
41. Determine if additional plotting is desired and respond to the prompt, 'REDO GRAPHICS? (Y/N)'. If additional plots are desired enter yes, 'Y' and go to step 37.

Analyzing the respiratory data

42. Enter the first data point to analyze.
43. Enter the last data point to analyze.
44. Select whether the line-by-line output of the various respiratory volumes for each breath is desired. Generally this information is not needed and can be obtained later.
45. The calculation of the breath-by-breath respiratory parameters will begin. The present analysis routine can process 2000 points/min using the temperature and viscosity corrections and 7000 points/min without the corrections (these rates are based on the omission of the line-by-line output).
46. When the specified data range has been analyzed the mean values are printed.

Displaying the respiratory parameters

47. Determine if the calculated breath-by-breath respiratory parameters are to be displayed (printed or plotted) and respond to the prompt, 'DISPLAY THE BREATH-BY-BREATH DATA? (Y/N)'. If the results are not to be displayed, enter no, 'N', and proceed to step 68.
48. Select whether the parameters are to be plotted (two parameters per plot) or printed.
49. Select how the parameters are to be averaged. If displaying the individual breaths was selected proceed to step 55. If averaging of individual breaths was selected execute the next

- step (50) then proceed to step 55. If window averaging of the parameters was selected execute steps 51 thru 54.
50. Specify the number of breaths to be averaged together. Continue to step 55.
 51. Refer to Figure 2.2.3 for an illustration of the window averaging technique. Enter the windowing period. The windowing period is the distance (in time) the center of the window is slid.
 52. Enter the window width. The window width is the time span of the window. All breaths in that span are averaged.
 53. Enter the starting time. This is the time at which the center of the first window is placed.
 54. Enter the ending time. The window is slid until the center of the window occurs after the ending time.
 55. Determine if 'Bad Breaths' are to be included in the display. Bad breaths are those breaths which have an inspiratory or an expiratory tidal volume of less than 400 mL.
 56. If plotting of the parameters was selected in step 48, proceed to the next step. If printing of the parameters was selected the values will be printed, proceed to step 67.
 57. Enter the respiratory parameter to be displayed in the top plot.
 58. Enter the respiratory parameter to be displayed in the bottom plot.
 59. Determine if the plot is to be displayed on the 9826's screen or the plotted on the plotter.
 60. Two events may be displayed on the plot. If the events are not to be specified then proceed to step 65.
 61. Specify the time of the first event.
 62. Specify the the first event.
 63. Specify the time of the second event.

64. Specify the second event.
65. Enter a title for the plot.
66. If the plot was sent to the screen (as specified in step 59) there are two options for obtaining a printed copy. For a small copy press the 'SHIFT' key and 'DUMP GRAPHICS' key simultaneously. To obtain an expanded copy, type the command 'CALL Expanded_dump' and press the 'EXECUTE' key.
67. Additional display of the results is possible by responding to the prompt, 'Do you wish to exit to the analysis routine? (Y/N)' with a no, 'N'. Proceed to step 48.
68. The current subject's data can be re-analyzed by responding to the prompt, 'REDO ANALYSIS? (Y/N)' with a yes, 'Y'. Proceed to step 4. If the subject's data is not to be re-analyzed proceed to step 1.

A5.7 Storage and Display of the Heart Rate Data

The storage of the heart rate data will now be described. The display of the heart rate is accomplished with Sprick's Universal Plotting Routine [16].

1. Power up the Basic operating system as described in section A5.2 of this appendix. If the Basic operating system is powered up, execution of the AUTOSTart program may be accomplished by the command

LOAD "AUTOST:INTERNAL",1
2. Press the k_4 soft key labeled "STOREHR". This will cause the STOREHR program to be loaded.
3. Press the k_4 softkey labeled "STOREHR" again to continue with the storage of the heart rate values. STOREHR allows the return to the AUTOST program by pressing the k_9 softkey labeled "EXIT". This may be desired if the STOREHR key was accidentally pressed from the AUTOSTart program. If you wish to plot the heart rate values with Sprick's plotting routine press the k_1 softkey labeled 'PLOT' (refer to step 10 for instructions on how to label the X-axis of the plot).

4. Enter the file name which will contain the heart rate values.
5. Enter the heart rate value. Repeat this step for each value. Do not worry about mistakes, as they may be corrected later (step 6). If all values have been entered enter, a negative number.
6. Ten heart rate values are displayed on the screen. If you wish to alter any of these values, enter 'Y' for yes and continue to step 7. If you do not wish to alter any of the displayed values then enter 'N' for no. If all heart rate values have been displayed then continue to step 8, otherwise this step will be repeated for the next ten heart rate values.
7. Enter the number corresponding to the value you wish to change. Enter the new heart rate value. Return to step 6 for the display of the same ten heart rate values including the updated value.
8. The values are stored on the disk in the 8" disk drive.
9. If you wish to plot the heart rate values answer 'Y' for yes. If you wish to return to the AUTOSTart routine enter 'N' for no, and press the k_9 softkey labeled 'EXIT'. The AUTOSTart program will be loaded.
10. A message will be displayed on the screen instructing the use 'TIME' (all capital letters) as the X-axis of the plot to be obtained using Sprick's plotting routine. Press CONTINUE to proceed to the plotting routine. When using Sprick's plotting routine enter, 30 for the sampling period and Seconds for the X-axis units in addition to 'TIME' as the X-axis.

APPENDIX VI. PASCAL PROGRAM DOCUMENTATION AND LISTING

This appendix gives the details of the Pascal programs used by the CBRMS. The documentation for each program is broken down into descriptions of the individual Pascal procedures which make up the program. The variables for a particular procedure will be defined in that procedure's section. The procedures within each program are documented in alphabetical order. The variables within each procedure are also listed in alphabetical order.

A6.1 CAP2: a Pascal Routine for system Calibration

The Pascal program CAP2 (Calibration Program, version 2) is used to generate calibration factors which relate the sampled data to the analog respiratory signals. A flowchart for the program is given in Chapter 6, Section 1. The method used by CAP2 to control the DAM is described by Riblett [13]. The calibration file contents maintain the file structure specified by Riblett, one serial ASCII file, but has been expanded to contain additional data. The contents of the file in order are

```
Co2_dc_offset (4 ASCII bytes)
O2_dc_offset (4 ASCII bytes)
Bin_zero_flow (4 ASCII bytes)
Co2_cal (25 ASCII bytes)
O2_cal (25 ASCII bytes)
Non_C_I_flow_cal (25 ASCII bytes)
Non_C_E_flow_cal (25 ASCII bytes)
Time_delay (25 ASCII bytes)
S (4 ASCII bytes)
O1 (25 ASCII bytes)
Ta (25 ASCII bytes)
Tb (25 ASCII bytes)
Tc (25 ASCII bytes)
Date (25 ASCII bytes)
Corr_I_flow_cal (25 ASCII bytes)
Corr_E_flow_cal (25 ASCII bytes)
Pb (25 ASCII bytes)
Rel_humid (25 ASCII bytes)
Room_temp (25 ASCII bytes)
```

A description of each of the procedures used by CAP2 follows.

A6.1.1 Ask_Y_or_N Procedure

The procedure Ask_Y_or_N (Ask Yes or No) is used to obtain only a Yes or a No response to a question. The procedure returns the character 'Y' for a Yes response and the character 'N' for a No response.

Variables passed to the procedure

None

Variables returned by the procedure

Q - character, passed by reference.

Variable definitions

Q - string variable which contains a capital 'Y' for a Yes response or a capital 'N' for a No response.

A6.1.2 BEEP Procedure

The procedure BEEP sounds an audible beep. This procedure is used to gain the operator's attention.

Variables passed to the procedure

None

Variables returned by the procedure

None

Variable definitions

No variables used.

A6.1.3 BIT_HI and BIT_TST Procedures

BIT_HI and BIT_TEST are external assembly language procedures. These procedures are used to control the DAM. BIT_HI and BIT_TEST procedures are documented by Riblett [13].

A6.1.4 Calc_Incr_vol Procedure

The Calc_Incr_Vol (Calculate the Incremental Volume) procedure calculates an incremental volume which is used in integrating the flow. Calc_Incr_Vol is nested within the Flow calibration, Flow_cal, procedure. The Rel_viscos function is nested within Calc_Incr_Vol. The procedure uses a sample of the differential pressure signal, a sample of the temperature signal, and the ambient conditions to compute an incremental volume. Two types of incremental volumes are computed, one under STPD conditions the other under ITPnS conditions.

Variables passed to the procedure

Bin_delta_P - integer, passed by value.

Fh2o - real, passed by value.

T - real, passed by value.

Temperature - real, passed by value.

Variables returned by the procedure

Corr_Incr_vol - real, passed by reference.

Non_C_Incr_vol - real, passed by reference.

Variable definitions

Bin_delta_P - an integer variable which is proportional to the PTG differential pressure signal.

Corr_Incr_vol - a real variable proportional to the incremental volume under STPD conditions which flowed through the PTM during the sampling period.

Fh2o - a real variable equal to the fractional concentration of water vapor in the flow gas.

ITPnS_to_STPD - a real variable which converts the ITPnS volume to a STPD volume.

Non_C_Incr_vol - a real variable proportional to the incremental volume under ITPnS conditions which flowed through the PTM during the sampling period.

Rel_Viscosity - a real variable equal to the viscosity of the gas relative to the viscosity of room air under STPD conditions.

Temperature - a real variable equal to the temperature of the flow gas.

T - a real variable equal to the sampling period.

A6.1.5 CAP2 Procedure

The CAP2 procedure provides the main control of the the calibration program, CAP2. CAP2 calls the calibration routines; GASCAL, FLOWCAL, and TEMPCAL; and stores the calibration factors in a disk file. CAP2 also calls the Ask_Y_or_N, Beep, HOLD_UP, and Line_feed procedures.

Variables passed to the procedure

None

Variables returned by the procedure

The following variables are stored in the calibration file.

Bin_zero_flow - integer.
 Corr_E_flow_cal - real.
 Corr_I_flow_cal - real.
 Co2_cal - real.
 Co2_dc_offset - integer.
 Date - character string.
 Non_C_E_flow_cal - real.
 Non_C_I_flow_cal - real.
 O1 - real.
 O2_cal - real.
 O2_dc_offset - integer
 Pb - real.
 Rel_humid - real.
 Room_temp - real.
 S - integer.
 Ta - real.
 Tb - real.
 Tc - real.
 Time_delay - real.

Variable definitions

Bin_zero_flow - an integer variable equal to the average sampled value from the PTG channel with zero flow through the PTM.
 Corr_E_flow_cal - a real variable relating binary data obtained from the flow channel to the the PTM differential pressure generated by expiratory flows. This calibration factor

does use the temperature and viscosity corrections.

Corr_flag - a Boolean variable which is set to true when the flow signal is corrected to STPD conditions or is false if the flow signal is not corrected.

Corr_Incr_Vol - a real variable equal to the incremental volume obtained from one flow sample using temperature and viscosity corrections. Although this variable is declared within the context of CAP2 it is not used. However, the variable is used within FLOWCAL but is not declared. Therefore, the Corr_Incr_Vol declaration should be moved to the FLOWCAL procedure.

Corr_I_flow_cal - a real variable relating binary data obtained from the flow channel to the the PTM differential pressure generated by inspiratory flows. This calibration factor does use the temperature and viscosity corrections.

Co2_cal - a real variable relating the binary data collected from the O₂ channel to fractional CO₂.

Co2_dc_offset - an integer variable equal to the average binary value obtained from the CO₂ channel for room air concentration of CO₂.

Date - a string containing the date the calibration was performed.

Device_pointer - an integer which is used to indicate which mass storage device is to contain the calibration data.

F - a text variable associated with the calibration file specified by the string variable Fname.

Fname - a string containing the calibration file name.

Line1 - an integer array, of 24,000 elements, containing the sampled values obtained from channel 1, the CO₂ channel, of the DAM.

Line2 - an integer array, of 24,000 elements, containing the sampled values obtained from channel 2, the O₂ channel, of the DAM.

Line3 - an integer array, of 24,000 elements, containing the sampled values obtained from channel 3, the flow channel, of the DAM.

Line4 - an integer array, of 24,000 elements, containing the sampled values obtained from channel 4, the temperature

channel, of the DAM.

- MSI_devices - a string array containing three elements. These elements correspond to the three mass storage devices which can be used for the storage of the calibration data. Array element 1 contains #12 corresponding to platter 1 of the hard disk, element 2 contains #13 corresponding to platter 2 of the hard disk, and element 3 contains #7 corresponding to the 8-inch disk drive.
- Non_C_E_flow_cal - a real variable relating binary data obtained from the flow channel to the the PTM differential pressure generated by expiratory flows. This calibration factor does not use temperature or viscosity corrections.
- Non_C_I_flow_cal - a real variable relating binary data obtained from the flow channel to the the PTM differential pressure generated by inspiratory flows. This calibration factor does not use the temperature or viscosity corrections.
- Non_C_Incr_Vol - a real variable equal to the incremental volume obtained from one flow sample not using the temperature and viscosity corrections. Although this variable is declared within the context of CAP2 it is not used. However, the variable is used within FLOWCAL but is not declared. Therefore, the Non_C_Incr_Vol declaration should be moved to the FLOWCAL procedure.
- NSTRING- a string variable used to represent the ASCII value of an integer number.
- O1 - a real variable containing the fractional concentration of O₂ in the calibration gas.
- O2_cal - a real variable relating the binary data collected from the O₂ channel to fractional O₂.
- O2_dc_offset - an integer variable equal to the average binary value obtained from the O₂ channel when the GMS probe samples the calibration gas.
- Pb - a real variable set equal to the ambient barometric pressure (mm Hg).
- Q - string variable containing the response to a Yes or No question.
- Rel_humid - a real variable set equal to the relative humidity in the room air.

- Room_temp - a real variable set equal to the ambient temperature ($^{\circ}\text{C}$).
- RSTRING- a string variable used to represent the ASCII value of a real number.
- S - an integer variable set equal to the DAM sampling frequency (Hz).
- Sam - an integer variable equal to the number of samples to be collected from the DAM.
- Ta - a real variable equal to the computed second order coefficient of the function relating the sampled temperature data to the actual temperature in $^{\circ}\text{C}$.
- Tb - a real variable equal to the computed first order coefficient of the function relating the sampled temperature data to the actual temperature in $^{\circ}\text{C}$.
- Tc - a real variable equal to the computed zero order coefficient of the function relating the sampled temperature data to the actual temperature in $^{\circ}\text{C}$.
- TEMP - an integer variable needed by the STRWRITE function to convert the calibration data to ASCII strings.
- Time_delay - a real variable equal to the fixed GMS time delay used in the calibration routine. This value was retained to remain compatible with the calibration files generated by Creel's program [4].

A6.1.6 CLKSET Procedure

The procedure CLKSET sets the 8253 timer in the DAM with the desired sampling frequency. CLKSET is called by the main CAP2 procedure to set the DAM's sampling frequency. This procedure was designed by Riblett [13] and has no modifications for version 2 of the calibration program (CAP2).

Variables passed to the procedure

None

Variables returned by the procedure

S - integer, passed by reference.

Variable definitions

- F1 - an integer used to set the least significant byte of the 8253 timer.
- Fm - an integer used to set the most significant byte of the 8253 timer.
- S - an integer equal to the user specified sampling frequency.
- X - an integer variable used to set clock 1 of the 8253 timer.

A6.1.7 DATA_COLLECT Procedure

The procedure DATA_COLLECT provides the necessary control of the DAM to collect a set of data from four channels. DATA_COLLECT is called by the calibration procedures; GASCAL, FLOWCAL, and TEMPCAL; to sample the analog signals. DATA_COLLECT calls the assembly language procedures BIT_HI and BIT_TST to test the status of the DAM. This procedure was designed by Riblett [13] and has only minor modifications for version 2 of the calibration program (CAP2).

Variables passed to the procedure

- S - integer, passed by reference.
- Sam - integer, passed by reference.

Variables returned by the procedure

- Line1 - integer array, passed by reference.
- Line2 - integer array, passed by reference.
- Line3 - integer array, passed by reference.
- Line4 - integer array, passed by reference.

Variable definitions

- Chana - a constant value equal to 15359 which sets the DAM's analog multiplexer so that channel A is passed to the analog to digital converter.
- Chanb - a constant value equal to 13311 which sets the DAM's analog multiplexer so that channel B is passed to the analog to digital converter.
- Chanc - a constant value equal to 11263 which sets the DAM's analog multiplexer so that channel C is passed to the analog to digital converter.

- Chand - a constant value equal to 9215 which sets the DAM's analog multiplexer so that channel D is passed to the analog to digital converter.
- Del - an integer variable used in the delay loop that allows the sample and hold amplifiers to reach equilibrium once the hold command is given.
- I - an integer variable used as a loop counter and a pointer into the four data arrays during collection of the specified number of datum points.
- Line1 - an integer array containing the sampled data acquired from the CO₂ channel of the DAM.
- Line2 - an integer array containing the sampled data acquired from the O₂ channel of the DAM.
- Line3 - an integer array containing the sampled data acquired from the flow channel of the DAM.
- Line4 - an integer array containing the sampled data acquired from the temperature channel of the DAM.
- Mask - a constant value equal to 4095 which is used to mask all but the 12 least significant data bits.
- R4 - an integer variable which is loaded with the contents of register 4 of the GPIO.
- R6 - an integer variable which is loaded with the contents of register 6 of the GPIO.
- S - an integer equal to the user specified sampling frequency.
- Sam - an integer variable equal to the number of samples to be collected from the DAM.

A6.1.8 FLOWCAL Procedure

The procedure FLOWCAL calculates the calibration factors which relate the sampled data to the flow through the PTM. FLOWCAL has two procedures nested within it, Calc_Incr_Vol and Valid_pointer. FLOWCAL also calls the Ask_Y_or_N, Beep, DATA_COLLECT, HOLDUP, and Line_feed.

The flow calibration procedure uses several constant values which will need to be changed with a different experimental setup. These constant variables are

Corr_Pump_vol - the volume of the calibration pump converted to

STPD conditions, currently 0.560 L (STPD).

First_element - the first element of the water vapor pressure array, currently 0.

Last_element - the last element of the water vapor pressure array, currently 250.

Max_Temp - the maximum temperature represented in the water vapor pressure array, currently 45°C.

Min_Temp - the minimum temperature represented in the water vapor pressure array, currently 20°C.

Non_C_Pump_vol - the volume of the calibration pump under ATPS conditions, currently 0.647 L (ATPS).

Vap_File_name - the location and file name of the Pascal file containing the water vapor pressure array, currently '#14:VAP_PASCAL' (the hard disk, platter 3, under the file name VAP_PASCAL).

Variables passed to the procedure

Corr_flag - Boolean, passed by value.

Pb - real, passed by value.

Rel_humid - real, passed by value.

Room_temp - real, passed by value.

S - integer, passed by value.

Sam - integer, passed by value.

Ta - real, passed by value.

Tb - real, passed by value.

Tc - real, passed by value.

Variables returned by the procedure

Bin_zero_flow - integer, passed by reference.

Corr_F_flow_cal - real, passed by reference.

Corr_I_flow_cal - real, passed by reference.

Non_C_F_flow_cal - real, passed by reference.

Non_C_I_flow_cal - real, passed by reference.

Variable definitions

A - an integer variable used as an index into the sampled PTG signal array, Line3.

Array_pointer - an integer variable used as an index into the water vapor pressure array, Vap.

- Bin_delta_P - an integer variable equal to the binary differential pressure developed by the PTM. This is equal to the sampled value minus the binary value corresponding to zero differential pressure (zero flow).
- Bin_zero_flow - an integer variable equal to the average binary value sampled for zero flow.
- Corr_Aire - a real variable used in the expiratory integration loop to sum up the volume (binary representation) of air expired by the calibration pump using the flow calculated under STPD conditions.
- Corr_Airi - a real variable used in the inspiratory integration loop to sum up the volume (binary representation) of air inspired by the calibration pump using the flow calculated under STPD conditions.
- Corr_Avg_Vol_expr - a real variable equal to the average volume (binary representation) expired by the calibration pump calculated under STPD conditions.
- Corr_Avg_Vol_insp - a real variable equal to the average volume (binary representation) inspired by the calibration pump calculated under STPD conditions.
- Corr_E_flow_cal - a real variable equal to the flow calibration factor which converts the sampled expiratory flow (converted to STPD conditions) to the units of liters per second.
- Corr_flag - a Boolean variable indicating the use of temperature and viscosity corrections in the calibration of the flow signal.
- Corr_Incr_Vol - a real variable equal to the incremental volume obtained from one flow sample using temperature and viscosity corrections.
- Corr_I_flow_cal - a real variable equal to the flow calibration factor which converts the sampled inspiratory flow (converted to STPD conditions) to the units of liters per second.
- Corr_Pump_vol - a constant value equal to the volume of the calibration pump converted to STPD conditions, 0.560 L (STPD).
- Corr_Tot_vol_expr - a real variable equal to the total STPD

- volume expired by all pump cycles.
- Corr_Tot_vol_insp - a real variable equal to the total STPD volume inspired by all pump cycles.
- Fh2o - the fractional concentration of water vapor in the room air.
- First_element - a constant value equal to the first element of the water vapor pressure array, 0.
- I - an integer used as an array pointer into the flow signal array, Line3.
- Last_element - a constant value equal to the last element of the water vapor pressure array, 250.
- Line1 - an integer array, of 24,000 elements, containing the sampled values obtained from channel 1, the CO₂ channel, of the DAM.
- Line2 - an integer array, of 24,000 elements, containing the sampled values obtained from channel 2, the O₂ channel, of the DAM.
- Line3 - an integer array, of 24,000 elements, containing the sampled values obtained from channel 3, the flow channel, of the DAM.
- Line4 - an integer array, of 24,000 elements, containing the sampled values obtained from channel 4, the temperature channel, of the DAM.
- Max_Temp - a constant value equal to the maximum temperature represented in the water vapor pressure array, 45°C.
- Min_Temp - a constant value equal to the minimum temperature represented in the water vapor pressure array, 20°C.
- Non_C_Aire - a real variable used in the expiratory integration loop to sum up the volume (binary representation) of air expired by the calibration pump using the under flow calculated ATPS conditions.
- Non_C_Airi - a real variable used in the inspiratory integration loop to sum up the volume (binary representation) of air inspired by the calibration pump using the under flow calculated ATPS conditions.
- Non_C_Avg_Vol_expr - a real variable equal to the average volume (binary representation) expired by the calibration pump under ATPS conditions.

- Non_C_Avg_Vol_insp - a real variable equal to the average volume (binary representation) inspired by the calibration pump under ATPS conditions.
- Non_C_E_flow_cal - a real variable equal to the flow calibration factor which converts the sampled expiratory flow to the units of liters per second.
- Non_C_I_flow_cal - a real variable equal to the flow calibration factor which converts the sampled inspiratory flow to the units of liters per second.
- Non_C_Incr_Vol - a real variable equal to the incremental volume obtained from one flow sample not using the temperature and viscosity corrections.
- Non_C_Pump_vol - a constant value equal to the volume of the calibration pump under ATPS conditions, 0.647 L (ATPS).
- Non_C_Tot_vol_expr - a real variable equal to the total ATPS volume expired by all pump cycles.
- Non_C_Tot_vol_insp - a real variable equal to the total ATPS volume inspired by all pump cycles.
- No_breaths - an integer variable equal to the number of calibration pump cycles (breaths).
- Pb - a real variable equal to the barometric pressure.
- Rel_humid - a real variable equal to the ambient relative humidity.
- Room_temp - a real variable equal to the ambient temperature.
- S - an integer variable equal to the sampling frequency.
- Sam - an integer variable equal to the number of samples to be collected from the DAM.
- Still_calculating - a Boolean variable which is True as long as flow data remains to be integrated.
- Still_expire - a Boolean variable which is True when the flow is an expiratory flows.
- Still_inspire - a Boolean variable which is True when the flow is an inspiratory flows.
- T - a real variable equal to the sampling period (Seconds).
- Ta - a real variable equal to the computed second order coefficient of the function relating the sampled temperature data to the actual temperature in °C.
- Tb - a real variable equal to the computed first order

coefficient of the function relating the sampled temperature data to the actual temperature in $^{\circ}\text{C}$.

Tc - a real variable equal to the computed zero order coefficient of the function relating the sampled temperature data to the actual temperature in $^{\circ}\text{C}$.

Temperature - a real variable equal to the temperature of the flow signal. The temperature is calculated using the sampled temperature signal and the temperature calibration factors; Ta, Tb, and Tc.

Tot_zero - an integer variable equal to the sum of the sampled PTG data when the PTM is isolated from flow.

Vap - a real array containing the water vapor pressures values.

Vap_file - a real file containing the water vapor pressure values.

Vap_file_name - a constant character string containing the name of the water vapor pressure file, '#14:VAP_PASCAL'.

A6.1.9 GASCAL Procedure

The gas calibration procedure, GASCAL, calibrates the Perkin-Elmer gas mass spectrometer for both the CO_2 and O_2 channels. This procedure was designed by Riblett [13] and has only minor modifications for version 2 of the calibration program (CAP2).

Variables passed to the procedure

S - integer, passed by reference.

Sam - integer, passed by reference.

Variables returned by the procedure

Co2_cal - real, passed by value.

Co2_dc_offset - integer, passed by value.

O1 - real, passed by value.

O2_cal - real, passed by value.

O2_dc_offset - integer, passed by value.

Variable definitions

Avg_CO2_cal_gas - an integer variable containing the average of the sampled data obtained from the CO_2 channel when the GMS probe was placed in the calibration gas.

- Avg_CO2_room_air - an integer variable containing the average of the sampled data obtained from the CO₂ channel when the GMS probe was placed in room air.
- Avg_O2_cal_gas - an integer variable containing the average of the sampled data obtained from the O₂ channel when the GMS probe was placed in the calibration gas.
- Avg_O2_room_air - an integer variable containing the average of the sampled data obtained from the O₂ channel when the GMS probe was placed in room air.
- Ch - a real variable containing the fractional concentration of CO₂ in the calibration gas.
- Cl - a real variable containing the fractional concentration of CO₂ in room air.
- Co2_cal - a real variable relating the binary data collected from the CO₂ channel to fractional CO₂.
- Co2_dc_offset - an integer variable equal to the average binary value obtained from the CO₂ channel for room air concentration of CO₂.
- I - an integer variable used as a loop counter and a pointer into the data arrays.
- Line1 - an integer array, of 24,000 elements, containing the sampled values obtained from channel 1, the CO₂ channel, of the DAM.
- Line2 - an integer array, of 24,000 elements, containing the sampled values obtained from channel 2, the O₂ channel, of the DAM.
- Line3 - an integer array, of 24,000 elements, containing the sampled values obtained from channel 3, the flow channel, of the DAM.
- Line4 - an integer array, of 24,000 elements, containing the sampled values obtained from channel 4, the temperature channel, of the DAM.
- O1 - a real variable containing the fractional concentration of O₂ in the calibration gas.
- Oh - a real variable containing the fractional concentration of O₂ in room air.
- O2_cal - a real variable relating the binary data collected from the O₂ channel to fractional O₂.

- O2_dc_offset - an integer variable equal to the average binary value obtained from the O₂ channel for the O₂ concentration in the calibration gas.
- S - an integer variable equal to the sampling frequency.
- Sam - an integer variable equal to the number of samples to be collected from the DAM.

A6.1.10 HOLD UP Procedure

The hold up procedure, HOLD_UP, pauses program execution until the operator is ready to proceed. To continue program execution the operator must press the 'ENTER' key. This procedure was designed by Riblett [13] and has no modifications for version 2 of the calibration program (CAP2).

Variables passed to the procedure

None

Variables returned by the procedure

None

Variable definitions

No variables used.

A6.1.11 Line feed Procedure

The line feed procedure, Line_feed, sends a specified number of line feeds to the screen.

Variables passed to the procedure

I - integer, passed by value.

Variables returned by the procedure

None

Variable definitions

- I - an integer variable containing the number of line feeds to send to the screen.
- J - an integer variable used as a loop counter. J is incremented for each line feed which is sent until it is equal to the number of line feeds to be sent, I.

A6.1.12 Rel_viscos Function

The relative viscosity function, Rel_viscos, returns a real value equal to the viscosity of the flow gas relative to the the viscosity of room air under STPD conditions.

Variables passed to the procedure

FH2O - real, passed by value.

Temperature - real, passed by value.

Variables returned by the procedure

Not applicable.

Variable definitions

FCO2 - a real variable containing the fractional concentration of CO₂ in the room air taking into account the amount of water vapor in the room.

FH2O - a real variable containing the fractional concentration of water vapor in the room air.

FN2 - a real variable containing the fractional concentration of N₂ in the room air taking into account the amount of water vapor in the room.

FO2 - a real variable containing the fractional concentration of O₂ in the room air taking into account the amount of water vapor in the room.

Temperature - a real variable containing the instantaneous temperature of the flow gas.

Vis_CO2 - the viscosity of CO₂ in the flow gas.

Vis_H2O - the viscosity of H₂O in the flow gas.

Vis_N2 - the viscosity of N₂ in the flow gas.

Vis_O2 - the viscosity of O₂ in the flow gas.

Vis_STPD - the viscosity of room air under STPD conditions.

A6.1.13 TEMPCAL Procedure

The temperature calibration procedure, TEMP_CAL, calculates the calibration factors for the temperature transducer. The temperature calibration factors are the coefficients of a second order polynomial. This procedure was designed by Riblett [13] and has only minor modifications for version 2 of the calibration program (CAP2).

TEMP_CAL uses calibration parameters for the thermometer used to calibrate the thermocouple. These parameters allow a thermometer reading entered by the operator to be converted to the true temperature. When a new thermometer is used these calibration factors must be determined and placed in the TEMP_CAL procedure. The constant variable, Thermometer_cal_Y_int, must be set equal to the y intercept of the thermometer's calibration curve. The constant variable, Thermometer_cal_Slope, must be set equal to the slope of the calibration curve.

Variables passed to the procedure

- S - integer, passed by reference.
- Sam - integer, passed by reference.

Variables returned by the procedure

- Ta - real, passed by reference.
- Tb - real, passed by reference.
- Tc - real, passed by reference.

Variable definitions

- Bin_temp - a real two dimensional array (matrix) used to compute the temperature calibration coefficients.
- Bin_temp_inv - a real two dimensional array (matrix) equal to the inverse of Bin_temp.
- I - an integer variable used as a loop counter and a pointer into the temperature data array.
- Line1 - an integer array, of 24,000 elements, containing the sampled values obtained from channel 1, the CO₂ channel, of the DAM.
- Line2 - an integer array, of 24,000 elements, containing the sampled values obtained from channel 2, the O₂ channel, of the DAM.
- Line3 - an integer array, of 24,000 elements, containing the sampled values obtained from channel 3, the flow channel, of the DAM.
- Line4 - an integer array, of 24,000 elements, containing the sampled values obtained from channel 4, the temperature channel, of the DAM.
- Norm_a - a real variable containing the normal of the Bin_temp matrix.

- S - an integer variable equal to the sampling frequency.
- Sam - an integer variable equal to the number of samples to be collected from the DAM.
- Ta - a real variable equal to the computed second order coefficient of the function relating the sampled temperature data to the actual temperature in $^{\circ}\text{C}$.
- Tb - a real variable equal to the computed first order coefficient of the function relating the sampled temperature data to the actual temperature in $^{\circ}\text{C}$.
- Tc - a real variable equal to the computed zero order coefficient of the function relating the sampled temperature data to the actual temperature in $^{\circ}\text{C}$.
- Thermometer_cal_Slope - a constant variable equal to the slope of the calibration thermometer's calibration curve. With the current calibration thermometer this value is 1.0.
- Thermometer_cal_Y_int - a constant variable equal to the y intercept of the calibration thermometer's calibration curve. With the current calibration thermometer this value is -0.35.
- Thigh - a real variable equal to the temperature of the high temperature water bath.
- Thigh_bin - an integer variable equal to the average binary value of the sampled temperature data read for the high temperature bath.
- Tlow - a real variable equal to the temperature of the low temperature water bath.
- Tlow_bin - an integer variable equal to the average binary value of the sampled temperature data read for the low temperature bath.
- Tmid - a real variable equal to the temperature of the middle temperature water bath.
- Tmid_bin - an integer variable equal to the average binary value of the sampled temperature data read for the middle temperature bath.
- Tot_temp - an integer variable containing the sum of all samples read from the temperature channel.

A6.1.14 Valid_pointer Procedure

The procedure, Valid_pointer, is used to determine if the pointer into the saturated water vapor array is within the limits of the array. This procedure was originally designed with the conception that the fractional concentration of water vapor in the flow gas would be determined from the instantaneous temperature of the flow gas. In this instance, the Valid_pointer procedure would protect against temperatures computed from bad sampled temperature data points which result from 'glitches' by the DAM. In this case the computed temperature would point to a water vapor pressure value which is beyond the bounds of the water vapor pressure array and thereby causing the CAP2 program to 'crash'. The Valid_pointer procedure would protect against this possibility by checking to make certain the water vapor pointer is within bounds.

Variables passed to the procedure

Array_pointer - integer, passed by reference.

Variables returned by the procedure

Array_pointer - integer, passed by reference.

Variable definitions

Array_pointer - an integer variable containing the pointer into the water vapor pressure table that is to be checked.

A6.1.15. CAP2 Program Listing

```

SSYSprog ON$
$Lines 57$
$TABLE$
$REF 50$ \ {ALLOCATE ROOM FOR REFERENCE TABLE}
PROGRAM CAP2(INPUT,OUTPUT);

```

```

{*****

```

SYSTEM CALIBRATION ROUTINE

PASCAL REV 2.1 SOURCE FILENAME: CAP2.TEXT

Department of Electrical and Computer Engineering
 Kansas State University

REVISION	DATE	PROGRAMMER
-----	----	-----
1.0	JUNE 28, 1984	LOREN E. RIBLETT, JR.
2.0	August 31, 1984	Michael Masters

```

*****

```

PURPOSE

THIS ROUTINE PERFORMS ALL THE NECESSARY ACTIONS TO CALIBRATE THE BREATH-BY-BREATH RESPIRATORY SYSTEMS INSTRUMENTATION AND STORES THE CALIBRATION FACTORS IN ASCII CALIBRATION FILES.

ROUTINE(S) CALLED BY THIS ROUTINE

BIT_TST - 68000 ASSEMBLY MODULE THAT WAITS UNTIL THE EOC BIT ON THE DAM GOES HIGH, THEN LOW
 BIT_HI - 68000 ASSEMBLY MODULE THAT WAITS UNTIL THE EOC BIT ON THE DAM GOES LOW
 CLKSET - INTERNAL PROCEDURE THAT SETS THE 8253 TIMER CHIP FOR THE PROPER SAMPLING FREQUENCY
 HOLD_UP - INTERNAL PROCEDURE FOR TEMPORARY PAUSING OF PROGRAM OPERATION
 DATA_COLLECT - INTERNAL PROCEDURE THAT CONTROLS THE DAM IN

THE

PROPER FASHION TO COLLECT THE DESIRED NUMBER

OF

DATA POINTS

GASCAL - INTERNAL PROCEDURE THAT CALIBRATES THE PERKIN-ELMER GAS MASS SPECTROMETER
 FLOWCAL - INTERNAL PROCEDURE THAT CALIBRATES THE FLEISCH/GODART FLOW APPARATUS
 TEMPCAL - INTERNAL PROCEDURE THAT CALIBRATES THE RESPIRATORY TEMPERATURE TRANSDUCER

BEEP - Sounds an audible beep to alert the operator.

Ask_Y_or_N - Obtains the response to a yes or no question and allows only a 'Y', 'y', 'N', or 'n' response.

Line_feed - Sends a specified number of line feeds to the terminal.

```

*****

```

NOTE 1: THE DAM SHOULD BE CONNECTED TO THE HP9826 COMPUTER VIA A

GPIO INTERFACE AT SELECT CODE #12. THIS INSURES THE PROPER DEVICE ADDRESS FOR SENDING AND RECEIVING INFORMATION BETWEEN THE DAM AND THE HP9826.

- NOTE 2: TWO EXTERNAL 68000 ASSEMBLY LANGUAGE ROUTINES (BIT_TST AND BIT_HI) ARE UTILIZED BY CAP2 TO HANDLE THE HIGH SPEED REQUIREMENTS NEEDED TO MONITOR THE EOC (End Of Conversion) SIGNAL FROM THE DAM.
- NOTE 3: BEEP Procedure. The procedure BEEP was written to sound an audible beep to the operator. This is especially useful for prompting for operator input bring something to the operators attention.
- NOTE 4: Line_feed Procedure. The procedure Line_feed was written to send a specified number of line feeds to the terminal.
- NOTE 5: HOLD_UP PROCEDURE. THE PROCEDURE HOLDUP WAITS FOR THE OPERATOR TO PRESS THE ENTER KEY FOR EXECUTION TO RESUME.
- NOTE 6: Ask_Y_or_N Procedure. The procedure Ask_Y_or_N prompts the operator for either a yes response (a 'Y' or a 'y') or a no response ('N' or 'n'). The procedure continually prompts for a yes or no response until either the 'Y' key, 'y' key, 'N' key, or 'n' key is entered. The operatory response is returned.
- NOTE 7: CAP2'S CLKSET PROCEDURE SETS THE 8253 TIMER CHIP ON THE DAM TO THE DESIRED SAMPLING FREQUENCY. A MAXIMUM SAMPLING RATE OF 350 HZ IS RECOMMENDED. THIS VALUE MAY HAVE TO BE REDUCED IF SUBSTANTIAL ADDITIONS TO THE PROCEDURE DATA_COLLECT ARE MADE.
- NOTE 8: PROCEDURE DATA_COLLECT IS USED BY CAP2 TO SAMPLE THE NECESSARY CHANNELS FOR CALIBRATION PURPOSES. IT (DATA_COLLECT) IS IDENTICAL TO THE DATA_COLLECT PROCEDURE USED BY DAP.CODE.
- NOTE 9: PROCEDURE GASCAL IS DESIGNED TO CALIBRATE THE PERKIN-ELMER GAS MASS SPECTROMETER FOR BOTH THE CO2 (CHANNEL 1) AND O2 (CHANNEL 2) DAM CHANNELS.
- NOTE 10: PROCEDURE FLOWCAL IS USED TO CALIBRATE THE FLEISCH/GODART PNEUMOTACH ASSEMBLY. FLOWCAL DETERMINES NOT ONLY THE BINARY VALUE FOR ZERO FLOW BUT ALSO COMPUTES INSPIRATORY AND EXPIRATORY FLOW CALIBRATION FACTORS FOR BOTH THE NON-CORRECTED DATA AND THE CORRECTED DATA.
- NOTE 11: PROCEDURE TEMPICAL IS DESIGNED TO CALIBRATE THE THERMOCOUPLE FOR MEASURING RESPIRATORY TEMPERATURE. TEMPICAL DETERMINES A 2ND ORDER EQUATION FOR CONVERTING BINARY DAM FIGURES TO ACTUAL TEMPERATURE VALUES.
- NOTE 12: CAP2 CONVERTS ALL THE CALIBRATION FACTORS TO ASCII UNITS AND STORES THESE UNITS IN A SINGLE ASCII DATA FILE
- NOTE 13: SEE EXTERNAL PROGRAM DOCUMENTATION FOR MORE DETAILS.

```
*****}
{*** LOAD NECESSARY LIBRARY MODULES ***}
IMPORT IODECLARATIONS,
      GENERAL_0,
      IOCOMASM;
```

```
{** SET PROGRAM CONSTANTS **}
```

```
CONST Time_delay=380.0;      {AVERAGE TIME DELAY STORED WITH CAL DATA}
```

```
{** DECLARE FOUR LARGE EXTERNAL DATA ARRAYS AND POINTERS **}
```

```
TYPE L1=ARRAY [1..5000] OF INTEGER;      {CO2 CHANNEL DATA ARRAY}
    PT1=^L1;      {POINTER TO ARRAY L1}
    L2=ARRAY [1..5000] OF INTEGER;      {O2 CHANNEL DATA ARRAY}
    PT2=^L2;      {POINTER TO ARRAY L2}
    L3=ARRAY [1..5000] OF INTEGER;      {FLOW CHANNEL DATA ARRAY}
    PT3=^L3;      {POINTER TO ARRAY L3}
    L4=ARRAY [1..5000] OF INTEGER;      {TEMPERATURE CHANNEL DATA ARRAY}
    PT4=^L4;      {POINTER TO ARRAY L4}
```

```
{** DECLARE PROGRAM VARIABLES **}
```

```
VAR S,Sam,TEMP,Co2_dc_offset,
    O2_dc_offset,Bin_zero_flow,
    GPINT[7077890] :      INTEGER;
    O1,Co2_cal,O2_cal,
    Non_C_I_flow_cal,Non_C_E_flow_cal,
    Corr_I_flow_cal,Corr_E_flow_cal,
    Ta,Tb,Tc :      REAL;
    NSTRING :      STRING [4];
    Q :      STRING [5];
    Date :      STRING [25];
    Fname :      STRING [16];
    RSTRING :      STRING [25];
    F :      TEXT;
    Line1: PT1;
    Line2: PT2;
    Line3: PT3;
    Line4: PT4;
    Corr_flag :      BOOLEAN;
    Corr_Incr_Vol,
    Non_C_Incr_Vol,
    Rel_humid,Pb,Room_temp :      REAL;
    Device_pointer :      INTEGER;
    Msi_devices :      ARRAY [1..3] OF STRING [4];
```

```
{
```

```
*** DECLARE EXTERNAL 68000 ASSEMBLY MODULES
```

```
PROCEDURE BIT_TST;EXTERNAL;      {WAITS UNTIL EOC BIT GOES HIGH, THEN LOW}
PROCEDURE BIT_HI;EXTERNAL;      {WAITS UNTIL EOC BIT IS LOW}
```

```
PROCEDURE BEEP;
```

```
{*****
*****
*
*      Procedure Name:   BEEP
*
*      File Name:       CAP2
*
*      REVISION          DATE          PROGRAMMER
*      -----          -
```

1.0

-22-Sept-84

Michael Masters.

Procedure discription:

This procedure sounds an audible beep to the operator.

Calling sequence:

BEEP;

Parameters supplied by the calling routine.

None

Parameters returned to the calling routine.

None

```

BEGIN
PROMPT (CHR(7));
END;

```

```

PROCEDURE Line_feed(I : INTEGER);

```

```

{*****
*****
*****

```

```

* Procedure Name: Line feed

```

```

* File Name: CAP2

```

```

* REVISION

```

```

* DATE

```

```

* PROGRAMMER

```

```

* -----
* 1.0

```

```

* 22-Sept-84

```

```

* Michael Masters.

```

```

* Procedure discription:

```

```

* This procedure sends a specified number of line feeds to the
* terminal.

```

```

* Calling sequence:

```

```

* Line_feed(i);

```

```

* Parameters supplied by the calling routine.

```

```

* I - is an integer value parameter corresponding to the
* number of line feeds to be sent to the terminal.

```

```

* Parameters returned to the calling routine.

```

```

* None

```

```

VAR J : INTEGER;

```

```

BEGIN

```

```

FOR J := 1 TO I DO

```

```

{Send the specified number of line feeds}

```

```

      BEGIN
      PROMPT (CHR(10));    {Send the line feed}
      END;
END;
=====

{
*** DECLARE PROCEDURE FOR PAUSING PROGRAM OPERATION
}
PROCEDURE HOLD_UP;
BEGIN
  PROMPT ('PRESS ENTER TO CONTINUE. ');    {DISPLAY PROMPT ON CRT}
  BEEP;
  READLN;    {WAIT UNTIL 'ENTER' IS PRESSED}
END; {HOLD_UP END}
=====

```

```

PROCEDURE Ask_Y_or_N(VAR Q:STRING);
*****
*
*      Procedure Name:   Ask yes or no question.
*
*      File Name:       CAP2
*
*      REVISION          DATE          PROGRAMMER
*      -----          -
*      1.0              22-Sept-84     Michael Masters.
*
*      Procedure discription:
*      This procedure prompts the operator for a yes or no response.
*
*      Calling sequence:
*      Ask_Y_or_N(Q);
*
*      Parameters supplied by the calling routine.
*      None
*
*      Parameters returned to the calling routine.
*      Q - a string reference parameter. Returns the value 'Y' for
*          a yes response and the value 'N' for a no response.
*
*
*****
=====
}

```

```

BEGIN
REPEAT
  BEEP;
  READLN(Q);
  IF Q='y' THEN Q := 'Y';
  IF Q='n' THEN Q := 'N';
  IF NOT((Q='Y') OR (Q='N')) THEN
    BEGIN
      WRITELN('Invalid response. Enter Y (yes) or N (no).');
    END
  UNTIL (Q='Y') OR (Q='N') ;
END; {Ask_Y_or_N}

```

```

{
*** DECLARE PROCEDURE TO SET DAM CLOCK
}

PROCEDURE CLKSET(VAR S:INTEGER);    {PASS SAMPLING FREQUENCY (S)}
VAR X,Fm,F1:INTEGER;
BEGIN
{
*** HAVE USER ENTER THE SAMPLING FREQUENCY
}
PROMPT ('ENTER SAMPLING FREQUENCY: ');
BEEP;
READLN(S);
{
*** DETERMINE 16-BIT COUNTER VALUE FOR CLK1 IN 8253 TIMER CHIP
}
X:=1000000 DIV 2 DIV S;
IF X>=256 THEN
BEGIN
Fm:=X DIV 256;
F1:=X-256*Fm;
END
ELSE
BEGIN
Fm:=0;
F1:=X;
END;
{
*** SET COUNTER 0 IN 8253 TIMER TO MODE 3
}
IOCONTROL(12,3,15678); {11110100111110}
IOCONTROL(12,3,15422); {11110000111110}
IOCONTROL(12,3,15670); {11110100110110}
{
*** SET COUNTER 1 IN 8253 TIMER TO MODE 2
}
IOCONTROL(12,3,15740); {11110101111100}
IOCONTROL(12,3,15484); {11110001111100}
IOCONTROL(12,3,15732); {11110101110100}
{
*** LOAD LSB OF COUNTER 0
}
IOCONTROL(12,3,9474); {10010100000010}
IOCONTROL(12,3,9218); {10010000000010}
IOCONTROL(12,3,9474); {10010100000010}
{
*** LOAD MSB OF COUNTER 0
}
IOCONTROL(12,3,9472); {10010100000000}
IOCONTROL(12,3,9216); {10010000000000}
IOCONTROL(12,3,9472); {10010100000000}
{
*** LOAD LSB OF COUNTER 1
}
IOCONTROL(12,3,13568+F1); {11010100000000}
IOCONTROL(12,3,13312+F1); {11010000000000}
IOCONTROL(12,3,13568+F1); {11010100000000}
{
*** LOAD MSB OF COUNTER 1
}

```

```

    }
    IOCONTROL(12,3,13568+Fm); {11010100000000}
    IOCONTROL(12,3,13312+Fm); {11010000000000}
    IOCONTROL(12,3,13568+Fm); {11010100000000}
END; {CLKSET END}
{
*** DECLARE PROCEDURE FOR COLLECTING FOUR CHANNELS OF DAM DATA
}
PROCEDURE DATA_COLLECT(VAR Sam,S:INTEGER;
                        VAR LINE1:PT1;VAR LINE2:PT2;
                        VAR LINE3:PT3;VAR LINE4:PT4);
VAR I,R6,DeI,R4:INTEGER;

    {BIT PATTERNS NECESSARY TO SET THE CHANNEL MULTIPLEXER}
CONST Chna=15359;Chnb=13311;
     Chnc=11263;Chnd=9215;

    Mask=4095;      {MASKS OFF ALL BUT 12 DATA BITS IN STATUS WORD}
{
*** MAIN LOOP FOR FOUR CHANNEL DATA ACQUISITION
}
BEGIN {DATA_COLLECT}
    Writeln('NOW COLLECTING DATA... please wait patiently. ');
    Writeln('Collecting ',Sam:5,' samples.
              This will take ',Sam DIV S:4,' Sec');
    FOR I:=1 TO Sam DO
        BEGIN
            {
            *** PUT S/H AMPS IN TRACKING MODE AND SELECT CHANNEL A
            }
            R6:=BINAND(15360,Chna);
            R6:=BINCMP(R6);
            IOCONTROL(12,3,R6);
            {
            *** GIVE S/H AMPS TIME TO TRACK INPUT SIGNALS
            }
            DeI:=15;
            WHILE DeI>0 DO
                BEGIN
                    DeI:=DeI-1;
                END;
            {
            *** SELECT CHANNEL A ON MULTIPLEXER AND CONVERT SIGNAL HIGH
            }
            R6:=BINAND(7168,Chna);
            R6:=BINCMP(R6);
            IOCONTROL(12,3,R6);
            {
            *** SELECT CHANNEL A ON MULTIPLEXER AND CONVERT SIGNAL LOW
            }
            R6:=BINAND(7680,Chna); {SEND CONVERT...}
            R6:=BINCMP(R6);        {...PULSE}
            IOCONTROL(12,3,R6);
            {
            *** SELECT CHANNEL A ON MULTIPLEXER AND CONVERT SIGNAL HIGH
            }
            R6:=BINAND(7168,Chna); {RETURN TO...}
            R6:=BINCMP(R6);        {...NORMAL}
            IOCONTROL(12,3,R6);
            {
            *** WAIT FOR EOC LINE TO GO LOW
            }
        }
        BIT_HI;
        {
        *** READ GPIO STATUS REGISTER AND KEEP ONLY 12 BITS

```



```

}
R4:=IOSTATUS(12,3);
R4:=R4 DIV 4;
R4:=BINAND(MASK,R4);
Line1^[1]:=R4;
{
*** SELECT CHANNEL B ON MULTIPLEXER AND CONVERT SIGNAL HIGH
}
R6:=BINAND(7168,Chnb);
R6:=BINCMP(R6);
IOCONTROL(12,3,R6);
{
*** SELECT CHANNEL B ON MULTIPLEXER AND CONVERT SIGNAL LOW
}
R6:=BINAND(7680,Chnb);
R6:=BINCMP(R6);
IOCONTROL(12,3,R6);
{
*** SELECT CHANNEL B ON MULTIPLEXER AND CONVERT SIGNAL HIGH
}
R6:=BINAND(7168,Chnb);
R6:=BINCMP(R6);
IOCONTROL(12,3,R6);
{
*** WAIT FOR EOC SIGNAL TO GO LOW
}
BIT_HI;
{
*** READ GPIO STATUS REGISTER AND KEEP ONLY 12 BITS
}
R4:=IOSTATUS(12,3);
R4:=R4 DIV 4;
R4:=BINAND(Mask,R4);
Line2^[1]:=R4;
{
*** SELECT CHANNEL C ON MULTIPLEXER AND CONVERT SIGNAL HIGH
}
R6:=BINAND(7168,Chnc);
R6:=BINCMP(R6);
IOCONTROL(12,3,R6);
{
*** SELECT CHANNEL C ON MULTIPLEXER AND CONVERT SIGNAL LOW
}
R6:=BINAND(7680,Chnc);
R6:=BINCMP(R6);
IOCONTROL(12,3,R6);
{
*** SELECT CHANNEL C ON MULTIPLEXER AND CONVERT SIGNAL HIGH
}
R6:=BINAND(7168,Chnc);
R6:=BINCMP(R6);
IOCONTROL(12,3,R6);
{
*** WAIT FOR EOC SIGNAL TO GO LOW
}
BIT_HI;
{
*** READ GPIO STATUS REGISTER AND KEEP ONLY 12 BITS
}
R4:=IOSTATUS(12,3);
R4:=R4 DIV 4;
R4:=BINAND(Mask,R4);
Line3^[1]:=R4;
{
*** SELECT CHANNEL D ON MULTIPLEXER AND CONVERT SIGNAL HIGH
}

```

```

    }
    R6:=BINAND(7168,Chnd);
    R6:=BINCOMP(R6);
    IOCONTROL(12,3,R6);
    {
    *** SELECT CHANNEL D ON MULTIPLEXER AND CONVERT SIGNAL LOW
    }
    R6:=BINAND(7680,Chnd);
    R6:=BINCOMP(R6);
    IOCONTROL(12,3,R6);
    {
    *** SELECT CHANNEL D ON MULTIPLEXER AND CONVERT SIGNAL HIGH
    }
    R6:=BINAND(7168,Chnd);
    R6:=BINCOMP(R6);
    IOCONTROL(12,3,R6);
    {
    *** WAIT FOR EOC SIGNAL TO GO LOW
    }
    BIT_HI;
    {
    *** READ GPIO STATUS REGISTER AND KEEP ONLY 12 BITS
    }
    R4:=IOSTATUS(12,3);
    R4:=R4 DIV 4;
    R4:=BINAND(Mask,R4);
    Line4^1:=R4;
    {
    *** WAIT FOR EOC SIGNAL TO GO HIGH, THEN LOW
    }
    BIT_TST;
    {
    *** LOOP BACK UNTIL ALL POINTS ARE COLLECTED
    }
    END;
END; {DATA_COLLECT}
}
*** DECLARE PROCEDURE FOR CALIBRATING THE PERKIN-ELMER GAS MASS SPECTROMETER
}
PROCEDURE GASCAL(VAR O1,Co2_cal,O2_cal          :      REAL;
                 VAR Co2_dc_offset,O2_dc_offset :      INTEGER;
                 Sam,S                          :      INTEGER);
VAR I,Avg_CO2_room_air,Avg_O2_room_air,
    Avg_CO2_cal_gas,Avg_O2_cal_gas           :      INTEGER;
    Cl,Ch,Oh                                :      REAL;
{
*** BEGIN GMS CALIBRATION
}
BEGIN {GASCAL}
{
    *** INSTRUCT USER TO CONNECT GMS PROBE FOR 21% O2 AND 0% CO2
    }
    WRITELN('CONNECT THE MASS SPECTROMETER PROBE TO ROOM AIR. ');
    Line_feed(1);
    {
    *** OBTAIN ACTUAL O2 AND CO2 CONCENTRATIONS FROM GMS FRONT PANEL
    }
    PROMPT ('ENTER ACTUAL PERCENT CO2 CONCENTRATION.  ');
    BEEP;
    READLN(C1);
    CL := CL/100.0;
    PROMPT ('ENTER ACTUAL PERCENT O2 CONCENTRATION.  ');
    BEEP;
    READLN(Oh);
    Oh := Oh/100.0;

```

```

{
*** FOLLOWING A CARRIAGE RETURN, TAKE 500 DATA POINTS ON CO2 AND O2
*** CHANNELS
}
HOLD_UP;
DATA_COLLECT(Sam,S,LINE1,LINE2,LINE3,LINE4);
{
*** COMPUTE AVERAGE BINARY VALUES FOR O2 AND CO2 CHANNELS
}
Avg_CO2_room_air:=LINE1^[1];
Avg_O2_room_air:=LINE2^[1];
FOR I:=2 TO Sam DO
  BEGIN
    Avg_CO2_room_air:=Avg_CO2_room_air+LINE1^[I];
    Avg_O2_room_air:=Avg_O2_room_air+LINE2^[I];
  END;
Avg_CO2_room_air:=Avg_CO2_room_air DIV Sam;
Co2_dc_offset:=Avg_CO2_room_air;
Avg_O2_room_air:=Avg_O2_room_air DIV Sam;
{
*** DISPLAY AVERAGES ON HP9826 CRT
}
Line_feed(1);
WRITELN('Average binary values read for room air');
WRITELN('   CO2: ',Avg_CO2_room_air);
WRITELN('   O2: ',Avg_O2_room_air);
{
*** INSTRUCT THE USER TO CONNECT GMS PROBE TO THE CALIBRATIO GAS.
}
WRITELN('CONNECT THE GMS PROBE TO THE CALIBRATION GAS. ');
Line_feed(1);
{
*** OBTAIN ACTUAL O2 AND CO2 CONCENTRATIONS FROM GMS FRONT PANEL
}
PROMPT('ENTER ACTUAL PERCENT CO2 CONCENTRATION. ');
BEEP;
READLN(Ch);
Ch := Ch / 100.0;
PROMPT('ENTER ACTUAL PERCENT O2 CONCENTRATION. ');
BEEP;
READLN(O1);
O1 := O1 / 100.0;
{
*** TAKE 500 DATA POINTS ON CO2 AND O2 CHANNELS
}
HOLD_UP;
DATA_COLLECT(Sam,S,LINE1,LINE2,LINE3,LINE4);
{
*** COMPUTE AVERAGE BINARY VALUES FOR O2 AND CO2 CHANNELS
}
Avg_CO2_cal_gas:=LINE1^[1];
Avg_O2_cal_gas:=LINE2^[1];
FOR I:=2 TO Sam DO
  BEGIN
    Avg_CO2_cal_gas:=Avg_CO2_cal_gas+LINE1^[I];
    Avg_O2_cal_gas:=Avg_O2_cal_gas+LINE2^[I];
  END;
Avg_CO2_cal_gas:=Avg_CO2_cal_gas DIV Sam;
Avg_O2_cal_gas:= Avg_O2_cal_gas DIV Sam;
O2_dc_offset:=Avg_O2_cal_gas;
{
*** DISPLAY AVERAGES ON HP9826 CRT
}
Line_feed(1);
WRITELN('Average binary values read for room air');

```

```

WRITELN('    CO2: ',Avg_CO2_cal_gas);
WRITELN('    O2: ',Avg_O2_cal_gas);
{
*** COMPUTE CO2 AND O2 CALIBRATION FACTORS FROM THESE AVERAGES
}
Co2_cal :=
ROUND((Ch-C1)/(Avg_CO2_cal_gas-Avg_CO2_room_air)*10000000)/10000000;
O2_cal :=
ROUND((Oh-O1)/(Avg_O2_room_air-Avg_O2_cal_gas)*10000000)/10000000;
{
*** DISPLAY CO2 AND O2 CALIBRATION FACTORS ON 9826 CRT
}
WRITELN('CO2 DC OFFSET =',Co2_dc_offset);
WRITELN('O2 DC OFFSET =',O2_dc_offset);
WRITELN('CO2 CALIBRATION FACTOR =',Co2_cal);
WRITELN('O2 CALIBRATION FACTOR =',O2_cal);
END; {GASCAL}

```

```

PROCEDURE FLOWCAL(VAR Non_C_I_flow_cal,Non_C_E_flow_cal,
                  Corr_I_flow_cal,Corr_E_flow_cal : REAL;
                  VAR Bin_zero_flow : INTEGER;
                  Sam,S : INTEGER;
                  Corr_flag : BOOLEAN;
                  Rel_humid,Pb,Room_temp,Ta,Tb,Tc : REAL);
{*****}

```

Procedure Name: FLOWCAL

File Name: CAP2

REVISION

DATE

PROGRAMMER

1.0

June 28, 1984

Loren Riblett Jr.

2.0

Sept. 6, 1984

Michael Masters

Procedure description:

FLOWCAL calculates the calibration factors for the flow signal. The binary value of zero flow is first determined and then two sets of flow calibration factors are determined. The first two flow calcs do not use any temperature or gas viscosity corrections in their determination. The second set uses incremental point by point temperature and viscosity correction in their determination.

Parameters supplied by the calling routine.

(all parameters passed to FLOWCAL are value parameters.)

Sam - The number of samples which is collected.

S - Sampling frequency.

Corr_flag - Indicates if temperature and viscosity corrections are requested.

TRUE - correct for temp. and visc.

FALSE - no corrections.

Rel_humid - The relative humidity of the ambient air.

Pb - The ambient barometric pressure.

```

*
* - Parameters returned to the calling routine.
* (all parameters returned are reference parameters.)
*
* Non_C_I_flow_cal - the inspiratory flow calibration factor
* which does not use temp. and visc. corrections.
*
* Non_C_E_flow_cal - the expiratory flow calibration factor
* which does not use temp. and visc. corrections.
*
* Corr_I_flow_cal - The inspiratory flow calibration factor
* which uses the temp. and visc. corrections.
*
* Corr_E_flow_cal - The expiratory flow calibration factor
* which uses the temp. and visc. corrections.
*
* Bin_zero_flow - The binary value corresponding to zero
* flow input.
*
* Routines called:
*
* Calc_incr_vol - calculates the incremental volume of the
* sample.
*
* Valid_pointer - Sees if the pointer to the vapor pressure
* array is valid.
*
*=====*
```

```

CONST Non_C_Pump_Vol = 0.647; {The volume of the pump under ambient
                                conditions.}
Corr_Pump_Vol = 0.560; {The volume of the pump under STPD
                        conditions.}
Min_Temp = 20; {degrees C. The minimum temperature for which
                the saturated vapor pressure may be
                found in the vapor pressure array.}
Max_Temp = 45; {degrees C. The maximum temperature for which
                the saturated vapor pressure may be
                found in the vapor pressure array.}
First_element = 0; {The first element in the vapor
                   pressure file.}
Last_element = 10 * (Max_Temp - Min_Temp);
                {The last element in the vapor
                pressure file.}
Vap_File_name = '#14:VAP_PASCAL'; {The vapor pressure file location
                                   and name.}

VAR I,Tot_zero,No_breaths,A,
    Array_pointer,Bin_delta_P : INTEGER;
    Still_calculating,Still_inspire,
    Still_expire : BOOLEAN;
    T,Non_C_Tot_vol_insp,
    Non_C_Tot_vol_expr,
    Corr_Tot_vol_insp,
    Corr_Tot_vol_expr,
    Non_C_Airi,Non_C_Aire,
    Corr_Airi,Corr_Aire,
    Non_C_Avg_Vol_insp,
    Non_C_Avg_Vol_expr,
    Corr_Avg_Vol_insp,
    Corr_Avg_Vol_expr,Fh2o,
    Temperature : REAL;
    Vap : ARRAY[First_element..Last_element] OF REAL;
    Vap_File : FILE OF REAL;
```

```

PROCEDURE Valid_pointer ( VAR Array_pointer      :      INTEGER);
{*****}
*****
*
*      Procedure Name: Valid_pointer
*
*      File Name:      CAP2
*
*      REVISION          DATE          PROGRAMMER
*      -----          -
*      1.0              22-Sept-84      Michael Masters
*
*      Program discription:
*
*          This procedure determines if the vapor pressure array
*          pointer is within the proper range.
*
*      Calling sequence:
*
*          Valid_pointer(Array_pointer);
*
*      Parameters passed from and returned to the calling routine.
*
*          Array_pointer - The pointer into the vapor pressure
*                          array. If it is not within the valid range it is made
*                          to point at either the first element or the last
*                          element. ( A reference parameter.)
*
*=====
*****}
BEGIN
  IF Array_pointer < First_element THEN      { The pointer is invalid.}
    BEGIN
      Array_pointer := First_element;
    END
  ELSE
    { The pointer may be valid.}
    BEGIN
      IF Array_pointer > Last_element THEN
        BEGIN
          { The pointer is invalid.}
          Array_pointer := last_element;
        END
      ELSE
        BEGIN
          { The vapor pressure pointer is valid so leave it alone.}
          END;
        END;
      END; {Valid_pointer}
    }
  -----
}

PROCEDURE Calc_Incr_vol(Bin_delta_P      :      INTEGER;
                        Fh2o,Temperature,T :      REAL;
                        VAR Corr_Incr_vol,Non_C_Incr_vol :      REAL);
{*****}

```

```

*****
*
* Program Name:   Calc_Incr_vol
*
* File Name:     CAP2
*
* REVISION       DATE           PROGRAMMER
* -----       -
* 1.0            22-Sept-84     Michael Masters.
*
*
* Program discription:
*
* This proceedure calculates the incremental volume of the sample
* from the measured binary differential pressure. The non corrected
* flow is assumed to be directly propotional to the pressure differ-
* ential so that the binary incremental volume is equal to the
* sampled value multiplied by the sampling period.
*
* The corrected volume is calculated by dividing the differential
* pressure by the relative viscosity of the gas to obtain the binary
* flow. The incremental volume is then calculated by multiplying by
* the sampling period. This volume is then converted to STPD con-
* ditions.
*
* If temperature and viscosity corrections are not desired then the
* corrected volume is set equal to the non corrected volume.
*
* Calling sequence:
*   Calc_Incr_vol( Bin_delta_P,Pb,Fh2o,Temperature,T
*                 Corr_Incr_vol,Non_C_Incr_vol );
*
* Parameters supplied by the calling routine.
*   (all parameters are value parameters)
*
*   Bin_delta_P   - The sampled pressure differential from LINE3
*
*   Fh2o          - The fractional content of water vapor.
*
*   Temperature   - The temperature of the flow gas obtained
*                   from the temperature transducer.
*
*   T             - The sampling period.
*
* Parameters returned to the calling routine.
*   (all parameters are reference parameters)
*
*   Corr_Incr_vol - The calculated incremental volume under STPD
*                   conditions which was obtained using vis-
*                   cosity corrections on the measured pressure
*                   differential. If corrections are not
*                   requested then it is equal to the non corr-
*                   ected volume.
*
*   Non_C_Incr_vol - The non corrected incremental volume.
*
* Routines called:
*   The function Rel_viscos.
*
*****
*
* VAR Rel_viscosity,ITPnS_to_STPD      :      REAL;
*
* }

```



```

FUNCTION Rel_viscos ( Temperature,Fh2o      :   REAL)      :   REAL;
{*****}
*
*   Function Name: Rel_viscos
*
*   File Name:      CAP2.TEXT
*
*   REVISION          DATE          PROGRAMMER
*   -----          -
*   1.0              Sept 6, 1984    Michael Masters
*
*   Function discription:
*       Rel_viscos returns the real value equal to the relative vis-
*       cosity of the gas.
*
*   Parameters supplied by the calling routine.
*       (all parameters are value parameters.)
*
*       Temperature - The temperature in degrees Centigrade.
*
*       Fh2o        - The fraction of water vapor in the room air.
*
*   =====}
*****}

VAR      Vis_H2O,Vis_O2,Vis_CO2,
        Vis_N2,Vis_STPD,FO2,FCO2,FN2      :      REAL;
BEGIN {FUNCTION Rel_viscos}
  Vis_STPD := 170.17502;

{
    Calculate the fractional concentrations of oxygen,
    carbon dioxide, and nitrogen in the wet room air.}

  FO2 := 0.2109 * ( 1.0 - FH2O);
  FCO2 := 0.0004 * ( 1.0 - FH2O);
  FN2 := (1.0 - FO2 - FCO2 - FH2O);

{
    Calculate the individual viscosities.
    }
  Vis_N2 := 165.4 + 0.451*Temperature;
  Vis_O2 := 188.0 + 0.606*Temperature;
  Vis_CO2 := 187.1 + 0.612*Temperature;
  Vis_H2O := 117.6 + 0.506*Temperature;

{
    Calculate the relative gas viscosity.
    }
  Rel_viscos := (FO2*Vis_O2 + FCO2*Vis_CO2
                + FN2*Vis_N2 + FH2O*Vis_H2O)/Vis_STPD;

  END; {FUNCTION Rel_viscos}
}
=====}

BEGIN {Calc_Incr_Vol}

```

```

Non_C_Incr_Vol := Bin_delta_P * T;
IF Corr_flag THEN
  BEGIN
    Rel_viscosity := Rel_viscos( Temperature, Fh2o );
    {Calculate the ITPnS to STPD conversion factor.}
    ITPnS_to_STPD :=
      (1.0 - Fh2o) * ( 273.15 / (Temperature + 273.15) ) * (Pb/760);
    Corr_Incr_Vol := Bin_delta_P / Rel_Viscosity * T;
    Corr_Incr_Vol := Corr_Incr_Vol * ITPnS_to_STPD;
  END
ELSE
  BEGIN
    Corr_Incr_Vol := Non_C_Incr_Vol;
  END;
END; {Calc_Incr_Vol}
{=====}

```

```

      *** BEGIN FLOW CALIBRATION}
BEGIN {FLOWCAL}

```

```

IF (Corr_flag) THEN      {Read the water vapor pressure table.}

```

```

  BEGIN
    RESET (Vap_File, Vap_File_name);
    FOR Array_pointer := First_element TO Last_Element      DO
      BEGIN
        READ (Vap_File, Vap[Array_pointer]);
      END;
    END;

```

```

      {Determine the binary value corresponding to zero flow.}

```

```

Line_feed(2);
WRITELN ('You can determine the binary zero flow or use a');
WRITELN ('default value of 2038. ');
PROMPT ('Do you wish to determine binary zero flow? (Y/N)');
Ask_Y_or_N(Q);
IF Q='Y' THEN
  BEGIN

```

```

    {*** INSTRUCT USER TO APPLY ZERO FLOW TO THE PNEUMOTACHOMETER}

```

```

    WRITELN('CONNECT ZERO FLOW TO PNEUMOTACHOMETER. ');

```

```

    {*** FOLLOWING A CARRIAGE RETURN, GO COLLECT 500 FLOW DATA POINTS}

```

```

    HOLD_UP;
    DATA_COLLECT(Sam, S, LINE1, LINE2, LINE3, LINE4);

```

```

    {*** AVERAGE THE 500 DATA POINTS FOR ZERO FLOW VALUE}

```

```

    Tot_zero:=LINE3^[1];

```

```

FOR I:=2 TO Sam DO
  BEGIN
    Tot_zero:=Tot_zero+LINE3^[I];
  END;

Bin_zero_flow:=Tot_zero DIV Sam;

  {*** DISPLAY BINARY ZERO FLOW VALUE ON 9826 CRT}

  WRITELN('Average binary value for zero flow =',Bin_zero_flow);
  END

ELSE

  BEGIN
    Bin_zero_flow := 2038;
  END;

  {Calibrate the flow signal by first integrating the measured
  differential pressure signal over each inspiratory and expir-
  atory cycle. The average inspiratory and expiratory binary
  volumes are then set equal to the known pump volume with the
  calibration factor.}

  {*** INSTRUCT USER TO CONNECT PNEUMOTACHOGRAPH TO HARVARD PUMP}
  Line_feed(2);
  IF Corr_flag THEN
    BEGIN
      WRITELN('INSERT THE THERMOCOUPLE INTO THE PTM HEAD');
    END;

  WRITELN('CONNECT PUMP FLOW TO THE PNEUMOTACHOGRAPH. ');
  Line_feed(1);

  {*** FOLLOWING A CARRIAGE RETURN, GO COLLECT 4000 DATA POINTS
  OF PUMP FLOW}

  HOLD_UP;
  Sam:=4000;
  DATA_COLLECT(Sam,S,LINE1,LINE2,LINE3,LINE4);

  { INSTRUCT USER DATA COLLECTION IS COMPLETE AND BEGIN INTEGRATION
  OF FLOW SIGNAL TO DETERMINE INSPIRATORY AND EXPIRATORY FLOW
  CALIBRATION}

  BEEP;
  WRITELN('DATA COLLECTION COMPLETE... turn off the pump. ');

  { INITIALIZE NECESSARY VARIABLES FOR FLOW SIGNAL INTEGRATION}
  NoBreaths:=0;
  T:=1/S;
  A:=1;
  Non_C_Tot_Vol_insp := 0;
  Non_C_Tot_Vol_expr := 0;
  Corr_Tot_Vol_insp := 0;
  Corr_Tot_Vol_expr := 0;

```

```

      { PRINT HEADER ON CRT FOR BREATH-BY-BREATH INTEGRATION DISPLAY}

WRITELN('      Non Corrected Values      | Corrected Values ');
WRITELN('-----|-----');
WRITELN('      BINARY      BINARY      | BINARY      BINARY');
WRITELN('BREATH      AIR      AIR      | AIR      AIR');
WRITELN('NUMBER      INSPIRED      EXPIRED      | INSPIRED      EXPIRED');
WRITELN('-----|-----');

Still_calculating := TRUE;
REPEAT { MAKE SURE FLOW INDEX IS AT BEGINNING OF FIRST INSPIRATION}
  A:=A+1;
  IF A > Sam-1 THEN
    BEGIN
      Still_calculating := FALSE;
    END;
UNTIL (LINE3^[A-1] > Bin_zero_flow) AND (LINE3^[A] < Bin_zero_flow)
      OR NOT (Still_calculating);

IF Corr_flag THEN
  BEGIN
    Array_pointer := ROUND ((Room_temp - Min_Temp) * 10);
    Valid_Pointer (Array_pointer);
    Fh2o := Rel_humid * Vap[Array_pointer] / Pb;
  END;

WHILE Still_calculating DO
  BEGIN
    IF A> Sam-10 THEN
      BEGIN
        Still_calculating := FALSE;
      END;

      {Calculate the binary inspiratory volume of this stroke (breath).}

      IF Still_calculating THEN
        BEGIN
          {Compute half of the first trapezoidal area.}
          Temperature := Ta*Line4^[A]*Line4^[A] + Tb*Line4^[A] + Tc;
          Bin_delta_P := Line3^[A]-Bin_zero_flow;
          Calc_Incr_vol(Bin_delta_P,Fh2o,Temperature,T,
            Corr_Incr_vol,Non_C_Incr_vol);
          Corr_Airi := 0.5 * Corr_Incr_Vol;
          Non_C_Airi := 0.5 * Non_C_Incr_vol;
        END;

        { SUM UP ENTIRE INSPIRATION TRAPEZOIDS}
        Still_inspire := TRUE;
        WHILE Still_inspire AND Still_calculating DO
          BEGIN
            A:=A+1;
            IF A>Sam THEN {data has been exhausted, quit calculating}
              BEGIN
                Still_calculating := FALSE;
              END
            ELSE {Data is still available for calculation.}
              BEGIN
                Bin_delta_P := Line3^[A]-Bin_zero_flow;

```

```

IF (Bin_delta_P >= 0) THEN      {The inspiration is over}
  BEGIN
    Still_inspire := FALSE
  END

ELSE      {The pump is still inspiring, compute
          the incremental volume.}
  BEGIN
    Temperature := Ta*Line4^[A]*Line4^[A] + Tb*Line4^[A] + Tc;
    Calc_Incr_vol(Bin_delta_P, Fh2o, Temperature, T,
    Corr_Incr_vol, Non_C_Incr_vol);

    {Add the incremental volume to the total}
    Corr_Airi := Corr_Airi + Corr_Incr_Vol;
    Non_C_Airi := Non_C_Airi + Non_C_Incr_Vol;
  END;
END; {While loop}

IF Still_calculating THEN
  {Place half of the volume corresponding to inspiratory/expir-
  atory transition on the inspired volume and half on the
  expired volume.}

  BEGIN
    Temperature := Ta*Line4^[A]*Line4^[A] + Tb*Line4^[A] + Tc;
    Bin_delta_P := Line3^[A]-Bin_zero_flow;
    Calc_Incr_vol(Bin_delta_P, Fh2o, Temperature, T,
    Corr_Incr_vol, Non_C_Incr_vol);

    Corr_Airi := Corr_Airi + (1/2) * Corr_Incr_Vol;
    Non_C_Airi := Non_C_Airi + (1/2) * Non_C_Incr_Vol;

    Corr_Aire := (1/2) * (Corr_Incr_Vol);
    Non_C_Aire := (1/2) * (Non_C_Incr_Vol);
  END;

  { **** SUM UP ENTIRE EXPIRATION TRAPEZOIDS ****}
  Still_expire := TRUE;
  WHILE Still_expire AND Still_calculating DO
    BEGIN
      A:=A+1;
      IF A>Sam THEN      {The data has been exhausted}
        BEGIN
          Still_calculating := FALSE;
        END
      ELSE      {Data is still available for calculation.}
        BEGIN
          Bin_delta_P := Line3^[A]-Bin_zero_flow;
          IF (Bin_delta_P <= 0) THEN      {The expiration is over}
            BEGIN
              Still_expire := FALSE;
            END
          ELSE      {The pump is still expiring, compute the
                  incremental volume.}
            BEGIN
              Temperature := Ta*Line4^[A]*Line4^[A] + Tb*Line4^[A] + Tc;

```

```

      Calc_Incr_vol(Bin_delta_P,Fh2o,Temperature,T,
                   Corr_Incr_vol,Non_C_Incr_vol);

      {Add the incremental volume to the total}
      Corr_Aire := Corr_Aire + Corr_Incr_Vol;
      Non_C_Aire := Non_C_Aire + Non_C_Incr_Vol;
      END;
    END;
  END; {End While loop}

IF Still_calculating THEN
  {Place half of the volume corresponding to the expiratory-
  inspiratory transition on the total expired volume.}
  BEGIN
    Temperature := Ta*Line4^[A]*Line4^[A] + Tb*Line4^[A] + Tc;
    Bin_delta_P := Line3^[A]-Bin_zero_flow;
    Calc_Incr_vol(Bin_delta_P,Fh2o,Temperature,T,
                  Corr_Incr_vol,Non_C_Incr_vol);
    Corr_Aire := Corr_Aire + 0.5 * Corr_Incr_Vol;
    Non_C_Aire := Non_C_Aire + 0.5 * Non_C_Incr_Vol;

    { Make the calculations for this pump stroke.}

    NoBreaths:=NoBreaths+1;

    { **** UPDATE TOTAL VOLUMES INSPIRED AND EXPIRED ****}
    Corr_Tot_vol_insp := Corr_Tot_vol_insp + Corr_Airi;
    Non_C_Tot_vol_insp := Non_C_Tot_vol_insp + Non_C_Airi;
    Corr_Tot_vol_expr := Corr_Tot_vol_expr + Corr_Aire;
    Non_C_Tot_vol_expr := Non_C_Tot_vol_expr + Non_C_Aire;

    {** DISPLAY INSPIRED AND EXPIRED VOLUMES FOR THIS STROKE **}
    WRITELN(' ',NoBreaths:3,' ',Non_C_Airi:6:1,
            ' ',Non_C_Aire:6:1,' ',Corr_Airi:6:1,
            ' ',Corr_Aire:6:1);
    END;

  END; { End Main integration Loop.}

  {*** COMPUTE AVERAGE VOLUMES INSPIRED AND EXPIRED (PER BREATH BASIS)***}
  Non_C_Avg_Vol_insp := Non_C_Tot_vol_insp/NoBreaths;
  Non_C_Avg_Vol_expr := Non_C_Tot_vol_expr/NoBreaths;
  Corr_Avg_Vol_insp := Corr_Tot_vol_insp/NoBreaths;
  Corr_Avg_Vol_expr := Corr_Tot_vol_expr/NoBreaths;

  { Compute the inspiratory and expiratory flow calibration factors
  for the non corrected average Binary pump volume.}
  Non_C_I_flow_cal := Non_C_Pump_Vol / (-1*Non_C_Avg_Vol_insp);
  Non_C_E_flow_cal := Non_C_Pump_Vol / (Non_C_Avg_Vol_expr);

  {Compute the inspiratory and expiratory flow calibration factors
  for the corrected average Binary pump volume.}
  Corr_I_flow_cal := Corr_Pump_Vol / (-1*Corr_Avg_Vol_insp);
  Corr_E_flow_cal := Corr_Pump_Vol / (Corr_Avg_Vol_expr);

  {**** DISPLAY FLOW CALIBRATIONS ON HP9826 CRT ****}
  WRITELN('BINARY ZERO FLOW =',Bin_zero_flow);
  LineFeed(2);

```

```

WRITELN('Inspiratory and expiratory calibration factors');
WRITELN('for the NON CORRECTED flows.');
```

WRITELN('	Insp. flow calibration factor = ',Non_C_I_flow_cal);
WRITELN('	Expr. flow calibration factor = ',Non_C_E_flow_cal);

```

Line_feed(2);
WRITELN('Inspiratory and expiratory calibration factors');
WRITELN('for the CORRECTED flows.');
```

WRITELN('	Insp. flow calibration factor = ',Corr_I_flow_cal);
WRITELN('	Expr. flow calibration factor = ',Corr_E_flow_cal);

```

END; {FLOWCAL}
{
```

```

*** DECLARE PROCEDURE FOR CALIBRATION OF TEMPERATURE TRANSDUCER
}
```

```

PROCEDURE TEMPCAL(VAR Ta,Tb,Tc : REAL;
                  VAR Sam,S : INTEGER);
```

```

CONST Thermometer_cal_Slope = 1; {The Thermometer calibration factor.
This is the slope of the calibration curve
This is determined by calibrating the calibration thermometer with the Standard
Thermometer which is available from Anat. and Phys.}
Thermometer_cal_Y_int = -0.35; {The y intercept of the Calibration
curve of the calibration thermometer.}
```

```

TYPE TWODIM=ARRAY [1..3,1..3] OF REAL;
VAR Tlow,Tmid,Thigh,Tlow_bin,Tmid_bin:REAL;
    Thigh_bin,Normal_a:REAL;
    I,Tot_temp:INTEGER;
    Bin_temp,Bin_temp_inv:TWODIM;
```

```

{
*** BEGIN TEMPERATURE CALIBRATION ROUTINE
}
```

```

BEGIN {TEMPCAL}
```

```

{
*** INSTRUCT USER TO PLACE TC IN LOW TEMPERATURE WATER BATH
}
```

```

WRITELN('PUT THERMOCOUPLE IN THE LOWEST TEMP WATER BATH.');
```

```

{
*** GET ACTUAL TEMPERATURE OF LOW TEMPERATURE WATER BATH
}
```

```

WRITELN('ENTER THE THERMOMETER READING (deg C).');
```

```

BEEP;
```

```

READLN(Tlow);
```

```

{
```

Determine the true temperature.

```

Tlow := Tlow * Thermometer_cal_Slope + Thermometer_cal_Y_int;
}
```

```

{
*** GO TAKE 500 DATA POINTS ON THE TEMPERATURE CHANNEL
}
```

```

Sam:=500;
```

```

DATA_COLLECT(Sam,S,LINE1,LINE2,LINE3,LINE4);
```

```

{
*** COMPUTE THE AVERAGE VALUE FOR THE 500 TEMPERATURE DATA POINTS
}
```

```

Tot_temp:=0;
```

```

FOR I:=1 TO Sam DO
```

```

    BEGIN
```



```

    Tot_temp:=Tot_temp+LINE4^[1];
  END;
  Tlow_bin:=Tot_temp/Sam;
  {
  *** DISPLAY THE AVERAGE VALUE ON THE HP9826 CRT
  }
  WRITELN('AVERAGE BINARY VALUE READ FOR ',Tlow:2:2,' deg C');
  WRITELN('IS: ',Tlow_bin:4:1);
  {
  *** INSTRUCT USER TO PLACE TC IN MIDDLE TEMPERATURE WATER BATH
  }
  WRITELN('PUT THERMOCOUPLE IN THE MIDDLE TEMP WATER BATH. ');
  {
  *** GET ACTUAL TEMPERATURE OF MIDDLE TEMPERATURE WATER BATH
  }
  WRITELN('ENTER THE THE THERMOMETER READING (deg C). ');
  BEEP;
  READLN(Tmid);
  {
    Determine the true temperature.
  }
  Tmid := Tmid * Thermometer_cal_Slope + Thermometer_cal_Y_int;
  {
  *** GO TAKE 500 DATA POINTS ON THE TEMPERATURE CHANNEL
  }
  DATA_COLLECT(Sam,S,LINE1,LINE2,LINE3,LINE4);
  {
  *** COMPUTE THE AVERAGE VALUE FOR THE 500 TEMPERATURE DATA POINTS
  }
  Tot_temp:=0;
  FOR I:=1 TO Sam DO
    BEGIN
      Tot_temp:=Tot_temp+LINE4^[1];
    END;
  Tmid_bin:=Tot_temp/Sam;
  {
  *** DISPLAY THE AVERAGE VALUE ON THE HP9826 CRT
  }
  WRITELN('AVERAGE BINARY VALUE READ FOR ',Tmid:2:2,' deg C');
  WRITELN('IS: ',Tmid_bin:4:1);
  {
  *** INSTRUCT USER TO PLACE TC IN HIGH TEMPERATURE WATER BATH
  }
  WRITELN('PUT THERMOCOUPLE IN THE HIGH TEMP WATER BATH. ');
  {
  *** GET ACTUAL TEMPERATURE OF HIGH TEMPERATURE WATER BATH
  }
  WRITELN('ENTER THE THE THERMOMETER READING (deg C). ');
  BEEP;
  READLN(Thigh);
  {
    Determine the true temperature.
  }
  Thigh := Thigh * Thermometer_cal_Slope + Thermometer_cal_Y_int;
  {
  *** GO TAKE 500 DATA POINTS ON THE TEMPERATURE CHANNEL
  }
  DATA_COLLECT(Sam,S,LINE1,LINE2,LINE3,LINE4);
  {
  *** COMPUTE THE AVERAGE VALUE FOR THE 500 TEMPERATURE DATA POINTS
  }
  Tot_temp:=0;
  FOR I:=1 TO Sam DO

```

```

      BEGIN
        Tot_temp:=Tot_temp+LINE4^[1];
      END;
      Thigh_bin:=Tot_temp/Sam;
    {
    *** DISPLAY THE AVERAGE VALUE ON THE HP9826 CRT
    }
    WRITELN('AVERAGE BINARY VALUE READ FOR ',Thigh:2:2,' deg C');
    WRITELN('IS: ',Thigh_bin:4:1);
    {
    *** SET UP TEMPERATURE MATRIX FOR 2ND ORDER CURVE FIT DETERMINATION
    }
    Bin_temp[1,1]:=1;
    Bin_temp[2,1]:=1;
    Bin_temp[3,1]:=1;
    Bin_temp[1,2]:=Tlow_bin;
    Bin_temp[1,3]:=SQR(Tlow_bin);
    Bin_temp[2,2]:=Tmid_bin;
    Bin_temp[2,3]:=SQR(Tmid_bin);
    Bin_temp[3,2]:=Thigh_bin;
    Bin_temp[3,3]:=SQR(Thigh_bin);
    {
    *** CALCULATE THE DETERMINANT OF Bin_temp MATRIX
    }
    Norm_a:=Bin_temp[1,1]*(Bin_temp[2,2]*
      Bin_temp[3,3]-Bin_temp[2,3]*
      Bin_temp[3,2])-Bin_temp[1,2]*
      (Bin_temp[2,1]*Bin_temp[3,3]-
      Bin_temp[2,3]*Bin_temp[3,1])+
      Bin_temp[1,3]*(Bin_temp[2,1]*
      Bin_temp[3,2]-Bin_temp[2,2]*
      Bin_temp[3,1]);
    {
    *** DETERMINE THE INVERSE OF Bin_temp MATRIX
    }
    Bin_temp_inv[1,1]:=(Bin_temp[2,2]*
      Bin_temp[3,3]-Bin_temp[2,3]*
      Bin_temp[3,2])/Norm_a;
    Bin_temp_inv[1,2]:=(Bin_temp[1,3]*
      Bin_temp[3,2]-Bin_temp[1,2]*
      Bin_temp[3,3])/Norm_a;
    Bin_temp_inv[1,3]:=(Bin_temp[1,2]*
      Bin_temp[2,3]-Bin_temp[1,3]*
      Bin_temp[2,2])/Norm_a;
    Bin_temp_inv[2,1]:=(Bin_temp[3,1]*
      Bin_temp[2,3]-Bin_temp[2,1]*
      Bin_temp[3,3])/Norm_a;
    Bin_temp_inv[2,2]:=(Bin_temp[1,1]*
      Bin_temp[3,3]-Bin_temp[1,3]*
      Bin_temp[3,1])/Norm_a;
    Bin_temp_inv[2,3]:=(Bin_temp[1,3]*
      Bin_temp[2,1]-Bin_temp[1,1]*
      Bin_temp[2,3])/Norm_a;
    Bin_temp_inv[3,1]:=(Bin_temp[2,1]*
      Bin_temp[3,2]-Bin_temp[2,2]*
      Bin_temp[3,1])/Norm_a;
    Bin_temp_inv[3,2]:=(Bin_temp[1,2]*
      Bin_temp[3,1]-Bin_temp[1,1]*
      Bin_temp[3,2])/Norm_a;
    Bin_temp_inv[3,3]:=(Bin_temp[1,1]*
      Bin_temp[2,2]-Bin_temp[2,1]*
      Bin_temp[1,2])/Norm_a;
    {
    *** MULTIPLY INVERSE OF Bin_temp MATRIX BY TEMPERATURE TO YIELD 2ND
    *** ORDER COEFFICIENTS

```

```

    }
    Tc:=Bin_temp_inv[1,1]*
        Tlow+Bin_temp_inv[1,2]*
        Thigh+Bin_temp_inv[1,3]*
        Thigh;
    Tb:=Bin_temp_inv[2,1]*
        Tlow+Bin_temp_inv[2,2]*
        Thigh+Bin_temp_inv[2,3]*
        Thigh;
    Ta:=Bin_temp_inv[3,1]*
        Tlow+Bin_temp_inv[3,2]*
        Thigh+Bin_temp_inv[3,3]*
        Thigh;
    {
    *** DISPLAY 2ND ORDER COEFFICIENTS ON HP9826 CRT
    }
    WRITELN('2nd ORDER POLYNOMIAL CALIBRATION COEFFICIENTS');
    WRITELN('SECOND ORDER COEFFICIENT --> ',Ta);
    WRITELN('FIRST ORDER COEFFICIENT --> ',Tb);
    WRITELN('ZERO ORDER COEFFICIENT --> ',Tc);
    END; {TEMPCAL}
}-----}

{
*****
}

{
    BEGIN MAIN SYSTEM CALIBRATION PROGRAM (CAP2)
}

BEGIN {CAP2 START}
    NEW(Line1);      {CREATE DYNAMIC VARIABLE Line1}
    NEW(Line2);      {CREATE DYNAMIC VARIABLE Line2}
    NEW(Line3);      {CREATE DYNAMIC VARIABLE Line3}
    NEW(Line4);      {CREATE DYNAMIC VARIABLE Line4}
    {
    *** GO SET DAM CLOCK AT DESIRED FREQUENCY
    }
    CLKSET(S);
    {
    *** SET NUMBER OF SAMPLES AT 500 POINTS PER CHANNEL
    }
    Sam:=500;
    {
    *** CALIBRATE FRACTIONAL CONCENTRATIONS SIGNALS IF DESIRED
    }
    PROMPT ('CALIBRATE FRACTIONAL CONCENTRATION SIGNAL? (Y/N) ');
    Ask_Y_or_N(Q);
    IF Q='Y' THEN
        BEGIN
            GASCAL(O1,Co2_cal,O2_cal,Co2_dc_offset,
                O2_dc_offset,Sam,S);
        END;
    {
    *** CALIBRATE THE TEMPERATURE SIGNAL IF DESIRED
    }
    WRITELN('Do you wish to calibrate the Temperature');
    PROMPT ('Transducer? (Y/N) ');
    Ask_Y_or_N(Q);
    IF Q='Y' THEN
        {Keep recalibrating the temperature signal until
        the user no longer desires to do so.}

```

```

BEGIN
REPEAT
    TEMPCAL(Ta,Tb,Tc,Sam,S);
    WRITELN('Do you wish to recalibrate the Temperature');
    PROMPT ('Transducer? (Y/N) ');
    Ask_Y_or_N(Q);
    IF Q='Y' THEN
        BEGIN
            WRITELN('You are going to recalibrate the Temperature');
            PROMPT ('Transducer. Is this what you want to do? (Y/N)');
            Ask_Y_or_N(Q);
            END;
    UNTIL Q='N';
END;

    {*** CALIBRATE THE FLOW SIGNAL IF DESIRED ***}

PROMPT ('CALIBRATE THE FLOW SIGNAL? (Y/N) ');
Ask_Y_or_N(Q);
IF Q='Y' THEN
    BEGIN
        WRITELN('Do you wish to use gas temperature and gas');
        WRITELN('viscosity corrections while calibrating the flow');
        WRITELN('signal? (Y/N)');
        Ask_Y_or_N(Q);
        IF Q='Y' THEN
            BEGIN
                Corr_flag := TRUE;

                PROMPT ('Enter the percent relative humidity ');
                BEEP;
                READLN(Rel_humid);
                Rel_humid := Rel_humid / 100;

                PROMPT ('Enter the room temperature. (deg F) ');
                BEEP;
                READLN(Room_temp);
                Room_temp := (Room_temp - 32.0) * 5/9;

                PROMPT ('Enter the barometric pressure. (inches) ');
                BEEP;
                READLN(Pb);          {read in inches}
                Pb := Pb * 25.4; {torr/inch}
            END
        ELSE
            BEGIN
                Corr_flag := FALSE;
            END;
        FLOWCAL(Non_C_I_flow_cal,Non_C_E_flow_cal,
            Corr_I_flow_cal,Corr_E_flow_cal,Bin_zero_flow,
            Sam,S,Corr_flag,Rel_humid,Pb,Room_temp,Ta,Tb,Tc);
        Linefeed(2);
    END;

    {*** STORE THE CALIBRATION DATA IN AN ASCII FILE IF DESIRED ***}

PROMPT ('STORE CALIBRATION FACTORS ON DISK? (Y/N) ');
Ask_Y_or_N(Q);
IF Q='Y' THEN

```

```

BEGIN

    {*** GET CALIBRATION FILE NAME ***}
    WRITELN('ENTER THE FILE NAME FOR CALIBRATION FACTORS. ');
    BEEP;
    READLN(Fname);

    {*** Determine where to store the 'MONSTER' ASCII files. ***}
    Msi_devices[1] := '#12: '; {The hard disk, platter 2}
    Msi_devices[2] := '#13: '; {The hard disk, platter 3}
    Msi_devices[3] := '#7: '; {The 8 in. floppy disk.}
    WRITELN('You may store the ASCII files in one of the');
    WRITELN('locations below. ');
    WRITELN(' ');
    WRITELN(' 1. The Hard disk, Platter 1');
    WRITELN(' 2. The Hard disk, Platter 2');
    WRITELN(' 3. The 8 in. floppy disk. ');
    WRITELN(' ');
    REPEAT
        BEEP;
        PROMPT ('Which device do you want to use? ');
        READLN(Device_pointer);
        IF (Device_pointer < 1) OR (Device_pointer > 3) THEN
            BEGIN
                WRITELN(' ');
                WRITELN('You entered an invalid selection');
            END;
    UNTIL (Device_pointer=1) OR (Device_pointer=2) OR (Device_pointer=3);

    Fname := Msi_devices[Device_pointer] + Fname + '.ASC';

    {*** GET TODAY'S DATE ***}
    WRITELN('ENTER TODAY'S DATE, FORMAT: Month/Day/Year');
    BEEP;
    READLN(Date);

    {*** CREATE OR REWRITE ASCII FILE ***}
    REWRITE(F, Fname);

    {*** WRITE ASCII Co2_dc_offset TO FILE ***}
    STRWRITE(NSTRING, 1, TEMP, Co2_dc_offset:4);
    WRITELN(F, NSTRING);

    {*** WRITE ASCII O2_dc_offset TO FILE ***}
    STRWRITE(NSTRING, 1, TEMP, O2_dc_offset:4);
    WRITELN(F, NSTRING);

    {*** WRITE ASCII Bin_zero_flow TO FILE ***}
    STRWRITE(NSTRING, 1, TEMP, Bin_zero_flow:4);
    WRITELN(F, NSTRING);

    {*** WRITE ASCII Co2_cal TO FILE ***}
    STRWRITE(RSTRING, 1, TEMP, Co2_cal);
    WRITELN(F, RSTRING);

    {*** WRITE O2_cal TO FILE ***}
    STRWRITE(RSTRING, 1, TEMP, O2_cal);
    WRITELN(F, RSTRING);

```

```

    {*** WRITE Insp_flow_cal TO FILE ***}
    STRWRITE(RSTRING,1,TEMP,Non_C_I_flow_cal);
    WRITELN(F,RSTRING);

```

```

    {*** WRITE Expr_flow_cal TO FILE ***}
    STRWRITE(RSTRING,1,TEMP,Non_C_E_flow_cal);
    WRITELN(F,RSTRING);

```

```

    {*** WRITE Time_delay TO FILE ***}
    STRWRITE(RSTRING,1,TEMP,Time_delay);
    WRITELN(F,RSTRING);

```

```

    {*** WRITE SAMPLING FREQUENCY (S) TO FILE ***}
    STRWRITE(NSTRING,1,TEMP,S:4);
    WRITELN(F,NSTRING);

```

```

    {*** WRITE ACTUAL O2 CONCENTRATION FOR GAS MIXTURE TO FILE ***}
    STRWRITE(RSTRING,1,TEMP,OI);
    WRITELN(F,RSTRING);

```

```

    {*** WRITE 2ND ORDER TEMPERATURE COEFFICIENT (Ta) TO FILE ***}
    STRWRITE(RSTRING,1,TEMP,Ta);
    WRITELN(F,RSTRING);

```

```

    {*** WRITE 1ST ORDER TEMPERATURE COEFFICIENT (Tb) TO FILE ***}
    STRWRITE(RSTRING,1,TEMP,Tb);
    WRITELN(F,RSTRING);

```

```

    {*** WRITE CONSTANT TEMPERATURE COEFFICIENT (Tc) TO FILE ***}
    STRWRITE(RSTRING,1,TEMP,Tc);
    WRITELN(F,RSTRING);

```

```

    {*** WRITE TODAYS DATE TO FILE ***}
    WRITELN(F,Date);

```

{This section writes theFlow calibrationn values which are a result of version 2.0 of the Calibration Aquisition Program (CAP2). The viscosity corrected, STPD flow calibration values are written first followed by the barometric pressure and the relative humidity.}

```

    STRWRITE(RSTRING,1,TEMP,Corr_I_flow_cal);
    WRITELN (F,RSTRING);

```

```

    STRWRITE(RSTRING,1,TEMP,Corr_E_flow_cal);
    WRITELN (F,RSTRING);

```

```

    STRWRITE(RSTRING,1,TEMP,Pb);
    WRITELN (F,RSTRING);

```

```

    STRWRITE(RSTRING,1,TEMP,Rel_humid);
    WRITELN (F,RSTRING);

```

```

    STRWRITE(RSTRING,1,TEMP,Room_temp);

```

```
WRITELN (F,RSTRING);

      {*** CLOSE AND COMPACT THE CALIBRATION FILE ***}
CLOSE(F,'CRUNCH');

      END;
WRITELN ('      CAP2 PROGRAM RUN COMPLETE');
BEEP;
END. {CAP2 END}
```


A6.2 DAP2: a Pascal Routine for Collection of Respiratory Data

The Pascal program DAP2 (Data Acquisition Program, version 2) is used to collect respiratory data from an instrumented subject. A flowchart for the program is given in Chapter 6, Section 2. The method used by DAP2 to control the DAM is described by Riblett [13]. The contents of the data files has the same file structure specified by Riblett: four serial ASCII files. A description of each of the procedures used by DAP2 follows.

A6.2.1 BEEP Procedure

The procedure BEEP sounds an audible beep. This procedure is used to gain the operator's attention. This is the same procedure used by CAP2.

Variables passed to the procedure

None

Variables returned by the procedure

None

Variable definitions

No variables used.

A6.2.2 BIT_HI and BIT_TST Procedures

BIT_HI and BIT_TEST are external assembly language procedures. These procedures are used to control the DAM. BIT_HI and BIT_TEST procedures are documented by Riblett [13]. These procedures are also used by CAP2.

A6.2.3 CHECK_IF_DISK_FULL Procedure

The CHECK_IF_DISK_FULL procedure checks the storage device to determine if the disk contains uncompact ASCII data. A status file, named 'DISK_STAT.ASC', created by the ASCII_CONF Pascal program is checked to determine if the data has been compacted.

Variables passed to the procedure

Msi_device - string, passed by reference.

Variables returned by the procedure

Disk_stat - string, passed by reference.

Variable definitions

Disk_stat - a string variable containing the status of the disk.

Disk_stat is equal to 'EMPTY' if the disk does not contain ASCII data and 'FULL' if the disk does contain ASCII data.

Disk_stat_file - a text variable associated with the file specified by File_name.

File_name - a string containing the name of the file whose status is to be checked. File_name is set equal to the variable Msi_device concatenated with the string 'DISK_STAT.ASC'.

Msi_device - a string containing the mass storage device which is to be checked.

A6.2.4 CHECK SATURATION Procedure

CHECK_SATURATION determines if a datum sample is saturated, equal to the maximum sample value of 4095 or equal to the minimum sample value of 0. If a saturated value is found, the appropriate saturated value counter is incremented. CHECK_SATURATION is nested within the MAXMIN procedure.

Variables passed to the procedure

Number_equal_4095 - integer, passed by reference.

Number_equal_0 - integer, passed by reference.

Sample - integer, passed by value.

Variables returned by the procedure

Number_equal_4095 - integer, passed by reference.

Number_equal_0 - integer, passed by reference.

Variable definitions

Number_equal_4095 - an integer value which is incremented if the sample is equal to 4095.

Number_equal_0 - an integer value which is incremented if the sample is equal to 0.

Sample - an integer which is equal to the sampled value to be checked for saturation.

A6.2.5 CLKSET Procedure

The procedure CLKSET sets the 8253 timer in the DAM with the desired sampling frequency. CLKSET is called by the main CAP2 procedure to set the DAM's sampling frequency. This procedure was designed by Riblett [13] and has no modifications for version 2 of the calibration program (CAP2). CLKSET is also used by CAP2.

Variables passed to the procedure

None

Variables returned by the procedure

S - integer, passed by reference.

Variable definitions

F1 - an integer used to set the least significant byte of the 8253 timer.
 Fm - an integer used to set the most significant byte of the 8253 timer.
 S - an integer equal to the user specified sampling frequency.
 X - an integer variable used to set clock 1 of the 8253 timer.

A6.2.6 DAP2 Procedure

The DAP2 procedure provides the main control of the the data acquisition. DAP2 calls the DATA_COLLECTION procedure, the MAXMIN procedure, and the DATA_STORAGE procedure. DAP2 also calls the BEEP and HOLD_UP procedures.

Variables passed to the procedure

None

Variables returned by the procedure

None

Variable definitions

Co2max - an integer containing the maximum sampled datum point obtained from the CO₂ channel, Line1.
 Co2min - an integer containing the minimum sampled datum point obtained from the CO₂ channel, Line1.

- Line1 - an integer array, of 24,000 elements, containing the sampled values obtained from channel 1, the CO₂ channel, of the DAM.
- Line2 - an integer array, of 24,000 elements, containing the sampled values obtained from channel 2, the O₂ channel, of the DAM.
- Line3 - an integer array, of 24,000 elements, containing the sampled values obtained from channel 3, the flow channel, of the DAM.
- Line4 - an integer array, of 24,000 elements, containing the sampled values obtained from channel 4, the temperature channel, of the DAM.
- MAX - a constant value equal to 24,000, the maximum number of samples which may be collected.
- O2max - an integer containing the maximum sampled datum point obtained from the O₂ channel, Line2.
- O2min - an integer containing the minimum sampled datum point obtained from the O₂ channel, Line2.
- S - an integer containing the sampling frequency.
- Sam - an integer containing the number of samples to be collected.
- Tmax - an integer containing the maximum sampled datum point obtained from the temperature channel, Line4.
- Tmin - an integer containing the minimum sampled datum point obtained from the temperature channel, Line4.
- Vmax - an integer containing the maximum sampled datum point obtained from the flow channel, Line3.
- Vmin - an integer containing the minimum sampled datum point obtained from the flow channel, Line3.

A6.2.7 DATA COLLECT Procedure

The procedure DATA_COLLECT provides the necessary control of the DAM to collect a set of data from four channels. DATA_COLLECT samples the analog signals. DATA_COLLECT calls the assembly language procedures BIT_H1 and BIT_TST to test the status of the DAM. This procedure was designed by Riblett [13] and has only minor modifications for version 2 of the calibration program (CAP2). This is the same

procedure used by CAP2 to collect data.

Variables passed to the procedure

- S - integer, passed by reference.
- Sam - integer, passed by reference.

Variables returned by the procedure

- Line1 - integer array, passed by reference.
- Line2 - integer array, passed by reference.
- Line3 - integer array, passed by reference.
- Line4 - integer array, passed by reference.

Variable definitions

- Chana - a constant value equal to 15359 which sets the DAM's analog multiplexer so that channel A is passed to the analog to digital converter.
- Chanb - a constant value equal to 13311 which sets the DAM's analog multiplexer so that channel B is passed to the analog to digital converter.
- Chanc - a constant value equal to 11263 which sets the DAM's analog multiplexer so that channel C is passed to the analog to digital converter.
- Chand - a constant value equal to 9215 which sets the DAM's analog multiplexer so that channel D is passed to the analog to digital converter.
- Del - an integer variable used in the delay loop that allows the sample and hold amplifiers to reach equilibrium once the hold command is given.
- I - an integer variable used as a loop counter and a pointer into the four data arrays during collection of the specified number of datum points.
- Line1 - an integer array containing the sampled data acquired from the CO₂ channel of the DAM.
- Line2 - an integer array containing the sampled data acquired from the O₂ channel of the DAM.
- Line3 - an integer array containing the sampled data acquired from the flow channel of the DAM.
- Line4 - an integer array containing the sampled data acquired from the temperature channel of the DAM.
- Mask - a constant value equal to 4095 which is used to mask of

- the all but the 12 least significant data bits.
- R4 - an integer variable which is loaded with the contents of register 4 of the GPIO.
- R6 - an integer variable which is loaded with the contents of register 6 of the GPIO.
- S - an integer equal to the user specified sampling frequency.
- Sam - an integer variable equal to the number of samples to be collected from the DAM.

A6.2.8 DATA_STORAGE Procedure

The data storage procedure, DATA_STORAGE, stores the collected data and the maximum and minimum values from each channel. The file format is specified by Riblett [13]. The procedure CHECK_IF_DISK_FULL is used to determine if the disk contains data. The procedure SET_DISK_FULL_FLAG is used to set the disk status to full.

Variables passed to the procedure

- Co2max - integer, passed by value.
- Co2min - integer, passed by value.
- Line1 - array, passed by reference.
- Line2 - array, passed by reference.
- Line3 - array, passed by reference.
- Line4 - array, passed by reference.
- O2max - integer, passed by value.
- O2min - integer, passed by value.
- Sam - integer, passed by value.
- Tmax - integer, passed by value.
- Tmin - integer, passed by value.
- Vmax - integer, passed by value.
- Vmin - integer, passed by value.

Variables returned by the procedure

None

Variable definitions

- Co2max - an integer containing the maximum sampled datum point obtained from the CO₂ channel, Line1.

- Co2min - an integer-containing the minimum sampled datum point obtained from the CO₂ channel, Line1.
- Device_pointer - an integer which is used to indicate which mass storage device is to contain the calibration data.
- Disk_stat - a string variable containing the status of the disk. Disk_stat is equal to 'EMPTY' if the disk does not contain ASCII data and 'FULL' if the disk does contain ASCII data.
- F - a text variable associated with the file specified by the string variable File_name.
- File_name - a string containing the name of the file to be stored.
- Line1 - an integer array, of 24,000 elements, containing the sampled values obtained from channel 1, the CO₂ channel.
- Line2 - an integer array, of 24,000 elements, containing the sampled values obtained from channel 2, the O₂ channel.
- Line3 - an integer array, of 24,000 elements, containing the sampled values obtained from channel 3, the flow channel.
- Line4 - an integer array, of 24,000 elements, containing the sampled values obtained from channel 4, the temperature channel.
- MSI_devices - a string array containing three elements. These elements correspond to the three mass storage devices which can be used for the storage of the calibration data. Array element 1 contains #12 corresponding to platter 1 of the hard disk, element 2 contains #13 corresponding to platter 2 of the hard disk, and element 3 contains #7 corresponding to the 8-inch disk drive.
- NSTR1NG- a string variable used to represent the ASCII value of an integer number.
- O2max - an integer containing the maximum sampled datum point obtained from the O₂ channel, Line2.
- O2min - an integer containing the minimum sampled datum point obtained from the O₂ channel, Line2.
- Sam - an integer containing the number of samples to be collected. .
- TEMP - an integer variable needed by the STRWRITE function to convert the calibration data to ASCII strings.
- Tmax - an integer-containing the maximum sampled datum point

- obtained from the temperature channel, Line4.
- Tmin - an integer containing the minimum sampled datum point obtained from the temperature channel, Line4.
- Vmax - an integer containing the maximum sampled datum point obtained from the flow channel, Line3.
- Vmin - an integer containing the minimum sampled datum point obtained from the flow channel, Line3.

A6.2.9 HOLD UP Procedure

The hold up procedure, HOLD_UP, pauses program execution until the operator is ready to proceed. To continue program execution the operator must press the 'ENTER' key. This procedure was designed by Riblett [13] and has no modifications for version 2 of the calibration program (CAP2). This procedure is also used by CAP2.

Variables passed to the procedure

None

Variables returned by the procedure

None

Variable definitions

No variables used.

A6.2.10 Line feed Procedure

The line feed procedure, Line_feed, sends a specified number of line feeds to the screen. This procedure is also used by CAP2.

Variables passed to the procedure

I - integer, passed by value.

Variables returned by the procedure

None

Variable definitions

- I - an integer variable containing the number of line feeds to send to the screen.
- J - an integer variable used as a loop counter. J is incremented for each line feed which is sent until it is equal to the number of line feeds to be sent, I.

A6.2.11 MAXMIN Procedure

MAXMIN computes the maximum sample value and minimum sample value obtained from each channel. The procedure calls CHECK SATURATION to determine the number of samples that are saturated, equal to 4095 or 0, from each channel.

Variables passed to the procedure

Sam - integer, passed by reference.

Variables returned by the procedure

Co2max - integer, passed by value.

Co2min - integer, passed by value.

O2max - integer, passed by value.

O2min - integer, passed by value.

Tmax - integer, passed by value.

Tmin - integer, passed by value.

Vmax - integer, passed by value.

Vmin - integer, passed by value.

Variable definitions

Co2max - an integer containing the maximum sampled datum point obtained from the CO₂ channel, Line1.

Co2min - an integer containing the minimum sampled datum point obtained from the CO₂ channel, Line1.

I - an integer variable used as a pointer into the data arrays.

Line1 - an integer array, of 24,000 elements, containing the sampled values obtained from channel 1, the CO₂ channel.

Line2 - an integer array, of 24,000 elements, containing the sampled values obtained from channel 2, the O₂ channel.

Line3 - an integer array, of 24,000 elements, containing the sampled values obtained from channel 3, the flow channel.

Line4 - an integer array, of 24,000 elements, containing the sampled values obtained from channel 4, the temperature channel.

Num_CO2_equal_4095 - an integer equal to the number of CO₂ samples which are saturated on the positive rail, 4095.

Num_CO2_equal_0 - an integer equal to the number of CO₂ samples

- which are saturated on the negative rail, 0
- Num_O2_equal_4095 - an integer equal to the number of O₂ samples which are saturated on the positive rail, 4095.
- Num_O2_equal_0 - an integer equal to the number of O₂ samples which are saturated on the negative rail, 0
- Num_T_equal_4095 - an integer equal to the number of temperature samples which are saturated on the positive rail, 4095.
- Num_T_equal_0 - an integer equal to the number of temperature samples which are saturated on the negative rail, 0
- Num_V_equal_4095 - an integer equal to the number of flow samples which are saturated on the positive rail, 4095.
- Num_V_equal_0 - an integer equal to the number of flow samples which are saturated on the negative rail, 0
- O2max - an integer containing the maximum sampled datum point obtained from the O₂ channel, Line2.
- O2min - an integer containing the minimum sampled datum point obtained from the O₂ channel, Line2.
- Sam - an integer containing the number of samples to be collected.
- Tmax - an integer containing the maximum sampled datum point obtained from the temperature channel, Line4.
- Tmin - an integer containing the minimum sampled datum point obtained from the temperature channel, Line4.
- Vmax - an integer containing the maximum sampled datum point obtained from the flow channel, Line3.
- Vmin - an integer containing the minimum sampled datum point obtained from the flow channel, Line3.

A6.2.12 SET_DISK_FULL_FLAG Procedure

The SET_DISK_FULL_FLAG procedure sets the status of the data storage disk to the full state indicating the disk contains uncompact ASCII data. A status file, named 'DISK_STAT.ASC', created by the ASCII_CONF Pascal program is set to the 'FULL' state.

Variables passed to the procedure

Msi_device - string, passed by reference.

Variables returned by the procedure

None

Variable definitions

Disk_stat_file - a text variable associated with the file specified by the File_name.

File_name - a string containing the name of the file to be checked for the disk status. File_name is set equal to the variable Msi_device concatenated with the name 'DISK_STAT.ASC'.

Msi_device - a string containing the mass storage device which is to be checked.

A6.2.13 DAP2 Program Listing

```

$SYSPROG ON$
$TABLESS
$LINES 57$
PROGRAM DAP2(INPUT,OUTPUT);
{*****

```

DATA ACQUISITION AND STORAGE ROUTINE

PASCAL REV 2.1 SOURCE FILENAME: DAP2.TEXT

Department of Electrical and Computer Engineering
 Kansas State University

REVISION	DATE	PROGRAMMER
1.0	JUNE 28, 1984	LOREN E. RIBLETT, JR.
2.0	1-Feb-85	Michael Masters

PURPOSE

THIS ROUTINE PERFORMS ALL THE NECESSARY ACTIONS TO ACQUIRE, CONVERT (TO ASCII), AND STORE FOUR CHANNELS (CO₂, O₂, FLOW, AND TEMPERATURE) OF 12-BIT BINARY DATA FROM THE DAM.

ROUTINE(S) CALLED BY THIS ROUTINE

BIT_TST - 68000 ASSEMBLY MODULE THAT WAITS UNTIL THE EOC BIT ON THE DAM GOES HIGH, THEN LOW
 BIT_HI - 68000 ASSEMBLY MODULE THAT WAITS UNTIL THE EOC BIT ON THE DAM GOES LOW
 CLKSET - INTERNAL PROCEDURE THAT SETS THE 8253 TIMER CHIP FOR THE PROPER SAMPLING FREQUENCY
 MAXMIN - INTERNAL PROCEDURE THAT DETERMINES THE MAXIMUM AND MINIMUM VALUES FOR EACH OF THE FOUR DATA CHANNELS
 DATA_STORAGE - INTERNAL PROCEDURE THAT CONVERTS THE FOUR CHANNELS OF 12-BIT VALUES TO ASCII AND STORES THESE VALUES IN FOUR SEPARATE ASCII FILES
 HOLD_UP - INTERNAL PROCEDURE FOR TEMPORARY PAUSING OF PROGRAM OPERATION
 DATA_COLLECT - INTERNAL PROCEDURE THAT CONTROLS THE DAM IN THE PROPER FASHION TO COLLECT THE DESIRED NUMBER OF DATA POINTS

BEEP - Sounds an audible beep to alert the operator.

Line_feed - Sends a specified number of line feeds to the terminal.

NOTE 1: THE DAM SHOULD BE CONNECTED TO THE HP9826 COMPUTER VIA A GPIO INTERFACE AT SELECT CODE #12. THIS INSURES THE PROPER DEVICE ADDRESS FOR SENDING AND RECEIVING INFORMATION BETWEEN THE DAM AND THE HP9826.

NOTE 2: A MAXIMUM OF 24000 DATA POINTS PER CHANNEL IS ALLOWED WITH THE CURRENT VERSION OF DAP2. THIS VALUE MAY HAVE TO BE REDUCED IF SUBSTANTIAL ADDITIONS TO DAP2'S PROGRAM LENGTH IS REQUIRED.

NOTE 3: TWO EXTERNAL 68000 ASSEMBLY LANGUAGE ROUTINES ARE UTILIZED BY DAP2 TO HANDLE THE HIGH SPEED REQUIREMENTS NEEDED TO MONITOR THE End Of Conversion (EOC) SIGNAL FROM THE DAM.

NOTE 4: AT PRESENT, A MAXIMUM SAMPLING RATE OF 350 HZ IS RECOMMENDED. THIS VALUE MAY HAVE TO BE REDUCED IF SUBSTANTIAL ADDITIONS TO THE PROCEDURE DATA COLLECT ARE MADE.

```

*****}
{
*** LOAD NECESSARY LIBRARY MODULES
}
IMPORT IODECLARATIONS,GENERAL_0,
      GENERAL_1,IOCCMASM;
{
*** DECLARE FOUR LARGE EXTERNAL DATA ARRAYS AND POINTERS
}
TYPE L1=ARRAY [1..24000] OF INTEGER;      {CO2 CHANNEL DATA ARRAY}
      PT1=~L1;      {POINTER TO ARRAY L1}
      L2=ARRAY [1..24000] OF INTEGER;      {O2 CHANNEL DATA ARRAY}
      PT2=~L2;      {POINTER TO ARRAY L2}
      L3=ARRAY [1..24000] OF INTEGER;      {FLOW CHANNEL DATA ARRAY}
      PT3=~L3;      {POINTER TO ARRAY L3}
      L4=ARRAY [1..24000] OF INTEGER;      {TEMPERATURE CHANNEL DATA ARRAY}
      PT4=~L4;      {POINTER TO ARRAY L4}
{
*** SET PROGRAM CONSTANTS
}
CONST MAX=24000;      {MAXIMUM NUMBER OF SAMPLES PER CHANNEL ALLOWED}
{
*** DECLARE PROGRAM VARIABLES
}
VAR S,Sam:INTEGER;
    Co2min,O2min,Vmin,Tmin,
    Co2max,O2max,Vmax,Tmax      :      INTEGER;
    Line1: PT1;
    Line2: PT2;
    Line3: PT3;
    Line4: PT4;

    {*** DECLARE EXTERNAL 68000 ASSEMBLY MODULES ***}
PROCEDURE BIT_TST;EXTERNAL;      {WAITS UNTIL EOC BIT GOES HIGH, THEN LOW}
PROCEDURE BIT_HI;EXTERNAL;      {WAITS UNTIL EOC BIT IS LOW}

PROCEDURE BEEP;
{*****}
*****}
*
*      Procedure Name:      BEEP
*
*      File Name:      DAP2
*
*      REVISION      DATE      PROGRAMMER
*      -----      -
*      1.0      1-Feb-85      Michael Masters
*
*      Procedure discription:
*      This procedure sounds an audible beep to the operator.
*
*      Calling sequence:
*      BEEP;
*
*

```

```

* Parameters supplied by the calling routine.
* None
*
* Parameters returned to the calling routine.
* None
*
*****

```

```

BEGIN
PROMPT (CHR(7));
END;

```

```

PROCEDURE Line_feed(I : INTEGER);
{*****
*
* Procedure Name: Line feed
*
* File Name: DAP2
*
* REVISION DATE PROGRAMMER
* -----
* 1.0 1-Feb-85 Michael Masters
*
* Procedure discription:
* This procedure sends a specified number of line feeds to the
* terminal.
*
* Calling sequence:
* Line_feed(1);
*
* Parameters supplied by the calling routine.
*
* I - is an integer value parameter corresponding to the
* number of line feeds to be sent to the terminal.
*
* Parameters returned to the calling routine.
* None
*
*****
}

```

```

VAR J : INTEGER;

```

```

BEGIN
FOR J := 1 TO I DO {Send the specified number of line feeds}
BEGIN
PROMPT (CHR(10)); {Send the line feed}
END;
END;

```

```

{*** DECLARE PROCEDURE FOR PAUSING PROGRAM OPERATION ***}
PROCEDURE HOLD_UP;
BEGIN
PROMPT ('PRESS ENTER TO CONTINUE.');
```

```

{DISPLAY PROMPT ON CRT}

```

```

BEEP;
READLN; {WAIT UNTIL 'ENTER' IS PRESSED}
END; {HOLD_UP END}

```

```

{*** DECLARE PROCEDURE TO SET DAM CLOCK ***}
PROCEDURE CLKSET(VAR S:INTEGER); {PASS SAMPLING FREQUENCY (S)}

```

```

VAR X,Fm,F1:INTEGER;
BEGIN

```

```

{*** HAVE USER ENTER THE SAMPLING FREQUENCY ***}
PROMPT ('ENTER SAMPLING FREQUENCY: ');
BEEP;
READLN(S);

```

```

{*** DETERMINE 16-BIT COUNTER VALUE FOR CLK1 IN 8253 TIMER CHIP ***}
X:=1000000 DIV 2 DIV S;
IF X>=256 THEN

```

```

    BEGIN
    Fm:=X DIV 256;
    F1:=X-256*Fm;
    END

```

```

ELSE
    BEGIN
    Fm:=0;
    F1:=X;
    END;

```

```

{*** SET COUNTER 0 IN 8253 TIMER TO MODE 3 ***}
IOCONTROL(12,3,15678); {11110100111110}
IOCONTROL(12,3,15422); {11110000111110}
IOCONTROL(12,3,15670); {11110100110110}

```

```

{*** SET COUNTER 1 IN 8253 TIMER TO MODE 2 ***}
IOCONTROL(12,3,15740); {11110101111100}
IOCONTROL(12,3,15484); {11110001111100}
IOCONTROL(12,3,15732); {11110101110100}

```

```

{*** LOAD LSB OF COUNTER 0 ***}
IOCONTROL(12,3,9474); {10010100000010}
IOCONTROL(12,3,9218); {10010000000010}
IOCONTROL(12,3,9474); {10010100000010}

```

```

{*** LOAD MSB OF COUNTER 0 ***}
IOCONTROL(12,3,9472); {10010100000000}
IOCONTROL(12,3,9216); {10010000000000}
IOCONTROL(12,3,9472); {10010100000000}

```

```

{*** LOAD LSB OF COUNTER 1 ***}
IOCONTROL(12,3,13568+F1); {11010100000000}
IOCONTROL(12,3,13312+F1); {11010000000000}
IOCONTROL(12,3,13568+F1); {11010100000000}

```

```

{*** LOAD MSB OF COUNTER 1 ***}
IOCONTROL(12,3,13568+Fm); {11010100000000}
IOCONTROL(12,3,13312+Fm); {11010000000000}

```

```
IOCONTROL(12,3,13568+Fn); {11010100000000}
END; {CLKSET END}
```

```
PROCEDURE MAXMIN(VAR Sam,Co2max,Co2min,O2max,
                 O2min,Vmax,Vmin,Tmax,Tmin : INTEGER);
{*****}
*****
*
* Procedure Name: MAXMIN
*
* File Name: DAP2
*
* REVISION DATE PROGRAMMER
* -----
* 1.0 JUNE 28, 1984 LOREN E. RIBLETT, JR.
* 2.0 1-Feb-85 Michael Masters
*
* Procedure discription:
* This procedure calculates the maximum and minimum binary
* values of CO2, O2, flow, and temperature. The maximum and
* minimum values are displayed along with the number of sat-
* uration points on each channel.
*
* Calling sequence:
* MAXMIN (Sam,Co2max,Co2min,O2max,O2min,Vmax,Vmin,Tmax,Tmin,
* Line1,Line2,Line3,Line4);
*
* Parameters supplied by the calling routine.
* (all parameters are integers)
*
* Sam - A value parameter equal to the number of samples
* collected.
*
* Line1 - A reference variable array containing the CO2 data.
*
* Line2 - A reference variable array containing the O2 data.
*
* Line1 - A reference variable array containing the flow data.
*
* Line1 - A reference variable array containing the temp. data.
*
* Parameters returned to the calling routine.
*
* Co2max - A reference parameter equal to the maximum CO2 value.
*
* Co2min - A reference parameter equal to the minimum CO2 value.
*
* O2min - A reference parameter equal to the minimum O2 value.
*
* Vmax - A reference parameter equal to the maximum flow value.
*
* Vmin - A reference parameter equal to the minimum flow value.
*
* Tmax - A reference parameter equal to the maximum temp value
*
* Tmin - A reference parameter equal to the minimum temp value
*
* Procedures called by this procedure.
* None
```



```
*****
```

```
}
```

```
VAR      I,Num_CO2_equal_0,Num_CO2_equal_4095,
          Num_O2_equal_0,Num_O2_equal_4095,
          Num_V_equal_0,Num_V_equal_4095,
          Num_T_equal_0,Num_T_equal_4095      :      INTEGER;
```

```
PROCEDURE CHECK_SATURATION(Sample : INTEGER;
                           VAR Number_equal_4095,Number_equal_0 : INTEGER);
```

```
  BEGIN
```

```
    IF Sample = 0 THEN Number_equal_0 := Number_equal_0 +1;
    IF Sample = 4095 THEN Number_equal_4095 := Number_equal_4095 +1;
  END;
```

```
  BEGIN {MAX/MIN ROUTINE}
```

```
    {*** INITIALIZE THE DATA ***}
```

```
    Co2max := Line1^[1];
    Co2min := Line1^[1];
    O2max  := Line2^[1];
    O2min  := Line2^[1];
    Vmax   := Line3^[1];
    Vmin   := Line3^[1];
    Tmax   := Line4^[1];
    Tmin   := Line4^[1];
```

```
    Num_CO2_equal_4095 := 0;
    Num_CO2_equal_0    := 0;
    Num_O2_equal_4095  := 0;
    Num_O2_equal_0     := 0;
    Num_V_equal_4095   := 0;
    Num_V_equal_0      := 0;
    Num_T_equal_4095   := 0;
    Num_T_equal_0      := 0;
```

```
    {*** STEP THROUGH REMAINDER OF DATA TO FIND TRUE MAX/MIN VALUES ***}
    FOR I:=1 TO Sam DO
      BEGIN
```

```
        {*** CHECK FOR NEW MAX/MIN VALUES ***}
```

```
        IF Co2max<Line1^[I] THEN Co2max := Line1^[I];
        IF Co2min>Line1^[I] THEN Co2min := Line1^[I];
        IF O2max<Line2^[I] THEN O2max  := Line2^[I];
        IF O2min>Line2^[I] THEN O2min  := Line2^[I];
        IF Vmax<Line3^[I] THEN Vmax   := Line3^[I];
        IF Vmin>Line3^[I] THEN Vmin   := Line3^[I];
        IF Tmax<Line4^[I] THEN Tmax   := Line4^[I];
        IF Tmin>Line4^[I] THEN Tmin   := Line4^[I];
```

```
        CHECK_SATURATION(Line1^[I],Num_CO2_equal_4095,Num_CO2_equal_0);
        CHECK_SATURATION(Line2^[I],Num_O2_equal_4095,Num_O2_equal_0);
        CHECK_SATURATION(Line3^[I],Num_V_equal_4095,Num_V_equal_0);
        CHECK_SATURATION(Line4^[I],Num_T_equal_4095,Num_T_equal_0);
```

```
      END; {Do Loop}
```

```
    {*** DISPLAY THESE MAX/MIN VALUES ON THE CRT ***}
```

```
    WRITELN ('Signal      Max      Min      #4095 s      #0 s');;
```

```

WRITELN ( ' CO2',
          ',Co2max:4,', ' ',Co2min:4,
          ',Num_CO2_equal_4095:5,', ' ',Num_CO2_equal_0:5);
WRITELN ( ' O2',
          ',O2max:4,', ' ',O2min:4,
          ',Num_O2_equal_4095:5,', ' ',Num_O2_equal_0:5);
WRITELN ( ' FLOW',
          ',Vmax:4,', ' ',Vmin:4,
          ',Num_V_equal_4095:5,', ' ',Num_V_equal_0:5);
WRITELN ( ' Temp',
          ',Tmax:4,', ' ',Tmin:4,
          ',Num_T_equal_4095:5,', ' ',Num_T_equal_0:5);
END; {MAXMIN END}

```

```

PROCEDURE DATA_STORAGE(Sam,Co2max,Co2min,O2max,
                        O2min,Vmax,Vmin,Tmax,Tmin
                        : INTEGER;
                        VAR Line1:PT1; VAR Line2:PT2; Line3:PT3; VAR Line4:PT4);
{*****}
*****
*
* Procedure Name: BEEP
*
* File Name: DAP2
*
* REVISION          DATE          PROGRAMMER
* -----          -
* 1.0              JUNE 28, 1984  LOREN E. RIBLETT, JR.
* 2.0              1-Feb-85      Michael Masters
*
*
* Procedure discription:
*   This procedure stores the respiratory data to a disk.
*
* Calling sequence:
*   DATA_STORAGE (Sam,Co2max,Co2min,O2max,O2min,Vmax,Vmin,
*                 Tmax,Tmin,Line1,Line2,Line3,Line4);
*
* Parameters supplied by the calling routine.
*   (all parameters are integers)
*
*   Sam - A value parameter equal to the number of samples
*         collected.
*
*   Co2max - A value parameter equal to the maximum CO2 value.
*
*   Co2min - A value parameter equal to the minimum CO2 value.
*
*   O2min - A value parameter equal to the minimum O2 value.
*
*   Vmax - A value parameter equal to the maximum flow value.
*
*   Vmin - A value parameter equal to the minimum flow value.
*
*   Tmax - A value parameter equal to the maximum temp. value.
*
*   Tmin - A value parameter equal to the minimum temp. value.
*
*   Line1 - A reference variable array containing the CO2 data.
*
*   Line2 - A reference variable array containing the O2 data.
*
*   Line1 - A reference variable array containing the flow data.
*
*   Line1 - A reference variable array containing the temp. data.

```

```

* Parameters returned to the calling routine.
* None

```

```

* Procedures called by this procedure.

```

```

* CHECK_IF_DISK_FULL - Checks the selected mass storage medium to
* see if it contains noncompacted ASCII data.

```

```

* SET_DISK_FULL_FLAG - Sets the ASCII disk to the full state.

```

```

*****
}
VAR TEMP,I,Device_pointer : INTEGER;
    NSTRING : STRING [4];
    Disk_stat : STRING[5];
    F : TEXT;
    Msi_devices : ARRAY[1..3] OF STRING [4];
    File_name : STRING [16];

```

```

PROCEDURE CHECK_IF_DISK_FULL( VAR Msi_device,Disk_stat : STRING);

```

```

{*****
*****

```

```

* Procedure Name: Check if the disk is full

```

```

* File Name: DAP2

```

```

* REVISION          DATE          PROGRAMMER
* -----          -
* 1.0              1-Feb-85      Michael Masters

```

```

* Procedure description:

```

```

* This procedure checks to see if the selected storage device
* contains ASCII data that has not been compacted.

```

```

* Calling sequence:

```

```

* CHECK_IF_DISK_FULL(Msi_device,Disk_stat);

```

```

* Parameters supplied by the calling routine.

```

```

* Msi_device - a string value parameter indicating which
* mass storage device is to be checked.

```

```

* Parameters returned to the calling routine.

```

```

* Disk_stat - a string reference parameter that returns the
* status of the disk. Disk_stat is equal to 'FULL'
* if the disk contains un-compacted data and is equal
* 'EMPTY' if the disk contains ascii data.

```

```

*****
}
VAR Disk_stat_file : TEXT;
    File_name : STRING[17];

BEGIN
    File_name := Msi_device + 'DISK_STAT.ASC';
    RESET (Disk_stat_file,File_name);
    READLN (Disk_stat_file,Disk_stat);
    IF NOT (Disk_stat = "FULL") THEN Disk_stat := 'EMPTY';

```

END;

```

{-----}

PROCEDURE SET_DISK_FULL_FLAG( VAR Msi_device : STRING);
{*****}
*****
*
*   Procedure Name:   Set the disk full flag
*
*   File Name:       DAP2
*
*   REVISION         DATE           PROGRAMMER
*   -----
*   1.0              1-Feb-85       Michael Masters
*
*   Procedure discription:
*       This procedure alters the disk status file and sets the flag
*       to FULL.
*
*   Calling sequence:
*       CHECK_IF_DISK_FULL(Msi_device,Disk_stat);
*
*   Parameters supplied by the calling routine.
*
*       Msi_device - a string value parameter indicating which
*                   mass storage device is to be set to the FULL state.
*
*   Parameters returned to the calling routine.
*       None
*
*-----}
*****
}

```

```

VAR Disk_stat_file : TEXT;
    File_name      : STRING[17];

```

BEGIN

File_name := Msi_device + 'DISK_STAT.ASC';

REWRITE (Disk_stat_file,File_name);

WRITELN (Disk_stat_file,'FULL');

CLOSE(Disk_stat_file,'CRUNCH');

END;

BEGIN {DATA_STORAGE}

{*** Determine where to store the 'MONSTER' ASCII files. ***}

Msi_devices[1] := '#12:'; {The hard disk, platter 2}

Msi_devices[2] := '#13:'; {The hard disk, platter 3}

Msi_devices[3] := '#7:'; {The 8 in. floppy disk.}

REPEAT

Line_feed(3);

WRITELN('You may store the ASCII files in one of the');

WRITELN('locations below.');

WRITELN('');

WRITELN(' 1. The Hard disk, Platter 1.');

WRITELN(' 2. The Hard disk, Platter 2.');

WRITELN(' 3. The 8 in. floppy disk.');

::

```

WRITELN(' ');

REPEAT
    PROMPT ('Which device do you want to use? ');
    BEEP;
    READLN (Device_pointer);
    IF (Device_pointer < 1) OR (Device_pointer > 3) THEN
        BEGIN
            Line_feed(1);
            WRITELN ('You entered an invalid device option.');
```

END;

```

UNTIL (Device_pointer>=1) AND (Device_pointer<=3);

CHECK_IF_DISK_FULL(Msi_devices[Device_pointer],Disk_stat);
IF Disk_stat='FULL' THEN
    BEGIN
        Line_feed(20);
        WRITELN ('The device you selected contains ASCII data.');
```

WRITELN ('Either exchange the medium or select another');

```

        WRITELN ('device.');
```

END;

```

UNTIL (Disk_stat='EMPTY');
```

*** BEGIN CREATING ASCII CO2 FILE, FILENAME = MONSTER1.ASC ***

```

CREATE OR REWRITE FILE ON THE SPECIFIED UNIT)
WRITELN ('Storing the CO2 ASCII data.');
```

File_name := Msi_devices[Device_pointer] + 'MONSTER1.ASC';

```

REWRITE(F,File_name);
STRWRITE(NSTRING,1,TEMP,Co2max:4);      {CONVERT CO2 MAXIMUM TO ASCII}
WRITELN(F,NSTRING);                     {WRITE CO2 MAXIMUM TO FILE}
STRWRITE(NSTRING,1,TEMP,Co2min:4);      {CONVERT CO2 MINIMUM TO ASCII}
WRITELN(F,NSTRING);                     {WRITE CO2 MINIMUM TO FILE}
```

*** MAIN LOOP FOR CONVERTING AND STORING CO2 DATA TO ASCII FILE ***

```

FOR I:=1 TO Sam DO
    BEGIN
        STRWRITE(NSTRING,1,TEMP,Line1^[I]:4);      {CONVERT CO2 VALUE TO ASCII}
        WRITELN(F,NSTRING);                         {WRITE CO2 VALUE TO FILE}
    END;
```

CLOSE(F, 'CRUNCH'); {CLOSE AND COMPACT ASCII CO2 FILE}

*** BEGIN CREATING ASCII O2 FILE, FILENAME = MONSTER2.ASC ***

```

WRITELN ('Storing the O2 ASCII data.');
```

File_name := Msi_devices[Device_pointer] + 'MONSTER2.ASC';

```

REWRITE(F,File_name);      {CREATE OR REWRITE FILE }
STRWRITE(NSTRING,1,TEMP,O2max:4); {CONVERT O2 MAXIMUM TO ASCII}
WRITELN(F,NSTRING);         {WRITE O2 MAXIMUM TO FILE}
STRWRITE(NSTRING,1,TEMP,O2min:4); {CONVERT O2 MINIMUM TO ASCII}
WRITELN(F,NSTRING);         {WRITE O2 MINIMUM TO FILE}
```

*** MAIN LOOP FOR CONVERTING AND STORING O2 DATA TO ASCII FILE ***

```

FOR I:=1 TO Sam DO
    BEGIN
        STRWRITE(NSTRING,1,TEMP,Line2^[I]:4);      {CONVERT O2 VALUE TO ASCII}
        WRITELN(F,NSTRING);                         {WRITE O2 VALUE TO FILE}
    END;
```

CLOSE(F, 'CRUNCH'); {CLOSE AND COMPACT ASCII O2 FILE}

```

(***) BEGIN CREATING ASCII FLOW FILE, FILENAME = MONSTER3.ASC ***)
WRITELN('Storing the Flow ASCII data. ');
File_name := Msi_devices[Device_pointer] + 'MONSTER3.ASC';
REWRITE(F,File_name);           {CREATE OR REWRITE FILE }
STRWRITE(NSTRING,1,TEMP,Vmax:4); {CONVERT FLOW MAXIMUM TO ASCII}
WRITELN(F,NSTRING);             {WRITE FLOW MAXIMUM TO FILE}
STRWRITE(NSTRING,1,TEMP,Vmin:4); {CONVERT FLOW MINIMUM TO ASCII}
WRITELN(F,NSTRING);             {WRITE FLOW MINIMUM TO FILE}

(***) MAIN LOOP FOR CONVERTING AND STORING FLOW DATA TO ASCII FILE ***)
FOR I:=1 TO Sam DO
  BEGIN
    STRWRITE(NSTRING,1,TEMP,Line3^[I]:4); {CONVERT FLOW VALUE TO ASCII}
    WRITELN(F,NSTRING);                   {WRITE FLOW VALUE TO FILE}
  END;

CLOSE(F,'CRUNCH');           {CLOSE AND COMPACT ASCII FLOW FILE}

(***) BEGIN CREATING ASCII TEMPERATURE FILE, FILENAME = MONSTER4.ASC ***)
WRITELN('Storing the Temperature ASCII data. ');
File_name := Msi_devices[Device_pointer] + 'MONSTER4.ASC';
REWRITE(F,File_name);           {CREATE OR REWRITE FILE }
STRWRITE(NSTRING,1,TEMP,Tmax:4); {CONVERT TEMPERATURE MAXIMUM TO ASCII}
WRITELN(F,NSTRING);             {WRITE TEMPERATURE MAXIMUM TO FILE}
STRWRITE(NSTRING,1,TEMP,Tmin:4); {CONVERT TEMPERATURE MINIMUM TO ASCII}
WRITELN(F,NSTRING);             {WRITE TEMPERATURE MINIMUM TO FILE}

(***) MAIN LOOP FOR CONVERTING AND STORING FLOW DATA TO ASCII FILE ***)
FOR I:=1 TO Sam DO
  BEGIN
    STRWRITE(NSTRING,1,TEMP,Line4^[I]:4); {CONVERT TEMP. VALUE TO ASCII}
    WRITELN(F,NSTRING);                   {WRITE TEMP. VALUE TO FILE}
  END;

CLOSE(F,'CRUNCH');           {CLOSE AND COMPACT ASCII TEMP. FILE}

      {Set the disk is full flag.}
SET_DISK_FULL_FLAG(Msi_devices[Device_pointer]);
END; {DATA_STORAGE}
=====

(***) DECLARE PROCEDURE FOR COLLECTING FOUR CHANNELS OF DAM DATA ***)
PROCEDURE DATA_COLLECT(VAR Sam,S:INTEGER;
  VAR LINE1:PT1;VAR LINE2:PT2;
  VAR LINE3:PT3;VAR LINE4:PT4);
  VAR I,R6,Del,R4:INTEGER;
  CONST Chna=15359;Chnb=13311;      {BIT PATTERNS NECESSARY TO SET THE CHANNEL
  CONST Chnc=11263;Chnd=9215;      MULTIPLIER
  CONST Mask=4095;      {MASKS OFF ALL BUT 12 DATA BITS IN STATUS WORD}
  {
  *** MAIN LOOP FOR FOUR CHANNEL DATA ACQUISITION
  }

  BEGIN {DATA_COLLECT}
    WRITELN('NOW COLLECTING DATA... please wait patiently. ');
    WRITELN('Collecting ',Sam:5,'-samples..This will take',Sam DIV S:4,' Sec');

```

```

FOR I:=1 TO Sam DO
  BEGIN
    {
      *** PUT S/H AMPS IN TRACKING MODE AND SELECT CHANNEL A
    }
    R6:=BINAND(15360,Chna);
    R6:=BINCMP(R6);
    IOCONTROL(12,3,R6);
    {
      *** GIVE S/H AMPS TIME TO TRACK INPUT SIGNALS
    }
    De1:=15;
    WHILE De1>0 DO
      BEGIN
        De1:=De1-1;
      END;
    {
      *** SELECT CHANNEL A ON MULTIPLEXER AND CONVERT SIGNAL HIGH
    }
    R6:=BINAND(7168,Chna);
    R6:=BINCMP(R6);
    IOCONTROL(12,3,R6);
    {
      *** SELECT CHANNEL A ON MULTIPLEXER AND CONVERT SIGNAL LOW
    }
    R6:=BINAND(7680,Chna); {SEND CONVERT...}
    R6:=BINCMP(R6);       {...PULSE}
    IOCONTROL(12,3,R6);
    {
      *** SELECT CHANNEL A ON MULTIPLEXER AND CONVERT SIGNAL HIGH
    }
    R6:=BINAND(7168,Chna); {RETURN TO...}
    R6:=BINCMP(R6);       {...NORMAL}
    IOCONTROL(12,3,R6);
    {
      *** WAIT FOR EOC LINE TO GO LOW
    }
    BIT_HI;
    {
      *** READ GPIO STATUS REGISTER AND KEEP ONLY 12 BITS
    }
    R4:=IOSTATUS(12,3);
    R4:=R4 DIV 4;
    R4:=BINAND(MASK,R4);
    Line1^1]:=R4;
    {
      *** SELECT CHANNEL B ON MULTIPLEXER AND CONVERT SIGNAL HIGH
    }
    R6:=BINAND(7168,Chnb);
    R6:=BINCMP(R6);
    IOCONTROL(12,3,R6);
    {
      *** SELECT CHANNEL B ON MULTIPLEXER AND CONVERT SIGNAL LOW
    }
    R6:=BINAND(7680,Chnb);
    R6:=BINCMP(R6);
    IOCONTROL(12,3,R6);
    {
      *** SELECT CHANNEL B ON MULTIPLEXER AND CONVERT SIGNAL HIGH
    }
    R6:=BINAND(7168,Chnb);
    R6:=BINCMP(R6);
    IOCONTROL(12,3,R6);
    {

```



```

*** WAIT FOR EOC SIGNAL TO GO LOW
}
BIT_HI;
{
*** READ GPIO STATUS REGISTER AND KEEP ONLY 12 BITS
}
R4:=IOSTATUS(12,3);
R4:=R4 DIV 4;
R4:=BINAND(Mask,R4);
Line2^[I]:=R4;
{
*** SELECT CHANNEL C ON MULTIPLEXER AND CONVERT SIGNAL HIGH
}
R6:=BINAND(7168,Chnc);
R6:=BINCMP(R6);
IOCONTROL(12,3,R6);
{
*** SELECT CHANNEL C ON MULTIPLEXER AND CONVERT SIGNAL LOW
}
R6:=BINAND(7680,Chnc);
R6:=BINCMP(R6);
IOCONTROL(12,3,R6);
{
*** SELECT CHANNEL C ON MULTIPLEXER AND CONVERT SIGNAL HIGH
}
R6:=BINAND(7168,Chnc);
R6:=BINCMP(R6);
IOCONTROL(12,3,R6);
{
*** WAIT FOR EOC SIGNAL TO GO LOW
}
BIT_HI;
{
*** READ GPIO STATUS REGISTER AND KEEP ONLY 12 BITS
}
R4:=IOSTATUS(12,3);
R4:=R4 DIV 4;
R4:=BINAND(Mask,R4);
Line3^[I]:=R4;
{
*** SELECT CHANNEL D ON MULTIPLEXER AND CONVERT SIGNAL HIGH
}
R6:=BINAND(7168,Chnd);
R6:=BINCMP(R6);
IOCONTROL(12,3,R6);
{
*** SELECT CHANNEL D ON MULTIPLEXER AND CONVERT SIGNAL LOW
}
R6:=BINAND(7680,Chnd);
R6:=BINCMP(R6);
IOCONTROL(12,3,R6);
{
*** SELECT CHANNEL D ON MULTIPLEXER AND CONVERT SIGNAL HIGH
}
R6:=BINAND(7168,Chnd);
R6:=BINCMP(R6);
IOCONTROL(12,3,R6);
{
*** WAIT FOR EOC SIGNAL TO GO LOW
}
BIT_HI;
{
*** READ GPIO STATUS REGISTER AND KEEP ONLY 12 BITS
}
R4:=IOSTATUS(12,3);

```



```

        R4:=R4 DIV 4;
        R4:=BINAND(Mask,R4);
        Line4^[1]:=R4;
        {
        ** WAIT FOR EOC SIGNAL TO GO HIGH, THEN LOW
        }
        BIT_TST;
        {
        ** LOOP BACK UNTIL ALL POINTS ARE COLLECTED
        }
    END;
END; {DATA_COLLECT}

```

```

{*** BEGIN MAIN DATA ACQUISITION PROGRAM (DAP2). ***}
BEGIN {DAP2 START}

```

```

    NEW(Line1);      {CREATE DYNAMIC VARIABLE Line1}
    NEW(Line2);      {CREATE DYNAMIC VARIABLE Line2}
    NEW(Line3);      {CREATE DYNAMIC VARIABLE Line3}
    NEW(Line4);      {CREATE DYNAMIC VARIABLE Line4}

```

```

    {*** GO SET DAM CLOCK AT DESIRED FREQUENCY ***}
    CLKSET(S);

```

```

    {*** DETERMINE NUMBER OF DATA POINTS TO ACQUIRE ***}
    REPEAT

```

```

        PROMPT ('ENTER NUMBER OF SAMPLES [24000 MAX]: ');
        BEEP;
        READLN(Sam);
    UNTIL (Sam<24001) AND (Sam>0);

```

```

    {*** GO COLLECT THE FOUR CHANNELS WORTH OF DATA ***}
    HOLD_UP;
    WRITELN ('Now collecting the data');
    DATA_COLLECT (Sam,S,LINE1,LINE2,LINE3,LINE4);
    BEEP;
    WRITELN ('DATA COLLECTION COMPLETE');

```

```

    {*** DETERMINE THE MAX/MIN VALUES FOR EACH CHANNEL ***}
    WRITELN ('CALCULATING THE MAXIMUM AND MINIMUM VALUES');
    MAXMIN(Sam,Co2max,Co2min,O2max,O2min,Vmax,Vmin,Tmax,Tmin);

```

```

    {*** GO STORE THE FOUR CHANNELS OF DATA AS ASCII FILES ***}
    HOLD_UP;
    DATA_STORAGE(Sam,Co2max,Co2min,O2max,O2min,
        Vmax,Vmin,Tmax,Tmin,Line1,Line2,
        Line3,Line4);
    WRITELN (' ');
    WRITELN ('***** PROGRAM RUN COMPLETE *****');
    BEEP;
END. {DAP2 END}

```

A6.3 ASCII_CONF: a Pascal Routine to Configure the ASCII Data Disks to Accept Data

The Pascal program ASCII_CONF (ASCII CONFIGuration) is used to configure the respiratory data disk. DAP2 checks the status file, 'DISK_STAT.ASC', to determine if the data disk contains uncompact ASCII data. This status file prevents DAP2 from overwriting previously collected data. The configuration program, ASCII_CONF, must be executed to create the status file prior to using a disk to store ASCII data. If the file is not present the data acquisition program, DAP2, will 'crash'.

The ASCII_CONF program can also be used to set a disk to the empty status so that DAP2 can store data on it. This is helpful in the event data is collected and stored but is not desired to be retained.

A6.3.1 ASCII_CONF Procedures

The ASCII_CONF procedure provides the main control for the configuration program. ASCII_CONF creates the status file and sets the status to the 'EMPTY' state. ASCII_CONF calls the BEEP and Line_feed procedures.

Variables passed to the procedures

None

Variables returned by the procedures

None

Variable definitions

Disk_stat_file - a text variable associated with the file specified by File_name.

Device_pointer - an integer which is used to indicate which mass storage device is to be configured.

File_name - a string containing the name of the file to be checked for the disk status. File_name is set equal to the variable Msi_device concatenated with the name 'DISK_STAT.ASC'.

MSI_devices - a string array containing three elements. These elements correspond to the three mass storage devices which can be used for the storage of the calibration data. Array element 1 contains #12 corresponding to platter 1 of

the hard disk, element 2 contains #13 corresponding to platter 2 of the hard disk, and element 3 contains #7 corresponding to the 8-inch disk drive.

A6.3.2 BEEP Procedures

The procedure BEEP sounds an audible beep. This procedure is used to gain the operator's attention. This is the same procedure used by CAP2 and DAP2.

Variables passed to the procedures

None

Variables returned by the procedures

None

Variable definitions

No variables used.

A6.3.3 Line feed Procedures

The line feed procedure, Line_feed, sends a specified number of line feeds to the screen. This is the same Line_feed procedure used by CAP2 and DAP2.

Variables passed to the procedures

1 - integer, passed by value.

Variables returned by the procedures

None

Variable definitions

- 1 - an integer variable containing the number of line feeds to send to the screen.
- J - an integer variable used as a loop counter. J is incremented for each line feed which is sent until it is equal to the number of line feeds to be sent, 1.

A6.3.4 ASCII_CONF Program Listing

```

$SYSPROG ON$
$LINES 57$
$TABLES$
$REF 25$
PROGRAM ASCII_CONF(INPUT,OUTPUT);
{*****
*****
*
*   Program Name:          ASCII_CONF
*
*   Department of Electrical and Computer Engineering
*   Kansas State University
*
*   Source code location:  ASCII_CONF
*
*   REVISION              DATE              PROGRAMMER
*   -----              -
*   1.0                  20-Feb-85          Michael Masters.
*
*   Procedure description:
*   This program sets up disks so that the respiratory data
*   collection program can store ASCII data on them. The program
*   alters, or creates in the case of new disks, the disk status
*   file so that the disk can be written to by the data collection
*   program.
*
*   Calling sequence:
*   From the Main Command Level of the Pascal operating system
*   press the R key (R for RUN) and type ASCII_CONF in response
*   to the system prompt followed by the execute key.
*
*   Procedures called
*   BEEP - sounds an audible beep to gain the attention of the
*         operator.
*
*   Line_feed - sends a specified number of line feeds to the
*               terminal
*
*****
}

VAR   Device_pointer      :      INTEGER;
      Disk_stat_file     :      TEXT;
      Msi_devices         :      ARRAY[1..3] OF STRING [4];
      File_name           :      STRING [17];

PROCEDURE BEEP;
{*****
*****
*
*   Procedure Name:  BEEP
*
*   File Name:      ASCII_CONF
*
*   REVISION              DATE              PROGRAMMER
*   -----              -
*   1.0                  22-Sept-84          Michael Masters.
*

```

```

* Procedure-discription:

```

```

*   This procedure sounds an audible beep to the operator.

```

```

* Calling sequence:

```

```

*   BEEP;

```

```

* Parameters supplied by the calling routine.

```

```

*   None

```

```

* Parameters returned to the calling routine.

```

```

*   None

```

```

* BEGIN

```

```

* PROMPT (CHR(7));

```

```

* END;

```

```

PROCEDURE Line_feed(I : INTEGER);

```

```

{*****}

```

```

* Procedure Name: Line feed

```

```

* File Name: ASCII_CONF

```

```

* REVISION

```

```

* DATE

```

```

* PROGRAMMER

```

```

* -----
* 1.0

```

```

* -----
* 22-Sept-84

```

```

* -----
* Michael Masters.

```

```

* Procedure discription:

```

```

*   This procedure sends a specified number of line feeds to the
*   terminal.

```

```

* Calling sequence:

```

```

*   Line_feed(1);

```

```

* Parameters supplied by the calling routine.

```

```

*   1 - is an integer value parameter corresponding to the
*   number of line feeds to be sent to the terminal.

```

```

* Parameters returned to the calling routine.

```

```

*   None

```

```

* VAR J : INTEGER;

```

```

* BEGIN

```

```

* FOR J := 1 TO I DO {Send the specified number of line feeds}

```

```

* BEGIN

```

```

* PROMPT (CHR(10)); {Send the line feed}

```

```

* END;

```

END;

```

{=====}

BEGIN {ASCII_CONF}
  Msi_devices[1] := '#12: '; {The hard disk, platter 2}
  Msi_devices[2] := '#13: '; {The hard disk, platter 3}
  Msi_devices[3] := '#7: '; {The 8 in. floppy disk.}
  Line_feed(3);

  WRITELN('ASCII_CONF will configure a disk so that it');
  WRITELN('will except the ASCII data created by the resp-');
  WRITELN('iratory data collection program DAP2. The mass');
  WRITELN('storage devices listed below are valid locations');
  WRITELN('for storage of the ASCII respiratory data.');
```

Line_feed(1);	
WRITELN(' 1. The Hard disk, Platter 1.');	
WRITELN(' 2. The Hard disk, Platter 2.');	
WRITELN(' 3. The 8 in. floppy disk.');	
WRITELN(' ');	

```

  REPEAT

    PROMPT ('Which device do you want to configure? ');
    BEEP;
    READLN (Device_pointer);
    IF (Device_pointer < 1) OR (Device_pointer > 3) THEN
      BEGIN
        WRITELN (' ');
        WRITELN ('You entered an invalid device option.');
```

UNTIL (Device_pointer>=1) AND (Device_pointer<=3);	
{Set up the file name.}	
File_name := Msi_devices[Device_pointer];	
STRAPPEND (File_name, 'DISK_STAT.ASC');	
{open the status file.}	
REWRITE (Disk_stat_file, File_name);	
{write an empty status and close the file.}	
WRITELN (Disk_stat_file, 'EMPTY');	
CLOSE(Disk_stat_file, 'CRUNCH');	
BEEP;	
Line_feed(3);	
WRITELN (' **** Configuration complete ****');	

```

END.
```

APPENDIX VII. BASIC PROGRAM DOCUMENTATION AND LISTING

This appendix gives the details of the Basic programs used by the CBRMS. The documentation is similar to that of the Pascal programs. Each program is broken down into descriptions of the individual Basic subroutines which make up the program. The variables for a particular subroutine will be defined in that subroutine's section. The subroutines within each program are documented in alphabetical order. The variables within each subroutine are also listed in alphabetical order.

It should be noted that subroutine parameters can not be specified as value parameter or as a reference parameter, as is the case with Pascal procedures. Therefore, the parameter specifications will not state whether a parameter is passed by value or by reference. The manner in which a subroutine is called determines if a value is passed by reference or value. The following example points out how values are passed to a subroutine by reference or by value.

```
CALL Calc_sig_val((A),(Z),("INSP"),Incr_vol,Fo2,Fco2)
```

The first three parameters are passed by value and the last three are passed by reference.

Two additional sections have been added to the documentation of the Basic programs, definition of the COMMON blocks (A7.1) and a discussion of the respiratory variable array (Resp_var). The COMMON blocks serve as a link between the AUTOSTART, CAPCRUNCH, DAPCRUNCH, and ANALYSIS programs. This link allows variables to be passed between the programs. Also, several COMMON blocks are used to pass variables from a calling routine to a subroutine. The COMMON blocks and the contained variables are defined in Section A7.1. The documentation for the individual subroutines will include a listing of the COMMON blocks used in that subroutine. The respiratory variable array, Resp_var, is a special array containing the calculated breath-by-breath data.

A7.1 Definition of the COMMON Blocks

The COMMON blocks used by AUTOSTART, CAPCRUNCH, DAPCRUNCH, and ANALYSIS are defined here. The variables within each COMMON block are also defined.

The Anal_data COMMON blocks contain several variables which are used by the subroutines within the ANALYSIS program.

Anal_data1

Data_available - an integer variable used as a Boolean value which indicates if respiratory data is present in memory.

Anal_data2

False - an integer used as the constant Boolean value of false.

True - an integer used as the constant Boolean value of true.

Anal_data3

Co2_prod - an integer used as a constant value which points to the computed rate of CO₂ production data in the respiratory variable array.

Insp_min_vent - an integer used as a constant value which points to the computed inspiratory minute ventilation data in the respiratory variable array.

O2_cons - an integer used as a constant value which points to the computed rate of O₂ consumption data in the respiratory variable array.

Time_of_brth - an integer used as a constant value which points to the beginning time of each breath in the respiratory variable array.

Anal_data4

Expr_min_vent - an integer used as a constant value which points to the computed expiratory minute ventilation data in the respiratory variable array.

Resp_freq - an integer used as a constant value which points to the computed respiratory frequency data in the respiratory variable array.

V_tid_expr - an integer used as a constant value which points to the computed expiratory tidal volume data in the respiratory variable array.

V_tid_insp - an integer used as a constant value which points to the computed inspiratory tidal volume data in the respiratory variable array.

Anal_data5

Breath_good - an integer used as a constant value which points to the good or bad breath data in the respiratory variable array.

Formfd\$ - a character used as the constant value of the ASCII form feed character (12 decimal, 0C hex).

Resp_quotient - an integer used as a constant value which points to the computed respiratory quotient data in the respiratory variable array.

Anal_data5a

Frc_co2_prod - an integer used as a constant value which points to the computed alveolar CO_2 production data in the respiratory variable array.

Frc_o2_cons - an integer used as a constant value which points to the computed alveolar O_2 consumption data in the respiratory variable array.

Volume_of_lung - an integer used as a constant value which points to the computed lung volume data in the respiratory variable array.

Anal_data6

Corr_flag - an integer variable used as a Boolean value which indicates if the temperature corrections are used in computing the respiratory flow.

Room_fh2o - a real variable equal to the relative concentration of water vapor in room air.

T - a real variable equal to the sampling frequency used to collect the respiratory data.

Anal_data7

Fh2o_sat - a real valued, 250 element array used to hold the saturated relative concentrations of water vapor in room air between 20°C and 45°C .

Vap - a real valued, 250 element array used to hold the saturated water vapor pressure between 20°C and 45°C .

Anal_data8

Resp_var - a real valued array containing the calculated breath-by-breath respiratory variables. Resp_var is a two dimensional array, the first dimension is the respiratory variable and the second dimension is the breath number. A more detailed description of the respiratory variable array is given in Section A7.2 of this appendix.

Anal_data9

Comment\$ - a string variable containing a user specified comment.

Name\$ - a string variable containing a user specified subject name.

The Cal_data Common blocks contain the calibration data generated by CAP2 and converted to numeric format by CAPCRUNCH.

Cal_data1

Cal\$ - a string variable containing the name of the calibration file.

Date\$ - a string variable containing the date data were collected.

Cal_data2

Bin_zero_flow - an integer variable containing the sampled value equal to zero flow through the PTM.

Co2_dc_offset - an integer variable containing the sampled CO₂ value corresponding to room air.

O2_dc_offset - an integer variable containing the sampled O₂ value corresponding to the calibration gas.

Cal_data3

Co2_cal - a real variable equal to the CO₂ calibration factor.

O2_cal - a real variable equal to the O₂ calibration factor.

Cal_data4

Non_c_e_flowcal - a real variable containing the PTG calibration factor for expiratory flows determined without the use of temperature corrections.

Non_c_i_flowcal - a real variable containing the PTG calibration factor for inspiratory flows determined without the use of temperature corrections.

Cal_data5

Corr_e_flowcal - a real variable containing the PTG calibration factor for expiratory flows determined using temperature corrections.

Corr_i_flowcal - a real variable containing the PTG calibration factor for inspiratory flows determined using

temperature corrections.

Cal_data6

- Ta - a real variable equal to the second order calibration coefficient for converting the collected temperature data to units of $^{\circ}\text{C}$.
- Tb - a real variable equal to the first order calibration coefficient for converting the collected temperature data to units of $^{\circ}\text{C}$.
- Tc - a real variable equal to the zero order calibration coefficient for converting the collected temperature data to units of $^{\circ}\text{C}$.

Cal_data7

- O1 - a real variable equal to the fractional concentration of O_2 in the calibration gas.
- Pb - a real variable equal to the barometric pressure at the time the system was calibrated.
- Rel_humid - a real variable equal to the relative humidity at the time the system was calibrated.
- Room_temp - a real variable equal to the room temperature at the time the system was calibrated.
- Time_delay - an integer variable equal to the GMS time delay in milli-seconds.

The Plot_resp_data COMMON blocks contain information used by the respiratory parameter display subroutines.

Plot_resp_data1

- No_b_avg - an integer variable equal to the number of breath-by-breath values to be averaged.
- Num_breaths - a real variable equal to the number of breaths that were integrated.
- Omit_bad - an integer variable used as a Boolean flag which indicates if the 'bad' breaths are not to be included in the average.

Plot_resp_data2

- End_time - a real variable equal to the ending time of the respiratory results display.
- Start_time - a real variable equal to the starting time of the

respiratory results display.

W_{period} - a real variable equal time of the center of the window.

W_{width} - a real variable equal to the time width of the window.

The Resp_data COMMON blocks contain the respiratory data collected by DAP2 and converted to numeric format by DAPCRUNCH.

Resp_data1

Line1 - an integer array, of 24,000 elements, containing the sampled values obtained from the CO₂ channel, channel 1 of the DAM.

Line2 - an integer array, of 24,000 elements, containing the sampled values obtained from the O₂ channel, channel 2 of the DAM.

Resp_data2

Line3 - an integer array, of 24,000 elements, containing the sampled values obtained from the flow channel, channel 2 of the DAM.

Line4 - an integer array, of 24,000 elements, containing the sampled values obtained from the temperature channel, channel 4 of the DAM.

Resp_data3

C_{max} - an integer variable containing the maximum sampled datum point obtained from the CO₂ channel, Line1.

C_{min} - an integer variable containing the minimum sampled datum point obtained from the CO₂ channel, Line1.

F_{max} - an integer variable containing the maximum sampled datum point obtained from the flow channel, Line3.

F_{min} - an integer variable containing the minimum sampled datum point obtained from the flow channel, Line3.

O_{max} - an integer variable containing the maximum sampled datum point obtained from the O₂ channel, Line2.

O_{min} - an integer variable containing the minimum sampled datum point obtained from the O₂ channel, Line2.

T_{max} - an integer variable containing the maximum sampled datum point obtained from the temperature channel, Line4.

Tmin - an integer variable containing the minimum sampled datum point obtained from the temperature channel, Line4.

Resp_data4

No_points - an integer variable containing the number of samples collected.

Resp_data5

C1\$ - a string variable containing the name of the CO₂ data file.

O\$ - a string variable containing the name of the O₂ data file.

T\$ - a string variable containing the name of the temperature data file.

V\$ - a string variable containing the name of the flow data file.

A7.2 Description of the Respiratory Variable Array

The respiratory variable array, Resp_var, contains the calculated breath-by-breath respiratory parameters. The respiratory variable array is a two dimensional array. The first dimension of the respiratory variable array is the respiratory parameter and the second dimension is the breath number. The array used in this work contains 13 respiratory parameters and can hold up to 500 breaths. The construction of the respiratory variable array is illustrated in Figure A7.2.1. The pointers to the array are shown on the left of the figure along with the values currently assigned to them. Access to a certain parameter for a particular breath is accomplished by placing the parameter of interest in the variable dimension and the breath number in the breath dimension. For example, X can be equated to the O₂ consumed for breath 5 by the statement.

$$X = \text{Resp_var}(\text{O2_cons}, 5)$$

Use of this type of array to contain the calculated results allows for easy addition of other respiratory parameters. Additional variables can be stored in the array by increasing the respiratory variable dimension by one and defining a pointer to that variable. Also, it is an easy matter to add another dimension to the array.

		Breath Number						
		1	2	3	4	498	499	500
Time_of_brth	(0)							
O2_cons	(1)						
Co2_prod	(2)						
Frc_o2_cons	(3)						
Frc_co2_prod	(4)						
Insp_min_vent	(5)						
Expr_min_vent	(6)						
V_tid_insp	(7)						
V_tid_expr	(8)						
Volume_of_lung	(9)						
Resp_freq	(10)						
Resp_quotient	(11)						
Breath_good	(12)						

Figure A7.2.1 Construction of the respiratory variable array.

A7.3 AUTOST: a Basic Program Linking all Basic Programs

The auto start program, AUTOST, links the other Basic programs of the CBRMS. The operator can load any other program by pressing a function key while AUTOST is executing.

Common blocks used by the subroutine

Common Block	Variables in the block
Anal_data1	- Data_available
Cal_data1	- Cal\$, Date\$
Cal_data2	- Bin_zero_flow, Co2_dc_offset, O2_dc_offset
Cal_data3	- Co2_cal, O2_cal
Cal_data4	- Non_c_e_flowcal, Non_c_i_flowcal
Cal_data5	- Corr_e_flowcal, Corr_i_flowcal
Cal_data6	- Ta, Tb, Tc
Cal_data7	- Ol, Pb, Rel_humid, Room_temp, Time_delay
Resp_data1	- Line1, Line2
Resp_data2	- Line3, Line4
Resp_data3	- Cmax, Cmin, Fmax, Fmin, Omax, Omin, Tmax,
Resp_data4	- No_points

Resp_data\$ - C1\$, O\$, T\$, V\$

Variable definitions

- A - a real variable used as a pointer into the mass storage device array, Dev\$.
- Dev\$ - a string array of five elements containing the five mass storage devices. This array is used to allow the operator to easily change the default mass storage device.
- File_to_load\$ - a string variable which contains an operator specified program file name. This program is loaded and begins execution.
- l - a real variable used as a pointer into the Dev\$ array.

A7.3.1 AUTOST Program Listing

```

10  ! *****
20  !
30  !     AUTO-START ROUTINE
40  !
50  !     HP BASIC FILENAME:  AUTOST
60  !
70  !     Department of Electrical and Computer Engineering
80  !     Kansas State University
90  !
100 !     REVISION          DATE          PROGRAMMER
110 !     -----          -
120 !     1.0              JUNE 1, 1984    LOREN E. RIBLETT
130 !
140 ! *****
150 !
160 !     PURPOSE
170 !
180 !     THIS ROUTINE ALLOWS THE USER TO ACCESS THE VARIOUS HP
190 !     BASIC ROUTINES THAT CURRENTLY EXIST FOR THE HUMAN
200 !     RESPIRATORY RESEARCH STUDIES.
210 !
220 !     ROUTINE(S) CALLED BY THIS ROUTINE
230 !
240 !     CAPCRUNCH - CALIBRATION ASCII TO BINARY FILE CONVERSION
250 !     DAPCRUNCH - DAM DATA ASCII TO BINARY FILE CONVERSION
260 !     ANALYSIS  - BREATH-BY-BREATH ANALYSIS ROUTINE
270 !     STOREHR   - Stores the heart rate values in a format
280 !                  compatible with Sprick's PLOT program.
290 !
300 ! *****
310 !
320 !     NOTE 1:  Because this is an AUTOST routine, it should appear
330 !              only on the 5.25" floppy used in the mass storage unit
340 !              ":INTERNAL".
350 !
360 !     NOTE 2:  The program is initiated by placing the floppy in the
370 !              mentioned drive and applying power to the HP9826.
380 !
390 !     NOTE 3:  This program is recalled upon completion of the called
400 !              routines.
410 !
420 ! *****
430 ! COM /Resp_data1/  INTEGER Line1(1:24000),Line2(1:24000)
440 ! COM /Resp_data2/  INTEGER Line3(1:24000),Line4(1:24000)
450 ! COM /Resp_data3/  INTEGER Cmin,Cmax,Qmin,Qmax,Fmin,Fmax,Tmin,Tmax
460 ! COM /Resp_data4/  INTEGER No_points
470 ! COM /Resp_data5/  C1$(10),O2$(10),V$(10),TS(10)
480 ! COM /Cal_data1/   Cal$(10),Date$(25)
490 ! COM /Cal_data2/   INTEGER Co2_dc_offset,O2_dc_offset,Bin_zero_flow,S
500 ! COM /Cal_data3/   REAL Co2_cal,O2_cal
510 ! COM /Cal_data4/   REAL Non_c_flowcal,Non_c_flowcal
520 ! COM /Cal_data5/   REAL Corr_i_flowcal,Corr_e_flowcal
530 ! COM /Cal_data6/   REAL Ta,Tb,Tc
540 ! COM /Cal_data7/   REAL Time_delay,O1,Pb,Rel_humid,Room_temp
550 ! COM /Anal_data1/  INTEGER Data_available
560 !
570 ! *** DECLARATIONS
580 !
590 ! DIM Dev$(5)[15],File_to_load$(25)
600 !
610 ! *** ASSIGN SPECIAL FUNCTION KEYS
620 !

```



```

630 ON KEY 0 LABEL "CCRUNCH" GOTO Ccrunch
640 ON KEY 1 LABEL "DCRUNCH" GOTO Dcrunch
650 ON KEY 2 LABEL "ANALYSIS" GOTO Analysis
660 ON KEY 4 LABEL "STOREHR" GOTO Heartrate
670 ON KEY 5 LABEL "New Msi" GOTO Msi
680 ON KEY 6 LABEL " LOAD" GOTO Load
690 ON KEY 7 LABEL " CAT" GOTO Cat
700 ON KEY 9 LABEL " EXIT" GOTO Exit
710 GOTO 630
720 !
730 !*** CALL TO DAPCRUNCH
740 !
750 Dcrunch:!
760 OFF KEY
770 LOAD "DAPCRUNCH:INTERNAL",1
780 !
790 !*** CALL TO CAPCRUNCH
800 !
810 Ccrunch:!
820 OFF KEY
830 LOAD "CAPCRUNCH:INTERNAL",1
840 !
850 !*** CALL TO ANALYSIS
860 !
870 Analysis:!
880 OFF KEY
890 LOAD "ANALYSIS:INTERNAL",1
900 Heartrate: !
910 !
920 !      Store heart rate routine
930 !
940 OFF KEY
950 LOAD "STOREHR:INTERNAL",1
960 !
970 !*** CATALOG REQUEST
980 !
990 Cat:!!
1000 OFF KEY
1010 CAT
1020 GOTO 630
1030!
1040!*** NEW MASS STORAGE REQUEST
1050!
1060 Msi:!
1070 OFF KEY
1080 PRINT CHR$(12)
1090 PRINT "Select the device you wish to use"
1100 Dev$(1)=":INTERNAL"
1110 Dev$(2)=":HP9895,700,0"
1120 Dev$(3)=":HP9895,702,1"
1130 Dev$(4)=":HP9895,702,2"
1140 Dev$(5)=":HP9895,702,3"
1150 FOR I=1 TO 5
1160 PRINT USING "3X,D,29A,15A";I," -is the mass storage device ",Dev$(I)
1170 NEXT I
1180 INPUT "ENTER the desired device's corresponding number.",A
1190 IF A<1 OR A>5 THEN Msi
1200 MASS STORAGE IS Dev$(A)
1210 PRINT CHR$(12)
1220 GOTO 630
1230!
1240!*** LOAD PROGRAM REQUEST
1250!
1260 Load:!
1270 OFF KEY

```

```
1280 BEEP
1290 LINPUT "ENTER THE NAME OF THE PROGRAM YOU WISH TO LOAD",File_to_load$
1300 LOAD File_to_load$
1310 GOTO 630
1320!
1330!*** PROGRAM TERMINATION REQUEST
1340!
1350 Exit:~!
1360 OFF KEY
1370 END
```

A7.4 CAPCRUNCH: a Basic Program Which Compacts the ASCII Data Collected by CAP2 to Numeric Format

CAPCRUNCH performs a conversion operation on the calibration data generated by the Pascal program CAP2. CAP2 stores the calibration data in an ASCII file. In order to minimize the required disk space and file access time, CAPCRUNCH converts this ASCII file to the numeric format of the Basic operating system.

A7.4.1 The Main Routine of CAPCRUNCH

The main routine of CAPCRUNCH performs all of the data conversion operations. The main routine calls the File_locations subroutine to determine the storage locations of the ASCII format calibration data file and where the numeric format calibration data is to be stored.

Common Blocks Used by the Subroutine

<u>Common Block</u>	<u>Variables in the block</u>
Anal_data1	- Data_available
Cal_data1	- Cal\$, Date\$
Cal_data2	- Bin_zero_flow, Co2_dc_offset, O2_dc_offset
Cal_data3	- Co2_ca, O2_cal
Cal_data4	- Non_c_e_flowcal, Non_c_i_flowcal
Cal_data5	- Corr_e_flowcal, Corr_i_flowcal
Cal_data6	- Ta, Tb, Tc
Cal_data7	- Ol, Pb, Rel_humid, Room_temp, Time_delay
Resp_data1	- Line1, Line2
Resp_data2	- Line3, Line4
Resp_data3	- Cmax, Gmin, Fmax, Fmin, Omax, Omin, Tmax,
Resp_data4	- No_points
Resp_data5	- C1\$, O\$, T\$, V\$

Variable definitions

- Ascii_loc\$ - a string variable equal to the operator specified storage location of the ASCII format calibration data.
- Bin_zero_flow - an integer variable containing the sampled value equal to zero flow through the PTM.
- Bin_zero_flow\$ - a string variable equal to the ASCII representation of Bin_zero_flow read from the calibration file.
- Cal\$ - a string variable containing the name of the calibration

file.

Char_length - a real variable containing the number of total number of characters to be stored in the numeric format calibration file.

Co2_cal - a real variable equal to the CO₂ calibration factor.

Co2_cal\$ - a string variable equal to the ASCII representation of Co2_cal read from the calibration file.

Co2_dc_offset - an integer variable containing the sampled CO₂ value corresponding to room air.

Co2_dc_offset\$ - a string variable equal to the ASCII representation of Co2_dc_offset read from the calibration file.

Corr_e_flowcal - a real variable containing the PTG calibration factor for expiratory flows determined using temperature corrections.

Corr_e_flowcal\$ - a string variable equal to the ASCII representation of Corr_e_flowcal read from the calibration file.

Corr_i_flowcal - a real variable containing the PTG calibration factor for inspiratory flows determined using temperature corrections.

Corr_i_flowcal\$ - a string variable equal to the ASCII representation of Corr_i_flowcal read from the calibration file.

Data_available - an integer variable used as a Boolean value which indicates if respiratory data is present in memory.

Data_loc\$ - a string variable set equal to the device specification of the 8-inch disk drive (:HP9895,700,0) which will be used to store the numeric format calibration data.

Date\$ - a string variable containing the date data were collected.

Formfd\$ - a single character string used as the constant value of the ASCII form feed character (12 decimal, 0C hex).

N1\$ - a string variable equal to the name of the calibration file created by CAP2 as it appears to the Basic operating system.

No_integers - a real variable equal to the number of integer

values to be stored in the calibration file.

No_reals - a real variable equal to the number of real values to be stored in the calibration file.

Non_c_e_flowcal - a real variable containing the PTG calibration factor for expiratory flows determined without the use of temperature corrections.

Non_c_e_flowcal\$ - a string variable equal to the ASCII representation of Non_c_e_flowcal read from the calibration file.

Non_c_i_flowcal - a real variable containing the PTG calibration factor for inspiratory flows determined without the use of temperature corrections.

Non_c_i_flowcal\$ - a string variable equal to the ASCII representation of Non_c_i_flowcal read from the calibration file.

O2_cal - a real variable equal to the O₂ calibration factor.

O2_cal\$ - a string variable equal to the ASCII representation of O2_cal read from the calibration file.

O2_dc_offset - an integer variable containing the sampled O₂ value corresponding to the calibration gas.

O2_dc_offset\$ - a string variable equal to the ASCII representation of O2_dc_offset read from the calibration file.

O1 - a real variable equal to the fractional concentration of O₂ in the calibration gas.

O1\$ - a string variable equal to the ASCII representation of O1 read from the calibration file.

Pb - a real variable equal to the barometric pressure at the time the system was calibrated.

Pb\$ - a string variable equal to the ASCII representation of Pb read from the calibration file.

Rel_humid - a real variable equal to the relative humidity at the time the system was calibrated.

Rel_humid\$ - a string variable equal to the ASCII representation of Rel_humid read from the calibration file.

Room_temp - a real variable equal to the room temperature at the time the system was calibrated.

Room_temp\$ - a string variable equal to the ASCII representation

- of Room_temp read from the calibration file.
- S - a real variable equal to the sampling frequency used by CAP2.
- SS - a string variable equal to the ASCII representation of S read from the calibration file.
- Ta - a real variable equal to the second order calibration coefficient for converting the collected temperature data to units of °C.
- Ta\$ - a string variable equal to the ASCII representation of Ta read from the calibration file.
- Tb - a real variable equal to the first order calibration coefficient for converting the collected temperature data to units of °C.
- Tb\$ - a string variable equal to the ASCII representation of Tb read from the calibration file.
- Tc - a real variable equal to the zero order calibration coefficient for converting the collected temperature data to units of °C.
- Tc\$ - a string variable equal to the ASCII representation of Tc read from the calibration file.
- Time_delay - an integer variable equal to the GMS time delay in milli-seconds.
- Time_delay\$ - a string variable equal to the ASCII representation of Time_delay read from the calibration file.
- True - an integer used as the constant Boolean value of true.

A7.4.2 File_locations Subroutine

The File_locations subroutine prompts the operator for the storage location of the ASCII format calibration data. The file location where the numeric format calibration data is to be stored is always set equal to the 8-inch disk drive (:HP9895,700,0). This could be easily changed to prompt the operator for a specific storage location. This subroutine is also used by DAPCRUNCH.

Common Blocks Used by the Subroutine

None

Variables passed to the procedures

None

Variables returned by the procedures

Ascii_loc\$ - string.

Data_loc\$ - string.

Variable definitions

A - a real variable used as a pointer into the Msi_devices\$ array.

Ascii_loc\$ - a string variable equal to the operator specified storage location of the ASCII format calibration data.

Data_loc\$ - a string variable set equal to the 8-inch disk drive device specification (:HP9895,700,0) which will be used to store the numeric format calibration data.

Msi_devices\$ - a string array containing the device specifications of the disk drives containing the data. Element 1 specifies platter 1 of the hard disk (:HP9895,702,1), element 2 specifies platter 2 of the hard disk (:HP9895,702,2), and element 3 specifies the 8-inch disk drive (:HP9895,700,0).

A7.4.3 CAPCRUNCH Program Listing

```

10 ! *****
20 !
30 ! CALIBRATION FILE, ASCII TO BINARY CONVERSION ROUTINE
40 !
50 ! HP BASIC FILENAME: CAPCRUNCH
60 !
70 ! Department of Electrical and Computer Engineering
80 ! Kansas State University.
90 !
100 ! REVISION          DATE          PROGRAMMER
110 ! -----          -
120 ! 1.0              JUNE 1, 1984    LOREN E. RIBLETT
130 ! 1.1              OCT 1, 1985    Michael Masters
140 ! *****
150 !
160 !
170 ! PURPOSE
180 !
190 ! THIS ROUTINE CONVERTS THE CALIBRATION FILE CREATED BY
200 ! THE PASCAL ROUTINE "CAP.CODE" FROM ASCII TO BINARY,
210 ! ALLOWING FOR MORE EFFICIENT DATA STORAGE.
220 !
230 ! ROUTINE(S) CALLED BY THIS ROUTINE
240 !
250 ! AUTOST - USER PROGRAM ACCESS ROUTINE
260 !
270 ! *****
280 !
290 !
300 ! NOTE 1: Converted files (binary) will be stored on the 8" floppy
310 ! "HP9895,700,0".
320 !
330 ! NOTE 3: ASCII files are purged following the conversion process.
340 !
350 ! NOTE 4: AUTOST is called following completion of CAPCRUNCH.
360 !
370 ! *****
380 COM /Resp_data1/ INTEGER Line1(1:24000),Line2(1:24000)
390 COM /Resp_data2/ INTEGER Line3(1:24000),Line4(1:24000)
400 COM /Resp_data3/ INTEGER Qmin,Qmax,Qmin,Qmax,Fmin,Fmax,Tmin,Tmax
410 COM /Resp_data4/ INTEGER No_points
420 COM /Resp_data5/ C1$(10),O2$(10),V$(10),T$(10)
430 COM /Cal_data1/ Cal$(10),Date$(25)
440 COM /Cal_data2/ INTEGER Co2_dc_offset,O2_dc_offset,Bin_zero_flow,S
450 COM /Cal_data3/ REAL Co2_cal,O2_cal
460 COM /Cal_data4/ REAL Non_c_i_flowcal,Non_c_e_flowcal
470 COM /Cal_data5/ REAL Corr_i_flowcal,Corr_e_flowcal
480 COM /Cal_data6/ REAL Ta,Tb,Tc
490 COM /Cal_data7/ REAL Time_delay,O1,Pb,Rel_humid,Room_temp
500 COM /Anal_data1/ INTEGER Data_available
510 True=(1=1)
520 Formfd$=CHR$(12)
530 !
540 !
550 !
560 ! *** ASSIGN SPECIAL FUNCTION KEYS
570 !
580 ON KEY 0 LABEL "CAPCRUNCH" GOTO 660
590 ON KEY 9 LABEL " EXIT" GOTO Done
600 GOTO 580
610 !
620 !

```



```

630 !
640 !*** MAKE DECLARATIONS
650 !
660 OFF KEY
670 DIM Co2_dc_offset$(4),O2_dc_offset$(4),Bin_zero_flow$(4)
680 DIM Co2_cal$(25),O2_cal$(25),Insp_flow_cal$(25)
690 DIM Expr_flow_cal$(25),Time_delay$(25),S$(4)
700 DIM O1$(25),Ta$(25),Tb$(25),Tc$(25)
710 DIM N$(10),N1$(10),Data_loc$(13),Ascii_loc$(13)
720 !
730 !
740 !
750 !*** GET FILE NAME TO CRUNCH
760 !
770 BEEP
780 INPUT "ENTER NAME OF CALIBRATION FILE TO CRUNCH: ",Cal$
790 File_locations(Ascii_loc$,Data_loc$)
800 !
810 IF Ascii_loc$=Data_loc$ THEN
820     PRINT TABXY(1,18);"Insert the ASCII data disk."
830     PRINT "Press CONTINUE when you are ready to proceed."
840     PAUSE
850     PRINT Formfd$
860 END IF
870 !
880 !
890 !*** ALTER FILE NAME TO REFLECT PASCAL TO BASIC NAME CHANGES
900 !
910 N1$=Cal$&"A"
920 WHILE LEN(N1$)<10
930     N1$=N1$&"-"
940 END WHILE
950 !
960 !
970 !
980 !*** READ IN ASCII VALUES FROM CALIBRATION FILE
990 !
1000 ASSIGN @Path1 TO N1$&Ascii_loc$
1010 ENTER @Path1;Co2_dc_offset$,O2_dc_offset$
1020 ENTER @Path1;Bin_zero_flow$,Co2_cal$
1030 ENTER @Path1;O2_cal$,Non_c_i_flowcal$
1040 ENTER @Path1;Non_c_e_flowcal$,Time_delay$,S$
1050 ENTER @Path1;O1$,Ta$,Tb$,Tc$,Date$
1060 ENTER @Path1;Corr_i_flowcal$,Corr_e_flowcal$
1070 ENTER @Path1;Pb$,Rel_humid$,Room_temp$
1080 ASSIGN @Path1 TO *
1090 !
1100 !
1110 !
1120 !
1130 !
1140 !
1150 Co2_dc_offset=VAL(Co2_dc_offset$)
1160 O2_dc_offset=VAL(O2_dc_offset$)
1170 Bin_zero_flow=VAL(Bin_zero_flow$)
1180 Co2_cal=VAL(Co2_cal$)
1190 O2_cal=VAL(O2_cal$)
1200 Non_c_i_flowcal=VAL(Non_c_i_flowcal$)
1210 Non_c_e_flowcal=VAL(Non_c_e_flowcal$)
1220 Time_delay=VAL(Time_delay$)
1230 S=VAL(S$)
1240 O1=VAL(O1$)
1250 Ta=VAL(Ta$)
1260 Tb=VAL(Tb$)
1270 Tc=VAL(Tc$)

```

```

1280 Corr_flowcal=VAL(Corr_flowcal$)
1290 Corr_flowcal=VAL(Corr_flowcal$)
1300 Pb=VAL(Pb$)
1310 Rel_humid=VAL(Rel_humid$)
1320 Room_temp=VAL(Room_temp$)
1330 !
1340 !
1350 !*** CREATE BINARY FILE ON THE DATA DISK
1360 !
1370 IF Data_loc$=Ascii_loc$ THEN
1380 PRINT TABXY(1,18);"Remove the ASCII data disk and put in"
1390 PRINT "the BINARY data disk."
1400 PRINT
1410 PRINT "Press CONTINUE when you are ready to proceed."
1420 BEEP
1430 PAUSE
1440 PRINT Formfd$
1450 END IF
1460 No_integers=4 !The number of calibration factors which are integers.
1470 No_reals=13 !The number of calibration factors which are reals.
1480 Char_length=25 !The total length of the char strings in the cal factors
1490 !
1500 !
1510 ! Create the file
1520 !
1530 CREATE BDAT Cal$&Data_loc$,1,2*No_integers+8*No_reals+Char_length
1540 !
1550 !*** WRITE BINARY CALIBRATION CONSTANTS TO FILE
1560 !
1570 ASSIGN @Path1 TO Cal$&Data_loc$
1580 OUTPUT @Path1;Co2_dc_offset
1590 OUTPUT @Path1;O2_dc_offset
1600 OUTPUT @Path1;Bin_zero_flow
1610 OUTPUT @Path1;Co2_cal
1620 OUTPUT @Path1;O2_cal
1630 OUTPUT @Path1;Non_c_flowcal
1640 OUTPUT @Path1;Non_c_flowcal
1650 OUTPUT @Path1;Time_delay
1660 OUTPUT @Path1;S,O1
1670 OUTPUT @Path1;Ta,Tb,Tc
1680 OUTPUT @Path1;Date$
1690 OUTPUT @Path1;Corr_flowcal
1700 OUTPUT @Path1;Corr_flowcal
1710 OUTPUT @Path1;Pb,Rel_humid,Room_temp
1720 ASSIGN @Path1 TO *
1730 !
1740 !
1750 !
1760 !
1770 !*** DELETE OLD ASCII CALIBRATION FILE
1780 !
1790 IF Data_loc$=Ascii_loc$ THEN
1800 PRINT TABXY(1,18);"Remove the BINARY data disk and put in"
1810 PRINT "the ASCII data disk."
1820 PRINT
1830 PRINT "Press CONTINUE when you are ready to proceed."
1840 BEEP
1850 PAUSE
1860 PRINT Formfd$
1870 END IF
1880 PURGE N1$&Ascii_loc$
1890 PRINT "CALIBRATION FILE COMPACTION COMPLETE."
1900!
1910!*** RETURN TO AUTOST
1920!

```

```

1930 Data_available=True
1940 Done:OFF KEY
1950 MASS STORAGE IS ":INTERNAL"
1960 LOAD "AUTOST",1
1970 END
1980 SUB File_locations(Ascii_loc$,Data_loc$)
1990 !
2000     DIM Msi_devices$(1:3)[13]
2010     Msi_devices$(1)=":HP9895,702,1"
2020     Msi_devices$(2)=":HP9895,702,2"
2030     Msi_devices$(3)=":HP9895,700,0"
2040     Formfd$=CHR$(12)
2050     PRINT Formfd$
2060     PRINT
2070     PRINT "Mass Storage devices"
2080     PRINT "    1.   The hard disk, platter 1"
2090     PRINT "    2.   The hard disk, platter 2"
2100     PRINT "    3.   The 8 inch floppy disk."
2110     BEEP
2120     INPUT "Which storage location contains the ASCII data",A
2130     Ascii_loc$=Msi_devices$(A)
2140     Data_loc$=Msi_devices$(3)
2150     PRINT Formfd$
2160 SUBEND

```

A7.5 DAPCRUNCH: a Basic Program Which Compacts the ASCII Data Collected by DAP2 to Numeric Format

DAPCRUNCH performs a conversion operation on the respiratory data collected by the Pascal program DAP2. DAP2 stores the data in four ASCII files. In order to minimize the disk space and file access time, DAPCRUNCH converts these ASCII files to the numeric format of the Basic operating system.

A7.5.1 The Main Routine of DAPCRUNCH

The main routine of DAPCRUNCH performs the main control of the program. The main routine calls the File_locations, Rd_and_crunch, and Write_data subroutines. File_locations prompts the operator for the mass storage device containing the ASCII data. Rd_and_crunch reads each ASCII file and converts the data from the ASCII format to the numeric format. Write_data writes the numeric format data to disk.

Common Blocks Used by the Subroutine

<u>Common Block</u>	<u>Variables in the block</u>
Anal_data1	- Data_available
Cal_data1	- Cal\$, Date\$
Cal_data2	- Bin_zero_flow, Co2_dc_offset, O2_dc_offset
Cal_data3	- Co2_ca, O2_cal
Cal_data4	- Non_c_e_flowcal, Non_c_i_flowcal
Cal_data5	- Corr_e_flowcal, Corr_i_flowcal
Cal_data6	- Ta, Tb, Tc
Cal_data7	- Ol, Pb, Rel_humid, Room_temp, Time_delay
Resp_data1	- Line1, Line2
Resp_data2	- Line3, Line4
Resp_data3	- Cmax, Cmin, Fmax, Fmin, Omax, Omin, Tmax,
Resp_data4	- No_points
Resp_data5	- C1\$, O\$, T\$, V\$

Variable definitions

Ascii_loc\$	- a string variable equal to the operator specified storage location of the ASCII format data.
C1\$	- a string variable containing the name of the CO ₂ data file.
Cmax	- an integer variable containing the maximum sampled datum

- point obtained from the CO₂ channel, Line1.
- Qmin** - an integer variable containing the minimum sampled datum point obtained from the CO₂ channel, Line1.
- Data_available** - an integer variable used as a Boolean value which indicates if respiratory data is present in memory.
- Data_loc\$** - a string variable set equal to the device specification of the 8-inch disk drive (:HP9895,700,0) which will be used to store the numeric format data.
- File_nm\$** - a string variable which is not used within the main routine of DAPCRUNCH. The declaration of **File_nm\$** within the main procedure (line 630) may be deleted. The variable is used within the **Rd_and_crunch** subroutine.
- Fmax** - an integer variable containing the maximum sampled datum point obtained from the flow channel, Line3.
- Fmin** - an integer variable containing the minimum sampled datum point obtained from the flow channel, Line3.
- Formfd\$** - a single character string used as the constant value of the ASCII form feed character (12 decimal, 0C hex).
- Line1** - an integer array, of 24,000 elements, containing the sampled values obtained from the CO₂ channel, channel 1, of the DAM.
- Line2** - an integer array, of 24,000 elements, containing the sampled values obtained from the O₂ channel, channel 2, of the DAM.
- Line3** - an integer array, of 24,000 elements, containing the sampled values obtained from the flow channel, channel 3, of the DAM.
- Line4** - an integer array, of 24,000 elements, containing the sampled values obtained from the temperature channel, channel 4, of the DAM.
- No_points** - an integer variable containing the number of samples collected.
- OS** - a string variable containing the name of the O₂ data file.
- Qmax** - an integer variable containing the maximum sampled datum point obtained from the O₂ channel, Line2.
- Qmin** - an integer variable containing the minimum sampled datum point obtained from the O₂ channel, Line2.

- T\$ - a string variable containing the name of the temperature data file.
- Tmax - an integer variable containing the maximum sampled datum point obtained from the temperature channel, Line4.
- Tmin - an integer variable containing the minimum sampled datum point obtained from the temperature channel, Line4.
- True - an integer used as the constant Boolean value of true.
- V\$ - a string variable containing the name of the flow data file.

A7.5.2 File locations Subroutine

The File_locations subroutine prompts the operator for the storage location of the ASCII format data. The file location where the numeric format data is to be stored is always set equal to the 8-inch disk drive (:HP9895,700,0). This could be easily changed to prompt the operator for a specific storage location. This subroutine is also used by CAPCRUNCH.

Common Blocks Used by the Subroutine

None

Variables passed to the procedures

None

Variables returned by the procedures

Ascii_loc\$ - string.

Data_loc\$ - string.

Variable definitions

A - a real variable used as a pointer into the Msi_devices\$ array.

Ascii_loc\$ - a string variable equal to the operator specified storage location of the ASCII format data.

Data_loc\$ - a string variable set equal to the 8-inch disk drive device specification (:HP9895,700,0) which will be used to store the numeric format data.

Msi_devices\$ - a string array containing the device specifications of the disk drives containing the data. Element 1 specifies platter 1 of the hard disk (:HP9895,702,1), element 2 specifies platter 2 of the hard

disk (:HP9895,702,2), and element 3 specifies the 8-inch disk drive (:HP9895,700,0).

A7.5.3 Rd_and_crunch Subroutine

The Rd_and_crunch (Read and crunch) subroutine performs the file conversion operation on the ASCII format data. The subroutine reads one of the ASCII format files from the disk. The data read is then converted to numeric data. The numeric data is then returned to the calling routine.

Common Blocks Used by the Subroutine

None

Variables passed to the procedures

Ascii_loc\$ - string.

File_nm\$ - string.

Num - integer.

Variables returned by the procedures

Array - array of integer.

Max - integer.

Min - integer.

Variable definitions

AS - an array of string elements. The size of the array is equal to the Num parameter. The ASCII data are read into this array.

Array - an array of integers. The ASCII data are converted to numeric data and stored in Array. Array is returned to the calling routine.

Ascii_loc\$ - a string variable equal to the operator specified storage location of the ASCII format data.

File_nm\$ - a string variable equal to ASCII file which is to be read from disk.

Formfd\$ - a single character string used as the constant value of the ASCII form feed character (12 decimal, 0C hex).

I - an integer variable used as a loop counter.

Max - an integer variable containing the maximum sampled datum point obtained from the channel being read and crunched.

- Max\$ - a string variable equal to the ASCII value of Max.
- Min - an integer variable containing the minimum sampled datum point obtained from the channel being read and crunched.
- Min\$ - a string variable equal to the ASCII value of Min.
- Num - an integer variable equal to the number of samples collected.

A7.5.4 Write_data Subroutine

The Write_data subroutine stores a channel of the sampled data in numeric format files. The subroutine creates the file and stores the data in the file. The file format is specified by Riblett [13].

Common Blocks Used by the Subroutine

None

Variables passed to the procedures

Data_loc\$ - string.

File_nm\$ - string.

Num - integer.

Variables returned by the procedures

Array - array of integer.

Max - integer.

Min - integer.

Variable definitions

Array - an array of integers. The ASCII data are converted to numeric data and stored in Array. Array is returned to the calling routine.

Data_loc\$ - a string variable equal to the operator specified mass storage specification of device which will contain the numeric data.

File_nm\$ - a string variable equal to the data file to be stored.

Max - an integer variable containing the maximum sampled datum point obtained from the channel being read and crunched.

Min - an integer variable containing the minimum sampled datum point obtained from the channel being read and crunched.

Num - an integer variable equal to the number of samples collected.

A7.5.5 DAPCRUNCH Program Listing

```

10  ! *****
20  !
30  !       DAM DATA FILE, ASCII TO BINARY CONVERSION ROUTINE
40  !
50  !       HP BASIC FILENAME:  DAPCRUNCH
60  !
70  !       Department of Electrical and Computer Engineering
80  !       Kansas State University.
90  !
100 !       REVISION          DATE          PROGRAMMER
110 !       -----          -
120 !       1.0              JUNE 1, 1984    LOREN E. RIBLETT
130 !       1.1              AUGUST 7, 1984  MICHAEL MASTERS
140 !
150 ! *****
160 !
170 !       PURPOSE
180 !       THIS ROUTINE CONVERTS FOUR ASCII FILES OF DAM DATA (NAMESLY
190 !       THE CO2, O2, FLOW, AND TEMPERATURE DATA FILES) CREATED
200 !       BY "DAP.CODE" TO FOUR FILES OF BINARY DATA, ALLOWING FOR
210 !       MORE EFFICIENT DATA STORAGE.
220 !
230 !       ROUTINE(S) CALLED BY THIS ROUTINE
240 !
250 !       AUTOST - USER PROGRAM ACCESS ROUTINE
260 !
270 ! *****
280 !
290 !       NOTE 1:  The files to be converted must be named MONSTER1A_,
300 !       MONSTER2A_, MONSTER3A_, and MONSTER4A_.
310 !       (These files would be named MONSTER1.ASC, MONSTER2.ASC,
320 !       etc. in the PASCAL operating system.)
330 !
340 !       NOTE 2:  Converted files (binary) will be stored on the 8" floppy
350 !       ":HP9895,700,0". The data from MONSTER1A_ is assumed to
360 !       be CO2 data, MONSTER2A_ is O2 data, MONSTER3A_ is flow
370 !       data, and MONSTER4A_ is temperature data.
380 !
390 !       NOTE 3:  Binary data file names in excess of 10 characters should
400 !       not be used.
410 !
420 !       NOTE 4:  ASCII files are purged following the conversion process.
430 !
440 !       NOTE 5:  AUTOST is called following completion of DAPCRUNCH.
450 !
460 ! *****
470 !
480 !       OPTION BASE 1
490 !       COM /Resp_data1/  INTEGER Line1(1:24000),Line2(1:24000)
500 !       COM /Resp_data2/  INTEGER Line3(1:24000),Line4(1:24000)
510 !       COM /Resp_data3/  INTEGER Cmin,Cmax,Omin,Omax,Fmin,Fmax,Tmin,Tmax
520 !       COM /Resp_data4/  INTEGER No_points
530 !       COM /Resp_data5/  C1$(10),O$(10),V$(10),T$(10)
540 !       COM /Cal_data1/  Cal$(10),Date$(25)
550 !       COM /Cal_data2/  INTEGER Co2_dc_offset,O2_dc_offset,Bin_zero_flow,S
560 !       COM /Cal_data3/  REAL Co2_cal,O2_cal
570 !       COM /Cal_data4/  REAL Non_c_i_flowcal,Non_c_e_flowcal
580 !       COM /Cal_data5/  REAL Corr_i_flowcal,Corr_e_flowcal
590 !       COM /Cal_data6/  REAL Ta,Tb,Tc
600 !       COM /Cal_data7/  REAL Time_delay,O1,Pb,Rel_humid,Room_temp
610 !       COM /Anal_data1/  INTEGER Data_available
620 !       INTEGER True

```

```

630 DIM Ascii_loc$(13),Data_loc$(13),File_nm$(10)
640 True=(1=1)
650 Formfd$=CHR$(12)
660 !
670 !*** SPECIAL FUNCTION KEY DEFINITIONS
680 !
690 ON KEY 1 LABEL "DCRUNCH" GOTO Crunch_data
700 ON KEY 9 LABEL "EXIT" GOTO Done
710 Idle:GOTO Idle
720 Crunch_data:OFF KEY
730 Formfd$=CHR$(12)
740 !
750 !           Determine where the ASCII data is stored and where the
760 !           BINARY data will be stored.
770 File_locations(Ascii_loc$,Data_loc$)
780 !
790 !*** GET NUMBER OF DATA POINTS AND MAKE APPROPRIATE DIMENSIONS
800 !
810 BEEP
820 INPUT "ENTER NUMBER OF DATA POINTS TO CRUNCH: ",No_points
830 !
840 !
850 !** Prompt the user for the file names in which the data will be stored
860 BEEP
870 INPUT "ENTER NAME OF CO2 BINARY DATA FILE",C1$
880 BEEP
890 OS="O"&C1$(2,LEN(C1$))
900 INPUT "ENTER NAME OF O2 BINARY DATA FILE: ",OS
910 BEEP
920 VS="V"&C1$(2,LEN(C1$))
930 INPUT "ENTER NAME OF FLOW BINARY DATA FILE: ",VS
940 BEEP
950 TS="T"&C1$(2,LEN(C1$))
960 INPUT "ENTER NAME OF TEMPERATURE BINARY DATA FILE: ",TS
970 !
980 !
990 IF Data_loc$=Ascii_loc$ THEN
1000 PRINT TABXY(1,18);"Install the ASCII data disk in the 8 in. drive"
1010 PRINT
1020 PRINT "Press CONTINUE when you are ready to proceed."
1030 BEEP
1040 PAUSE
1050 PRINT Formfd$
1060 END IF
1070 !
1080 !
1090 !
1100 !
1110 !*** READ AND CRUNCH ASCII DATA MONSTER FILES.
1120 !
1130 Rd_and_crunch(("MONSTER1A_"),Ascii_loc$,No_points,Cmax,Gmin,Line1(*))
1140 Rd_and_crunch(("MONSTER2A_"),Ascii_loc$,No_points,Cmax,Gmin,Line2(*))
1150 Rd_and_crunch(("MONSTER3A_"),Ascii_loc$,No_points,Fmax,Fmin,Line3(*))
1160 Rd_and_crunch(("MONSTER4A_"),Ascii_loc$,No_points,Tmax,Tmin,Line4(*))
1170 !
1180 !
1190 !
1200 !           Store the data.
1210 !
1220 IF Data_loc$=Ascii_loc$ THEN
1230 PRINT TABXY(1,18);"Take out the ASCII data disk and put in the"
1240 PRINT "BINARY data disk."
1250 PRINT
1260 PRINT "Press CONTINUE when you are ready to proceed."
1270 BEEP

```

```

1280     PAUSE
1290     PRINT Formfd$
1300 END IF
1310 Write_data(C1$,Data_loc$,No_points,Cmax,Cmin,Line1(*))
1320 Write_data(O$,Data_loc$,No_points,Cmax,Cmin,Line2(*))
1330 Write_data(V$,Data_loc$,No_points,Fmax,Fmin,Line3(*))
1340 Write_data(T$,Data_loc$,No_points,Tmax,Tmin,Line4(*))
1350 !
1360 !
1370 !           Purge the monster files.
1380 !
1390 IF Data_loc$=Ascii_loc$ THEN
1400     PRINT TABXY(1,18);"Exchange the BINARY data disk and insert"
1410     PRINT "the ASCII data disk."
1420     PRINT
1430     PRINT "Press CONTINUE when you are ready to proceed."
1440     BEEP
1450     PAUSE
1460 END IF
1470 PURGE "MONSTER1A."&Ascii_loc$
1480 PURGE "MONSTER2A."&Ascii_loc$
1490 PURGE "MONSTER3A."&Ascii_loc$
1500 PURGE "MONSTER4A."&Ascii_loc$
1510 ASSIGN @Path TO "DISK_STATA"&Ascii_loc$
1520 OUTPUT @Path;"EMPTY"
1530 ASSIGN @Path TO *
1540 !
1550 !*** RETURN TO AUTOST
1560 !
1570 BEEP 1200,2
1580 Data_available=True
1590 PRINT Formfd$
1600 PRINT "DATA FILE COMPACTION COMPLETE. RETURNING TO AUTOST"
1610 Done:OFF KEY
1620 MASS STORAGE IS ":INTERNAL"
1630 LOAD "AUTOST",1
1640 END
1650 !
1660 !
1670 !
1680 SUB Rd_and_crunch(File_nm$,Ascii_loc$,INTEGER Num,Max,Min,Array(*))
1690     ALLOCATE A$(1:Num)[4],Max$(4),Min$(4)
1700     INTEGER I
1710     Formfd$=CHR$(12)
1720 !
1730 !
1740 !           Read the ASCII file
1750 !
1760     DISP "Now reading in the ASCII file ";File_nm$
1770     ASSIGN @Path TO File_nm&&Ascii_loc$
1780     ENTER @Path;Max$,Min$
1790     ENTER @Path;A$(*)
1800 !
1810 !           *** CONVERT ASCII DATA TO BINARY
1820 !
1830     DISP "Converting the "&File_nm&&" file to Int. values."
1840     Max=VAL(Max$)
1850     Min=VAL(Min$)
1860     FOR I=1 TO Num
1870         Array(I)=VAL(A$(I))
1880     NEXT I
1890     ASSIGN @Path TO *
1900     DISP
1910 SUBEND
1920 !

```

```

1930 !
1940 !
1950 !
1960 SUB Write_data(File_nm$,Data_loc$,INTEGER Num,Max,Min,Array(*))
1970 !
1980 !*** CREATE BINARY DATA FILE FOR DATA
1990 !
2000     DISP "Now storing the Integer data file "&File_nm$
2010     CREATE BDAT File_nm$&Data_loc$,1,2.0*(Num+2)
2020     ASSIGN @Path TO File_nm$&Data_loc$
2030     ON END @Path GOTO Exit_sub
2040 !
2050 !
2060 !*** WRITE BINARY DATA
2070 !
2080     OUTPUT @Path;Max,Min
2090     OUTPUT @Path;Array(*)
2100 Exit_sub:ASSIGN @Path TO *
2110     DISP
2120 SUBEND
2130 !
2140 !
2150 !
2160 SUB File_locations(Ascii_loc$,Data_loc$)
2170 !
2180     DIM Msi_devices$(1:4)[13]
2190     Msi_devices$(1)=":HP9895,702,1"
2200     Msi_devices$(2)=":HP9895,702,2"
2210     Msi_devices$(3)=":HP9895,700,0"
2220     Formfd$=CHR$(12)
2230     PRINT Formfd$
2240     PRINT
2250     PRINT "Mass Storage devices"
2260     PRINT "    1.  The hard disk, platter 1"
2270     PRINT "    2.  The hard disk, platter 2"
2280     PRINT "    3.  The 8 inch floppy disk."
2290     BEEP
2300     INPUT "Which storage location contains the ASCII data",A
2310     Ascii_loc$=Msi_devices$(A)
2320     Data_loc$=Msi_devices$(3)
2330     PRINT Formfd$
2340 SUBEND

```

A7.6 ANALYSIS: a Basic Program Which Computes the Respiratory Parameters

The ANALYSIS program computes the breath-by-breath respiratory parameters from the sampled respiratory signals. ANALYSIS uses the respiratory data and performs the calculations described in Chapter IV and Appendix III. The program has the ability to display the calculated respiratory parameters in a variety of formats. The parameters may be plotted, two parameters per plot, or printed in tabular format. The parameters calculated for individual breaths may be displayed or the parameters for several breaths may be combined and averaged. Averaging is done by one of two methods, average the parameter values of a specified number of breaths or average the parameter values of breaths appearing in a window of time.

A7.6.1 The Main Routine of ANALYSIS

The main routine of ANALYSIS calculates the respiratory parameters. The routine relies on the Calc_sig_val subroutine to compute the fractional concentration of CO_2 and O_2 and the incremental volume for each sample. The Expiration and Inspiration functions are used to determine if a flow value is an inspiratory or an expiratory flow. The calculated respiratory parameters are displayed using the Disp_results subroutine. The main routine provides the plotting of the sampled data, displays the average respiratory values for the analyzed window, calculates the GMS time delay, and reads the respiratory data and calibration data from disk files.

Common blocks used by the subroutine

<u>Common Block</u>	<u>Variables in the block</u>
Anal_data1	- Data_available
Anal_data2	- False, True
Anal_data3	- Co2_prod, Insp_min_vent, O2_cons, Time_of_brth
Anal_data4	- Expr_min_vent, Resp_freq, V_tid_expr, V_tid_insp
Anal_data5	- Breath_good, Formfd\$, Resp_quotient
Anal_data5a	- Frc_co2_prod, Frc_o2_cons, Volume_of_lung
Anal_data6	- Corr_flag, Room_fh2o, T
Anal_data7	- Fh2o_sat, Vap

Anal_data8 - Resp_var
 Anal_data9 - Comment\$, Name\$
 Cal_data1 - Cal\$, Date\$
 Cal_data2 - Bin_zero_flow, Co2_dc_offset, O2_dc_offset
 Cal_data3 - Co2_cal, O2_cal
 Cal_data4 - Non_c_e_flowcal, Non_c_i_flowcal
 Cal_data5 - Corr_e_flowcal, Corr_i_flowcal
 Cal_data6 - Ta, Tb, Tc
 Cal_data7 - Ol, Pb, Rel_humid, Room_temp, Time_delay
 Resp_data1 - Line1, Line2
 Resp_data2 - Line3, Line4
 Resp_data3 - Cmax, Cmin, Fmax, Fmin, Omax, Omin, Tmax,
 Resp_data4 - No_points
 Resp_data5 - C1\$, O\$, T\$, V\$

Variable definitions

A - an integer variable used as a pointer into the flow and temperature data arrays during integration.
 Adiff - a real variable equal to the difference between Asum and Bsum.
 Air_expr - a real variable equal to the volume of air expired for the current breath being analyzed.
 Air_insp - a real variable equal to the volume of air inspired for the current breath being analyzed.
 Asum - a real variable containing the area above the CO₂ signal based on the integration limits Beg_pnt and Beg_intg. Used in the calculation of the breath-by-breath time delay.
 Avco2prod - a real variable equal to the average volume of CO₂ produced per breath
 Avg_air_expr - a real variable equal to the average expiratory tidal volume of the subject.
 Avg_air_insp - a real variable equal to the average expiratory tidal volume of the subject.
 Avg_co2_expr - a real variable equal to the average volume of CO₂ expired per breath.
 Avg_co2_insp - a real variable equal to the average volume of CO₂ inspired per breath.
 Avg_o2_expr - a real variable equal to the average volume of O₂

- expired per breath.
- Avg_o2_insp - a real variable equal to the average volume of O₂ inspired per breath.
- Avg_time_delay - a real variable equal to the average of the valid time delays computed on a breath-by-breath basis.
- Avo2cons - a real variable equal to the average volume of O₂ consumed per breath.
- AS - a string constant equal to 'Air' and used in printing the analyzed results.
- Begtime_colct - a real variable equal to the experimental time at which collection of the breath-by-breath data began.
- Beg_intg - a real variable used as an integration marker in the determination of the breath-by-breath time delay. The area above the curve is found by integrating from the point of maximum CO₂ to Beg_intg. The area below the curve is found by integrating from Beg_intg to the ending point. Beg_intg is slid from the point of maximum CO₂ to the ending point.
- Beg_pt - a real variable used as a pointer for the CO₂ signal which points to where integration above the CO₂ signal begins (used in the calculation of the breath-by-breath time delay).
- Best_index - a real variable used as a pointer which points to the location in CO₂ and O₂ signal arrays corresponding to the beginning of inspiration (used in the calculation of the breath-by-breath time delay).
- Best_match - a real variable containing the smallest difference in the area above and the area below the fractional CO₂ signal (used in the calculation of the breath-by-breath time delay).
- Bin_zero_flow - an integer variable containing the flow sample value equal to zero flow through the PTM.
- Body_temp - a real variable equal to the subject's body temperature.
- Breath_count - an integer variable used as a breath counter and a pointer into the Resp_var array.
- Breath_good - an integer used as a constant value which points to the good or bad breath parameter in the respiratory

variable array.

- Bsum - a real variable containing the area below the CO₂ signal based on the integration limits Beg_intg and End_pt (used in the calculation of the breath-by-breath time delay)
- Btps_to_stpd - a real variable equal to the BTPS to STPD conversion factor.
- B_by_b_output - an integer variable used as a Boolean value. The variable is true if the breath-by-breath output is not to be omitted and is false if the output is to be omitted.
- B\$ - a string constant equal to 'O2' and used in printing the analyzed results.
- C - a real variable equal to the Co2_dc_offset. C is used to shorten the length of the statements involved in the calculation of the breath-by-breath time delay.
- Cal\$ - a string variable containing the name of the calibration file.
- Chng_fco2 - a real variable equal to the change in the end expirate concentration of CO₂ between the current breath being analyzed and the previous breath.
- Chng_fo2 - a real variable equal to the change in the end expirate concentration of O₂ between the current breath being analyzed and the previous breath.
- Chng_lung_vol - a real variable equal to the change in the lung volume between the current breath being analyzed and the previous breath.
- Gmax - an integer variable containing the maximum sampled datum point obtained from the CO₂ channel, Line1.
- Gmin - an integer variable containing the minimum sampled datum point obtained from the CO₂ channel, Line1.
- Comment\$ - a string variable containing an operator specified comment.
- Corr_flowcal - a real variable containing the PTG calibration factor for expiratory flows determined using temperature corrections.
- Corr_flag - an integer variable used as a Boolean value which indicates if the temperature corrections are to be used in computing the respiratory flow.
- Corr_i_flowcal - a real variable containing the PTG calibration

factor for inspiratory flows determined using temperature corrections.

Co2max - the maximum CO_2 value for the breath (used in the computation of the breath-by-breath time delay).

Co2min - the minimum CO_2 value for the breath (used in the computation of the breath-by-breath time delay).

Co2prod - a real variable equal to the volume of CO_2 produced for the current breath being analyzed.

Co2_cal - a real variable equal to the CO_2 calibration factor.

Co2_dc_offset - an integer variable containing the sampled CO_2 value corresponding to room air.

Co2_expr - a real variable equal to the volume of CO_2 expired for the current breath being analyzed.

Co2_insp - a real variable equal to the volume of CO_2 inspired for the current breath being analyzed.

Co2_prod - an integer used as a constant value which points to the computed rate of CO_2 production parameter in the respiratory variable array.

Ctmax - a real variable equal to the temperature corresponding to T_{max} .

Ctmin - a real variable equal to the temperature corresponding to T_{min} .

C1\$ - a string variable containing the name of the CO_2 data file.

C\$ - a string constant equal to 'CO2' and used in printing the analyzed results.

Data_available - an integer variable used as a Boolean value which indicates if respiratory data are present in memory.

Date\$ - a string variable containing the date data were collected.

D\$ - a string constant equal to 'Inspired' and used in printing the analyzed results.

End - a real variable equal to the ending point to analyze or plot.

End_intg - a real variable equal to End_pt.

End_pt - a real variable used as a pointer to the CO_2 signal which points to where integration ends (used in the calculation of the breath-by-breath time delay).

- Expr_begin - an integer variable equal to the first expiratory flow data point of the current breath being analyzed.
- Expr_flowcal - a real variable set equal to Non_c_e_flowcal if temperature corrections are not used and set equal to Corr_e_flowcal if temperature corrections are used.
- Expr_min_vent - an integer used as a constant value which points to the computed expiratory minute ventilation parameter in the respiratory variable array.
- Expr_time - a real variable equal to the duration of the expiratory cycle of the current breath being analyzed.
- ES - a string constant equal to 'Expired' and used in printing the analyzed results.
- False - an integer variable used as a constant Boolean value of False.
- Fco2 - a real variable equal to the fractional concentration of CO_2 in the sample being integrated.
- Fh2o_sat - a real valued, 250 element array used to hold the saturated relative concentrations of water vapor in room air between 20°C and 45°C.
- Final_index - a real variable equal to the final point in the window of data which has been analyzed.
- Final_insp - an integer variable equal which points to the beginning point of the last inspiration analyzed.
- Fmax - an integer variable containing the maximum sampled datum point obtained from the flow channel, Line3.
- Fmin - an integer variable containing the minimum sampled datum point obtained from the flow channel, Line3.
- Formfd\$ - a single character string used as the constant value of an ASCII form feed character (12 decimal, 0C hex).
- Found - an integer variable used as a Boolean value. Found is used in the search of the first point to be integrated. Found is false until the first inspiratory flow is found.
- Fo2 - a real variable equal to the fractional concentration of O_2 in the sample being integrated.
- Frac_h2o_body - the fractional concentration of water vapor at body temperature.
- Frac_co2_1 - a real variable equal to the end expirate fractional concentration of CO_2 of the current breath being analyzed.

- Frac_co2_2 - a real variable equal to the end expirate fractional concentration of CO_2 of the breath previous to the current breath being analyzed.
- Frac_o2_1 - a real variable equal to the end expirate fractional concentration of O_2 of the current breath being analyzed.
- Frac_o2_2 - a real variable equal to the end expirate fractional concentration of O_2 of the breath previous to the current breath being analyzed.
- Frc_co2prod - a real variable equal to the CO_2 produced during the current breath, taking into account the change in lung volume.
- Frc_co2_prod - an integer used as a constant value which points to the computed alveolar CO_2 production parameter in the respiratory variable array.
- Frc_flag - a real variable used as a Boolean value which is true if FRC computations are used and is false otherwise.
- Frc_o2cons - a real variable equal to the O_2 consumed during the current breath, taking into account the change in lung volume.
- Frc_o2_cons - an integer used as a constant value which points to the computed alveolar O_2 consumption parameter in the respiratory variable array.
- F\$ - a string constant equal to '(liters)' and used in printing the analyzed results.
- Good_exp_count - an integer variable used as a counter for the number of good expirations.
- Good_insp_count - an integer variable used as a counter for the number of good inspirations.
- G\$ - a string constant equal to 'BTPS' and used in printing the analyzed results.
- H\$ - a string constant equal to 'STPD' and used in printing the analyzed results.
- I - an integer variable used as a loop counter.
- Incr - a real variable equal to an increment value which is used as the increment parameter of the FOR loops used to label the X axes in the data plotting routine.
- Incr_vol - a real variable equal to the incremental volume of air computed from the flow sample.

- `Init_index` - a real variable equal to the first point in the window of data which is analyzed.
- `Insp_count` - an integer variable equal to the first inspiratory point of the current breath.
- `Insp_flowcal` - a real variable set equal to `Non_c_i_flowcal` if temperature corrections are not used and set equal to `Corr_i_flowcal` if temperature corrections are used.
- `Insp_min_vent` - an integer used as a constant value which points to the computed inspiratory minute ventilation parameter in the respiratory variable array.
- `Insp_time` - a real variable equal to the duration of the inspiratory cycle of the current breath being analyzed.
- `Left` - a real variable equal to the X value of the left hand side of the data plots.
- `Line1` - an integer array, of 24,000 elements, containing the sampled values obtained from the CO_2 channel, channel 1, of the DAM.
- `Line2` - an integer array, of 24,000 elements, containing the sampled values obtained from the O_2 channel, channel 2, of the DAM.
- `Line3` - an integer array, of 24,000 elements, containing the sampled values obtained from the flow channel, channel 3, of the DAM.
- `Line4` - an integer array, of 24,000 elements, containing the sampled values obtained from the temperature channel, channel 4, of the DAM.
- `Lung_vol` - a real variable equal to the calculated lung volume.
- `Max_index` - a real variable used as a pointer into the CO_2 data array where the maximum CO_2 sample for the current breath is observed. (used in the calculation of the breath-by-breath time delay).
- `Max_pnt` - a real variable equal to the sample corresponding to the maximum fractional concentration of CO_2 of the current breath being analyzed.
- `Mid_index` - a real variable used as a pointer into the CO_2 data array where one-half of the maximum fractional concentration of CO_2 is observed in the current breath (used in the calculation of the breath-by-breath time

delay).

Minvole - a real variable equal to the average expiratory minute ventilation of the subject.

Minvoli - a real variable equal to the average inspiratory minute ventilation of the subject.

Min_index - a real variable used as a pointer into the CO₂ data array where the minimum CO₂ sample for the current breath is observed. (used in the calculation of the breath-by-breath time delay).

Name\$ - a string variable containing an operator specified subject name.

Net_lung_chng - a real variable equal to the net change in lung volume for the analyzed window of data.

Non_c_e_flowcal - a real variable containing the PTG calibration factor for expiratory flows determined without the use of temperature corrections.

Non_c_i_flowcal - a real variable containing the PTG calibration factor for inspiratory flows determined without the use of temperature corrections.

No_points - an integer variable containing the number of samples collected.

Num_breaths - a real variable equal to the number of breaths that were analyzed.

Offset - a real variable added to the CO₂ and O₂ array pointers for the plotting of time aligned signals.

O1 - a real variable equal to the fractional concentration of O₂ in the calibration gas.

Omax - an integer variable containing the maximum sampled datum point obtained from the O₂ channel, Line2.

Omin - an integer variable containing the minimum sampled datum point obtained from the O₂ channel, Line2.

O2cons - a real variable equal to the volume of O₂ consumed for the current breath being analyzed.

O2_cal - a real variable equal to the O₂ calibration factor.

O2_cons - an integer used as a constant value which points to the computed rate of O₂ consumption parameter in the respiratory variable array.

O2_dc_offset - an integer variable containing the sampled O₂

- value corresponding to the calibration gas.
- O2_expr - a real variable equal to the volume of O₂ expired for the current breath being analyzed.
- O2_insp - a real variable equal to the volume of O₂ inspired for the current breath being analyzed.
- OS - a string variable containing the name of the O₂ data file.
- P - a real variable equal to the number of data points to be plotted.
- Pb - a real variable equal to the barometric pressure at the time the system was calibrated.
- Ph2o_body - a real variable equal to the saturated partial pressure of water vapor at body temperature.
- QS - a string variable used to obtain the operator's response to a question.
- R - a real variable equal to the respiratory quotient.
- Rel_humid - a real variable equal to the relative humidity at the time the system was calibrated.
- Resp_f - a real variable equal to the average respiratory frequency.
- Resp_freq - an integer used as a constant value which points to the computed respiratory frequency parameter in the respiratory variable array.
- Resp_quotient - an integer used as a constant value which points to the computed respiratory quotient parameter in the respiratory variable array.
- Resp_var - a real valued array containing the calculated breath-by-breath respiratory parameters. Resp_var is a two dimensional array, the first dimension is the respiratory variable and the second dimension is the breath number. A more detailed description of the respiratory variable array is given in Section A7.2 of this appendix.
- Right - a real variable equal to the X value on the right hand side of the data plots.
- Room_fh2o - a real variable equal to the concentration of water vapor in room air.
- Room_temp - a real variable equal to the room temperature at the time the system was calibrated.

- S - a real variable equal to the sampling frequency.
- Start - a real variable equal to the beginning point to be analyzed or plotted.
- Still_calc - a real variable used as a Boolean value which indicates if data remains in the window to be analyzed.
- Stpd_to_btps - a real variable equal to the STPD to BTPS volume conversion factor.
- T - a real variable equal to the sampling period used to collect the respiratory data.
- Ta - a real variable equal to the second order calibration coefficient for converting the collected temperature data to units of $^{\circ}\text{C}$.
- Tb - a real variable equal to the first order calibration coefficient for converting the collected temperature data to units of $^{\circ}\text{C}$.
- Tc - a real variable equal to the zero order calibration coefficient for converting the collected temperature data to units of $^{\circ}\text{C}$.
- Temp - a real variable equal to the temperature corresponding to a sample of the temperature channel.
- Temporary - a real variable used as an intermediate variable. Temporary is used when the average results are printed.
- Temp_a - a real variable used by the breath-by-breath time delay routine to preserve the variable 'A', the flow and temperature signal pointer.
- Temp_z - a real variable used by the breath-by-breath time delay routine to preserve the variable 'Z', the CO_2 and O_2 signal pointer.
- Time_delay - an integer variable equal to the GMS time delay in milli-seconds.
- Time_delay_cnt - a real variable equal to the number of valid time delays computed on a breath-by-breath basis.
- Time_delay_flag - a real variable which to indicate the type of time delay used. The flag is equal to zero for a fixed time delay, equal to one for a variable time delay, and equal to two for a variable time delay with an invalid computed time delay.
- Time_delay_sum - a real variable equal to the sum of the valid

- time delays and is used with Time_delay_cnt to compute the Avg_time_delay.
- Time_of_brth - an integer used as a constant value which points to the time of breath parameter in the respiratory variable array.
- Tmax - an integer variable containing the maximum sampled datum point obtained from the temperature channel, Line4.
- Tmin - an integer variable containing the minimum sampled datum point obtained from the temperature channel, Line4.
- Tot_co2_exp - a real variable equal to the total volume of CO_2 expired in the analyzed window of data.
- Tot_co2_insp - a real variable equal to the total volume of CO_2 inspired for all breaths in the analyzed window of data.
- Tot_co2_prod - a real variable equal to the total volume of CO_2 produced for all breaths in the analyzed window of data.
- Tot_o2_cons - a real variable equal to the total volume of O_2 consumed for all breaths in the analyzed window of data.
- Tot_o2_exp - a real variable equal to the total volume of O_2 expired in the analyzed window of data.
- Tot_o2_insp - a real variable equal to the total volume of O_2 inspired for all breaths in the analyzed window of data.
- Tot_time - a real variable equal to the duration of the respiratory cycle currently being analyzed.
- Tot_time_expr - a real variable equal to the total time of expiration during the analyzed window of data.
- Tot_time_insp - a real variable equal to the total time of inspiration during the analyzed window of data.
- Tot_time_resp - a real variable equal to the total time of respiration.
- Tot_vol_exp - a real variable equal to the total volume expired in the analyzed window of data.
- Tot_vol_insp - a real variable equal to the total volume inspired for all breaths in the analyzed window of data.
- True - an integer used as the constant Boolean value of true.
- TS - a string variable containing the name of the temperature data file.
- Vap - a real valued, 250 element array used to hold the saturated water vapor pressure between 20°C and 45°C .

- Volume_of_lung - an integer used as a constant value which points to the computed lung volume parameter in the respiratory variable array.
- V_dot_co2 - a real variable equal to the average rate of CO₂ production.
- V_dot_o2 - a real variable equal to the average rate of O₂ consumption.
- V_tid_expr - an integer used as a constant value which points to the computed expiratory tidal volume parameter in the respiratory variable array.
- V_tid_insp - an integer used as a constant value which points to the computed inspiratory tidal volume parameter in the respiratory variable array.
- V\$ - a string variable containing the name of the flow data file.
- Wye - a real variable used as a loop counter in the breath-by-breath time delay calculation.
- Z - an integer variable used as a pointer into the CO₂ and O₂ data arrays during integration.

A7.6.2 Avg_breath Subroutine

The Avg_breath subroutine is used to compute the average of a specified number of breath-by-breath values of any respiratory parameter in the respiratory variable array. Those breaths specified as 'bad' breaths may be omitted in the computation of the average. The subroutine is used by the Max_min, Plot_value, and Print_results subroutines.

Common blocks used by the subroutine

<u>Common Block</u>	<u>Variables in the block</u>
Anal_data3	Co2_prod, Insp_min_vent, O2_cons, Time_of_brth
Anal_data5	Breath_good, Formfd\$, Resp_quotient
Anal_data5a	Frc_co2_prod, Frc_o2_cons, Volume_of_lung
Anal_data8	Resp_var
Plot_resp_data1	Omit_bad, Num_breaths, No_b_avg

Variables passed to the subroutine

Br_pntr - integer.

Variable - integer.

Variables returned by the subroutine

Average - real.

Num_badBreaths - integer.

Time - real.

Variable definitions

Average - a real variable equal to the average of the specified number of breath-by-breath values of the specified respiratory parameter.

Breath_good - an integer used as a constant value which points to the good or bad breath parameter in the respiratory variable array.

Br_pntr - an integer variable used as a pointer into the breath dimension of the respiratory variable array. Br_pntr points to the first breath to be included in the average.

J - an integer variable used as a loop counter.

No_b_avg - an integer variable equal to the number of breath-by-breath values to be averaged.

Num_badBreaths - an integer variable equal to the number of bad breaths that are not included in the average.

NumBreaths - a real variable equal to the number of breaths to be analyzed.

Omit_bad - an integer variable used as a Boolean flag which indicates if the 'bad' breaths are not to be included in the average.

Pointer - an integer variable used as a pointer into the breath dimension of the respiratory variable array.

Resp_var - a real valued array containing the calculated breath-by-breath respiratory parameters.

Time - a real variable equal to the time that is midway between the first breath included in the average and the last breath included in the average.

Time_of_brth - an integer used as a constant value which points to the time of breath parameter in the respiratory variable array.

Variable - an integer variable used as a pointer into the respiratory variable dimension of the respirator variable array. Variable is equal to the respiratory parameter to be averaged.

A7.6.3 Avg_window Subroutine

The Avg_window subroutine is used to compute the average of several breath-by-breath values for all breaths occurring in a specified window in time. Any respiratory parameter in the respiratory variable array may be averaged. Those breaths specified as 'bad' breaths may be omitted in the computation of the average. The subroutine is used by the Max_min, Plot_value, and Print_results subroutines.

Common blocks used by the subroutine

<u>Common Block</u>	<u>Variables in the block</u>
Anal_data3	- Co2_prod, Insp_min_vent, O2_cons, Time_of_brth
Anal_data5	- Breath_good, Formfd\$, Resp_quotient
Anal_data5a	- Frc_co2_prod, Frc_o2_cons, Volume_of_lung
Anal_data8	- Resp_var
Plot_resp_data1	- Omit_bad, Num_breaths, No_b_avg
Plot_resp_data2	- Start_time, End_time, W_period, W_width

Variables passed to the subroutine

Br_pntr - integer.
Variable - integer.
W_cntr - real.

Variables returned by the subroutine

Average - real.
Br_in_w_flag - integer.
Br_pntr - integer.

Variable definitions

Average - a real variable equal to the average of all breaths occurring in the time window.
Br_in_w_flag - an integer variable used as a Boolean value which indicates if breaths were found in the specified time

window.

Breath_good - an integer used as a constant value which points to the good or bad breath parameter in the respiratory variable array.

Br_pntr - an integer variable used as a pointer into the breath dimension of the respiratory variable array. Br_pntr points to the first breath to be included in the average.

Fstbr_in_w_fnd - an integer variable used as a Boolean value which indicates when the first breath in the specified window is found.

Left_edge_w - a real variable equal to the time of the left side of the window.

Num_breaths - a real variable equal to the number of breaths that were analyzed.

Num_b_in_window - an integer variable equal to the number of breaths in the window which were averaged.

Omit_bad - an integer variable used as a Boolean flag which indicates if the 'bad' breaths are not to be included in the average.

Resp_var - a real valued array containing the calculated breath-by-breath respiratory parameters.

Time_of_brth - an integer used as a constant value which points to the time of breath parameter in the respiratory variable array.

True - an integer used as the constant Boolean value of true.

Variable - an integer variable used as a pointer into the respiratory variable dimension of the respirator variable array. Variable is equal to the respiratory parameter to be averaged.

W_cntr - a real variable equal to the time of the center of the window.

W_wdth - a real variable equal to the time width of the window.

A7.6.4 Calc_sig_val Subroutine

The Calc_sig_val subroutine calculates the physical signal values from one set of samples of the four channels. The subroutine converts the CO₂ sample to the fractional concentration of CO₂ and the O₂ sample to the fractional concentration of O₂. The incremental volume for the

sample from the flow sample is calculated. If the temperature and viscosity corrections are to be performed the incremental volume is converted to STPD conditions. This conversion is accomplished using the temperature sample, ambient conditions, the fractional gas concentrations, and the relative viscosity function, Rel_viscos (A7.6.14). The Calc_sig_val subroutine is similar to the Calc_Incr_Vol procedure (A6.1.4) used by the calibration program, CAP2 (A6.1).

Common blocks used by the subroutine

<u>Common Block</u>	<u>Variables in the block</u>
Anal_data6	- Corr_flag, Room_fh2o, T
Anal_data7	- Fh2o_sat, Vap
Cal_data2	- Bin_zero_flow, Co2_dc_offset, O2_dc_offset
Cal_data3	- Co2_cal, O2_cal
Cal_data6	- Ta, Tb, Tc
Cal_data7	- Ol, Pb, Rel_humid, Room_temp, Time_delay
Resp_data1	- Line1, Line2
Resp_data2	- Line3, Line4

Variables passed to the procedure

A - integer.
 Insp_or_expr\$ - string.
 Z - integer.

Variables returned by the procedure

Fco2 - real.
 Fo2 - real.
 Incr_vol - real.

Variable definitions

A - an integer variable used as a pointer into the flow and temperature data arrays during integration.
 Bin_flow - a real variable proportional to the flow. The value is computed by subtracting the value of zero flow and dividing by the relative viscosity.
 Bin_zero_flow - an integer variable containing the flow sample value corresponding to zero flow through the PTM.
 Corr_flag - an integer variable used as a Boolean value which indicates if the temperature corrections are used in

computing the respiratory flow.

Co2_cal - a real variable equal to the CO₂ calibration factor.

Co2_dc_offset - an integer variable containing the sampled CO₂ value corresponding to room air.

Fco2 - a real variable equal to the fractional concentration of CO₂ calculated from the CO₂ sample. This concentration value neglects the amount of water vapor in the respiratory flow gas.

Fco2_wet - a real variable equal to the fractional concentration of CO₂ in the wet respiratory gas. This concentration value takes into account the amount of water vapor in the respiratory flow gas.

Fh2o - a real variable equal to the fractional concentration of water vapor in the respiratory flow gas.

Fh2o_sat - a real valued, 250 element array used to hold the saturated relative concentrations of water vapor in room air between 20°C and 45°C.

Fn2_wet - a real variable equal to the fractional concentration of N₂ in the wet respiratory gas. This concentration value takes into account the amount of water vapor in the respiratory flow gas.

Fo2 - a real variable equal to the fractional concentration of O₂ calculated from the O₂ sample. This concentration value neglects the amount of water vapor in the respiratory flow gas.

Fo2_wet - a real variable equal to the fractional concentration of O₂ in the wet respiratory gas. This concentration value takes into account the amount of water vapor in the respiratory flow gas.

Incr_vol - a real variable proportional to the incremental volume of gas computed from the flow sample. Multiplying Incr_vol by the flow calibration factor yields the incremental volume in liters. However, the multiplication of the sample by the flow calibration factor is done after the entire respiratory cycle is integrated in order to reduce computation time in the integration loop.

Insp_or_expr\$ - a string variable used to indicate if the sample being analyzed is an inspiratory or an expiratory flow.

- Line1 - an integer array, of 24,000 elements, containing the sampled values obtained from the CO₂ channel, channel 1, of the DAM.
- Line2 - an integer array, of 24,000 elements, containing the sampled values obtained from the O₂ channel, channel 2, of the DAM.
- Line3 - an integer array, of 24,000 elements, containing the sampled values obtained from the flow channel, channel 3, of the DAM.
- Line4 - an integer array, of 24,000 elements, containing the sampled values obtained from the temperature channel, channel 4, of the DAM.
- O1 - a real variable equal to the fractional concentration of O₂ in the calibration gas.
- O2_cal - a real variable equal to the O₂ calibration factor.
- O2_dc_offset - an integer variable containing the sampled O₂ value corresponding to the calibration gas.
- Pb - a real variable equal to the barometric pressure at the time the system was calibrated.
- Rel_Viscosity - a real variable equal to the viscosity of the respiratory gas relative to the viscosity of room air under STPD conditions.
- Room_fh2o - a real variable equal to the relative concentration of water vapor in room air.
- T - a real variable equal to the sampling period used to collect the respiratory data.
- Ta - a real variable equal to the second order calibration coefficient for converting the collected temperature data to units of °C.
- Tb - a real variable equal to the first order calibration coefficient for converting the collected temperature data to units of °C.
- Tc - a real variable equal to the zero order calibration coefficient for converting the collected temperature data to units of °C.
- Temperature - a real variable equal to the temperature of the flow gas.
- Z - an integer variable used as a pointer into the CO₂ and

O₂ data arrays during integration.

A7.6.5 Disp_results Subroutine

The Disp_results subroutine provides the main control for the display of the respiratory parameters. The subroutine provides the ability to generate two types of respiratory parameter output, a plot of any two respiratory parameters or a printed copy of all respiratory parameters. The values of a respiratory parameter from several breaths may be averaged by two techniques: breath averaging or window averaging.

Common Block

Variables in the block

Anal_data2 - False, True
 Anal_data3 - Co2_prod, Insp_min_vent, O2_cons, Time_of_brth
 Anal_data4 - Expr_min_vent, Resp_freq, V_tid_expr, V_tid_insp
 Anal_data5 - Breath_good, Formfd\$, Resp_quotient
 Anal_data5a - Frc_co2_cons, Frc_o2_cons, Volume_of_lung
 Anal_data8 - Resp_var
 Anal_data9 - Comment\$, Name\$
 Cal_data1 - Cal\$, Date\$
 Plot_resp_data1 - Omit_bad, Num_breaths, No_b_avg
 Plot_resp_data2 - Start_time, End_time, W_period, W_width

Variables passed to the procedure

Breaths - integer.
 Corr_flag - integer.

Variables returned by the procedure

None

Variable definitions

Avg_bad_comnt\$ - a string variable which is used to label the plot with the type of averaging technique used and indicate if bad breaths are omitted.
 Avg_type\$ - a string variable which indicates the type of averaging technique used to average the respiratory parameters.
 Breaths - an integer variable equal to the number of breaths contained in the respiratory parameter array.

- Corr_flag - an integer variable used as a Boolean value which indicates if the temperature corrections are used in computing the respiratory flow.
- Date\$ - a string variable containing the date the data were collected.
- End_time - a real variable equal to the ending time of the respiratory results display.
- Event1\$ - a string variable used as an operator defined event corresponding to the time defined by Time1\$. The event is labeled on plots of respiratory data.
- Event2\$ - a string variable used as an operator defined event corresponding to the time defined by Time2\$. The event is labeled on plots of respiratory data.
- False - an integer variable used as a constant Boolean value of False.
- Fig1 - an integer variable equal to the first respiratory parameter to be plotted.
- Fig2 - an integer variable equal to the second respiratory parameter to be plotted.
- Formfd\$ - a single character string used as the constant value of an ASCII form feed character (12 decimal, 0C hex).
- Max1 - a real variable equal to the maximum value to be plotted for the first respiratory variable.
- Max2 - a real variable equal to the maximum value to be plotted for the second respiratory variable.
- Min1 - a real variable equal to the minimum value to be plotted for the first respiratory variable.
- Min2 - a real variable equal to the minimum value to be plotted for the second respiratory variable.
- Name\$ - a string variable containing the subject name.
- No_b_avg - an integer variable equal to the number of breaths to average when performing breath averaging.
- Num_breaths - a real variable equal to the number of breaths in the respiratory variable array.
- Omit_bad - an integer variable used as a Boolean flag which indicates if the 'bad' breaths are not to be included in the average.
- Plot_dev\$ - a string variable containing the plotting device to

be used to plot the respiratory parameters.

QS - a string variable used to obtain the operator's response to a question.

Resp_quotient - an integer used as a constant value which points to the computed respiratory quotient parameter in the respiratory variable array.

Resp_var - a real valued array containing the calculated breath-by-breath respiratory variables. Resp_var is a two dimensional array, the first dimension is the respiratory variable and the second dimension is the breath number. A more detailed description of the respiratory variable array is given in Section A7.2 of this appendix.

Result_type\$ - a string variable used to indicate the type of output used to display the respiratory parameters.

Start_time - a real variable equal to the starting time of the respiratory results display.

Time1\$ - a string variable used as an operator defined time mark. The time is labeled on plots of respiratory data.

Time2\$ - a string variable used as an operator defined time mark. The time is labeled on plots of respiratory data.

Title\$ - a string variable used as an operator defined title to be placed on the plot.

Time_of_brth - an integer used as a constant value which points to the beginning time of each breath in the respiratory variable array.

True - an integer used as the constant Boolean value of true.

W_period - a real variable equal to the period of which the window is slid.

W_width - a real variable equal to the time width of the window.

A7.6.6 Expand_dump Subroutine

The Expanded_dump subroutine generates a full page graphics dump of the HP9826's screen on the thermal printer. Expanded_dump is not called within the program but may be called by the operator. While the program is paused the operator must type the command below and press the 'EXECUTE' key.

CALL Expanded_dump

Common blocks used by the subroutine

None

Variables passed to the subroutine

None

Variables returned by the subroutine

None

Variable definitions

None

A7.6.7 Expiration Function

The Expiration function tests a flow sample to determine if the flow is an expiratory flow. The function returns an integer value which acts as a Boolean variable. The returned value is equal to true if the flow is an expiratory flow and is equal to false if the flow is not an expiratory flow. An expiratory flow sample must meet one of the following two conditions.

1. The flow sample is greater than the sample corresponding to zero flow, or
2. one of the next five flow samples are greater than or equal to zero flow.

These conditions were defined by Riblett [13].

Common Blocks Used by the functionCommon
BlockVariables in the
block

Cal_data2 - Bin_zero_flow, Co2_dc_offset, O2_dc_offset

Resp_data2 - Line3, Line4

Variables passed to the function

Pntr - integer.

Variable definitions

Bin_zero_flow - an integer variable containing the flow sample corresponding to zero flow through the PTM.

Expiration - an integer variable used as a Boolean value which

- indicates if the sample is an expiratory flow.
- 1 - an integer variable used as a loop counter.
- Line3 - an integer array, of 24,000 elements, containing the sampled values obtained from the flow channel, channel 3, of the DAM.
- Pntr - an integer variable equal to the flow sample being tested.

A7.6.8 Inspiration Function

The Inspiration function tests a flow sample to determine if the flow is an inspiratory flow. The function returns an integer value which acts as a Boolean variable. The returned value is equal to true if the flow is an inspiratory flow and is equal to false if the flow is not an inspiratory flow. An inspiratory flow sample must meet one of the following two conditions.

1. The flow sample is less than the sample corresponding to zero flow, or
2. one of the next five flow samples are less than or equal to zero flow.

These conditions were defined by Riblett [13].

Common Blocks Used by the function

<u>Common Block</u>	<u>Variables in the block</u>
Cal_data2	Bin_zero_flow, Co2_dc_offset, O2_dc_offset
Resp_data2	Line3, Line4

Variables passed to the function

Pntr - integer.

Variable definitions

- Bin_zero_flow - an integer variable containing the flow sample corresponding to zero flow through the PTM.
- Inspiration - an integer variable used as a Boolean value which indicates if the sample is an inspiratory flow.
- I - an integer variable used as a loop counter.
- Line3 - an integer array, of 24,000 elements, containing the sampled values obtained from the flow channel, channel 3,

of the DAM.

Pntr - an integer variable equal to the flow sample being tested.

A7.6.9 Make_axes Subroutine

The Make_axes subroutine generates a set of axes for plots of the respiratory parameters. The scale of the plot is declared from the maximum and minimum values to be plotted and the starting and ending times. The X-axis is labeled with the units of time and the Y-axis is labeled with the respiratory parameter to be plotted.

Common blocks used by the subroutine

<u>Common Block</u>	<u>Variables in the block</u>
Anal_data3	- Co2_prod, Insp_min_vent, O2_cons, Time_of_brth
Anal_data4	- Expr_min_vent, Resp_freq, V_tid_expr, V_tid_insp
Anal_data5	- Breath_good, Formfd\$, Resp_quotient
Anal_data5a	- Frc_co2_cons, Frc_o2_cons, Volume_of_lung
Plot_resp_data2	- Start_time, End_time, W_period, W_width

Variables passed to the subroutine

Corr_flag - integer.
 Max - real.
 Min - real.
 Variable - integer.

Variables returned by the subroutine

None

Variable definitions

Bottom - a real variable equal to the bottom of the plot in terms of the X dimension. The value is slightly less than the minimum value to be plotted.

Co2_prod - an integer used as a constant value which points to the computed rate of CO₂ production parameter in the respiratory variable array.

Corr_flag - an integer variable used as a Boolean value which indicates if the temperature corrections are used in computing the respiratory flow.

End_time - a real variable equal to the ending time of the

respiratory results display.

Expr_min_vent - an integer used as a constant value which points to the computed expiratory minute ventilation parameter in the respiratory variable array.

Frc_co2_prod - an integer used as a constant value which points to the computed alveolar CO_2 production parameter in the respiratory variable array.

Frc_o2_cons - an integer used as a constant value which points to the computed alveolar O_2 consumption parameter in the respiratory variable array.

Headings\$ - a string array of eleven elements. The elements contain heading information of the respiratory parameters. The element specified by Variable is used to label the Y axes of the plot.

Insp_min_vent - an integer used as a constant value which points to the computed inspiratory minute ventilation parameter in the respiratory variable array.

Left - a real variable equal to the X value of the left hand side of the data plots.

Max - a real variable equal to the maximum value to be plotted.

Min - a real variable equal to the minimum value to be plotted.

O2_cons - an integer used as a constant value which points to the computed rate of O_2 consumption parameter in the respiratory variable array.

Resp_freq - an integer used as a constant value which points to the computed respiratory frequency parameter in the respiratory variable array.

Resp_quotient - an integer used as a constant value which points to the computed respiratory quotient parameter in the respiratory variable array.

Right - a real variable equal to the X value on the right hand side of the data plots.

Start_time - a real variable equal to the starting time of the respiratory results display.

Top - a real variable equal to the top of the plot in terms of the X dimension. The value is slightly greater than the

maximum value to be plotted.

Variable - an integer variable which indicates which respiratory parameter is to be plotted.

Volume_of_lung - an integer used as a constant value which points to the computed lung volume parameter in the respiratory variable array.

V_tid_expr - an integer used as a constant value which points to the computed expiratory tidal volume parameter in the respiratory variable array.

V_tid_insp - an integer used as a constant value which points to the computed inspiratory tidal volume parameter in the respiratory variable array.

X - a real variable used as a loop counter to label the time marks on the X axes.

Xtick - the time mark spacing on the X axes.

Y - a real variable used as a loop counter to label values on the Y axes.

Ytick - the spacing of tick marks on the Y axes.

A7.6.10 Max_co2_ptr Function

The Max_co2_ptr function is used to determine the end expirate CO₂ concentration. The function determines a pointer to the maximum fractional concentration of CO₂ during the final stages of expiration. The CO₂ concentration corresponding to this sample is assumed to be the end expirate sample. This subroutine was developed by Pieschl [12] for use with FRC calculations.

Common blocks used by the function

None

Variables passed to the function

A - integer.

Line1 - integer array.

Variable definitions

A - an integer variable used as a pointer into the flow and temperature data arrays during integration.

I - an integer variable used as a loop counter.

Line1 - an integer array, of 24,000 elements, containing the

sampled values obtained from the CO₂ channel, channel 1, of the DAM.

Max - an integer variable equal to the element in the CO₂ array determined to be the maximum sample.

A7.6.11 Max_min Subroutine

The Max_min subroutine is used to determine the maximum and minimum values of a respiratory parameter. The subroutine uses the specified averaging technique (breath averaging or window averaging) to average the values of the parameter. The maximum and minimum values are used to determine the scale for a plot of a respiratory parameter.

Common blocks used by the subroutine

<u>Common Block</u>	<u>Variables in the block</u>
Anal_data8 - Resp_var	
Plot_resp_data1 - Omit_bad, Num_breaths, No_b_avg	
Plot_resp_data2 - Start_time, End_time, W_period, W_width	

Variables passed to the subroutine

Avg_type\$ - string.
Variable - integer.

Variables returned by the subroutine

Max - real.
Min - real.

Variable definitions

Average - a real variable equal to the average value obtained from the averaging subroutines.

Avg_type\$ - a string variable which indicates the type of averaging technique used to average the respiratory parameters.

Br_in_w_flag - an integer variable used as a Boolean value which indicates if breaths were found in the specified time window. This flag is used when performing window averaging.

Br_pntr - an integer variable used as a pointer into the breath dimension of the respiratory variable array. Br_pntr points to the first breath to be included in the average.

End_time - a real variable equal to the ending time of the

respiratory results display.

- Max** - a real variable equal to the maximum value of the respiratory parameter.
- Min** - a real variable equal to the minimum value of the respiratory parameter.
- No_b_avg** - an integer variable equal to the number of breaths to average when performing breath averaging.
- Num_bad_breaths** - an integer variable equal to the number of bad breaths that are found in a window of time when using the window averaging technique.
- Num_breaths** - a real variable equal to the number of breaths in the respiratory variable array.
- Start_time** - a real variable equal to the starting time of the respiratory results display.
- Time** - a real variable equal to the time that is midway between the first breath included in the average and the last breath included in the average. The Time variable is used only as a dummy parameter when calling the Avg_breath subroutine.
- Variable** - an integer variable which indicates which respiratory parameter is to be plotted.
- W_cntr** - a real variable equal to the time of the center of the window.
- W_width** - a real variable equal to the time width of the window.

A7.6.12 Plot values Subroutine

The Plot_values subroutine generates a plot of the respiratory parameter. The subroutine uses the specified averaging technique to determine the average of the respiratory parameter. The subroutine plots the values on the scale generated by the Make_axes subroutine.

Common blocks used by the subroutine

Common
Block

Variables in the
block

Anal_data8 - Resp_var

Plot_resp_data1 - Omit_bad, Num_breaths, No_b_avg

Plot_resp_data2 - Start_time, End_time, W_period, W_width

Variables passed to the subroutine

Avg_type\$ - string.

Variable - integer.

Variables returned by the subroutine

None

Variable definitions

Average - a real variable equal to the average value obtained from the averaging subroutines.

Avg_type\$ - a string variable which indicates the type of averaging technique used to average the respiratory parameters.

Br_in_w_flag - an integer variable used as a Boolean value which indicates if breaths were found in the specified time window. This flag is used when performing window averaging.

Br_pntr - an integer variable used as a pointer into the breath dimension of the respiratory variable array. Br_pntr points to the first breath to be included in the average.

End_time - a real variable equal to the ending time of the respiratory results display.

No_b_avg - an integer variable equal to the number of breaths to average when performing breath averaging.

Num_bad_breaths - an integer variable equal to the number of bad breaths that are found in a window of time when using the window averaging technique.

Num_breaths - a real variable equal to the number of breaths in the respiratory variable array.

Start_time - a real variable equal to the starting time of the respiratory results display.

Time - a real variable equal to the time that is midway between the first breath included in the average and the last breath included in the average. This value is used as the time value of the data point when using the breath averaging technique.

Variable - an integer variable which indicates which respiratory parameter is to be plotted.

W_cntr - a real variable equal to the time of the center of the

window.

W_period - a real variable equal to the period of which the window is slid.

A7.6.13 Print_values Subroutine

The Print_values subroutine generates a printout of all respiratory parameters. The subroutine uses the specified averaging technique to determine the average of the respiratory parameters.

Common blocks used by the subroutine

<u>Common Block</u>	<u>Variables in the block</u>
Anal_data3 -	Co2_prod, Insp_min_vent, O2_cons, Time_of_brth
Anal_data4 -	Expr_min_vent, Resp_freq, V_tid_expr, V_tid_insp
Anal_data5 -	Breath_good, Formfd\$, Resp_quotient
Anal_data5a -	Frc_co2_cons, Frc_o2_cons, Volume_of_lung
Anal_data6 -	Corr_flag, Room_fh2o, T
Anal_data8 -	Resp_var
Anal_data9 -	Comment\$, Name\$
Cal_data1 -	Cal\$, Date\$
Plot_resp_data1 -	Omit_bad, Num_breaths, No_b_avg
Plot_resp_data2 -	Start_time, End_time, W_period, W_width

Variables passed to the subroutine

Avg_type\$ - string.

Variables returned by the subroutine

None

Variable definitions

Average - a real variable equal to the average value obtained from the averaging subroutines.

Avg_type\$ - a string variable which indicates the type of averaging technique used to average the respiratory parameters.

Br_in_w_flag - an integer variable used as a Boolean value which indicates if breaths were found in the specified time window. This flag is used when performing window averaging.

Br_index - an integer variable which is set equal to the value of Br_pntr. Br_index is used when the Avg_window subroutine

is called so that the value of Br_ptr is not changed.

Br_ptr - an integer variable used as a pointer into the breath dimension of the respiratory variable array. Br_ptr points to the first breath to be included in the average.

Co2_prod - an integer used as a constant value which points to the computed rate of CO₂ production parameter in the respiratory variable array.

Comment\$ - a string variable containing an operator specified comment.

Corr_flag - an integer variable used as a Boolean value which indicates if the temperature corrections are used in computing the respiratory flow.

Date\$ - a string variable containing the date data were collected.

End_time - a real variable equal to the ending time of the respiratory results display.

Expr_min_vent - an integer used as a constant value which points to the computed expiratory minute ventilation parameter in the respiratory variable array.

Frc_co2_prod - an integer used as a constant value which points to the computed alveolar CO₂ production parameter in the respiratory variable array.

Frc_o2_cons - an integer used as a constant value which points to the computed alveolar O₂ consumption parameter in the respiratory variable array.

l - an integer variable used as a loop counter.

Insp_min_vent - an integer used as a constant value which points to the computed inspiratory minute ventilation parameter in the respiratory variable array.

Name\$ - a string variable containing the subject name.

No_b_avg - an integer variable equal to the number of breath to average when performing breath averaging.

Num_badBreaths - an integer variable equal to the number of bad breaths that are found in a window of time when using the window averaging technique.

NumBreaths - a real variable equal to the number of breaths in the respiratory variable array.

Omit_bad - an integer variable used as a Boolean flag which

indicates if the 'bad' breaths are not to be included in the average.

O2_cons - an integer used as a constant value which points to the computed rate of O₂ consumption parameter in the respiratory variable array.

Resp_freq - an integer used as a constant value which points to the computed respiratory frequency parameter in the respiratory variable array.

Resp_quotient - an integer used as a constant value which points to the computed respiratory quotient parameter in the respiratory variable array.

Some_rs_to_big - an integer variable used as a Boolean value which indicates that some values of the respiratory quotient average are too large to fit the print format.

Start_time - a real variable equal to the starting time of the respiratory results display.

Time - a real variable equal to the time that is midway between the first breath included in the average and the last breath included in the average.

Volume_of_lung - an integer used as a constant value which points to the computed lung volume parameter in the respiratory variable array.

V_tid_expr - an integer used as a constant value which points to the computed expiratory tidal volume parameter in the respiratory variable array.

V_tid_insp - an integer used as a constant value which points to the computed inspiratory tidal volume parameter in the respiratory variable array.

W_centr - a real variable equal to the time of the center of the window.

W_period - a real variable equal to the period of which the window is slid.

W_width - a real variable equal to the time width of the window.

A7.6.14 Rel_viscos Function

The Rel_viscos function calculates the viscosity of the flow gas relative to the viscosity of room air under STPD conditions. The concentrations of the flow gases and the flow gas temperature are used to determine the relative viscosity.

Common blocks used by the subroutine

None

Variables passed to the procedure

Fco2 - real.

Fh2o - real.

Fn2 - real.

Fo2 - real.

Temperature - real.

Variable definitions

Fh2o - a real variable equal to the fractional concentration of water vapor in the respiratory flow gas.

Fco2 - a real variable equal to the fractional concentration of CO₂ in the wet respiratory gas. This concentration value takes into account the amount of water vapor in the respiratory flow gas.

Fn2 - a real variable equal to the fractional concentration of N₂ in the wet respiratory gas. This concentration value takes into account the amount of water vapor in the respiratory flow gas.

Fo2 - a real variable equal to the fractional concentration of O₂ in the wet respiratory gas. This concentration value takes into account the amount of water vapor in the respiratory flow gas.

Rel_Viscosity - a real variable equal to the viscosity of the respiratory gas relative to the viscosity of room air under STPD conditions.

Temperature - a real variable equal to the temperature of the flow gas.

Vis_co2 - a real variable equal to the viscosity of pure CO₂ at the temperature of the flow gas.

Vis_h2o - a real variable equal to the viscosity of pure H₂O at the temperature of the flow gas.

Vis_n2 - a real variable equal to the viscosity of pure N₂ at the temperature of the flow gas.

Vis_o2 - a real variable equal to the viscosity of pure O₂ at the temperature of the flow gas.

A7.6.15 View Subroutine

The View subroutine defines the area of the plotting device that will contain a plot. View considers the plotting device to be an area of 100 by 100. The subroutine operates similar to the VIEWPORT command. However, using the View subroutine allows plotting areas to be defined independent of which axis is physically longer.

Common blocks used by the subroutine

None

Variables passed to the subroutine

Bottom - real.

Left - real.

Right - real.

Top - real.

Variables returned by the subroutine

None

Variable definitions

Bottom - a real variable defining the bottom of the plotting area on the 100 by 100 plotting device.

Left - a real variable defining the left side the plotting area on the 100 by 100 plotting device.

Right - a real variable defining the right side of the plotting area on the 100 by 100 plotting device.

Top - a real variable defining the top of the plotting area on the 100 by 100 plotting device.

A7.6.16 ANALYSIS Program Listing

```

5  | *****
10 | *****
15 |
20 | BREATH-BY-BREATH RESPIRATORY ANALYSIS/PLOTTING ROUTINE
25 |
30 | HP BASIC FILENAME: ANALYSIS
35 |
40 | Department of Electrical and Computer Engineering,
45 | Kansas State University
50 |
55 | REVISION      DATE      PROGRAMMER
60 | -----      -
65 | 1.0           JUNE 1, 1984    LOREN E. RIBLETT
70 | 2.0           January 1, 1985 Michael Masters
75 |
80 | *****
85 |
90 | PURPOSE
95 | THIS ROUTINE PERFORMS ALL ANALYSIS THAT IS CURRENTLY
100 | DONE ON THE RESPIRATORY DATA. RESULTS OF THIS ANALYSIS
105 | ARE PRESENTED IN BOTH TABULAR AND GRAPHICAL FORMS.
110 |
115 | *****
120 |
125 | NOTE 1: THIS ROUTINE ASSUMES THAT THE BINARY CALIBRATION FILES
130 | CREATED BY "CAPCRUNCH" ARE STORED ON THE HP9895A 8"
135 | FLEXIBLE DISK ":HP9895,700,0" (VOLUME #7 IN THE PASCAL
140 | OPERATING SYSTEM).
145 |
150 | NOTE 2: ANALYSIS ASSUMES THAT THE FOUR BINARY DATA FILES CREATED
155 | BY "DAPCRUNCH" ARE ALSO STORED ON THE HP9895A 8" FLEXIBLE
160 | DISK ":HP9895,700,0" (VOLUME #7 IN THE PASCAL OPERATING
165 | SYSTEM).
170 |
175 | NOTE 3: GAS MASS SPECTROMETER TIME DELAY VALUES CAN BE DETERMINED
180 | ON A BREATH-BY-BREATH BASIS OR A FIXED TIME DELAY CAN BE
185 | SELECTED FOR ANALYSIS OF THE ACQUIRED DATA. SHOULD AN
190 | EXTREME BREATH-BY-BREATH TIME BE CALCULATED, AN AVERAGE
195 | TIME DELAY IS SUBSTITUTED FOR THE COMPUTED TIME DELAY.
200 |
205 | NOTE 4: RESPIRATORY VOLUMES CAN BE CORRECTED TO STPD/BTPS CON-
210 | DITIONS PROVIDED THE BAROMETRIC PRESSURE (TORR), RELATIVE
215 | HUMIDITY (%), AND BODY TEMPERATURE (DEG C) IS SUPPLIED.
220 | USING THIS INFORMATION ALONG WITH POINT-BY-POINT TEMP-
225 | ERATURE CORRECTION (USING CHANNEL 4, THE RESPIRATORY
230 | TEMPERATURE CHANNEL), THE INSPIRATORY AND EXPIRATORY
235 | GAS VOLUMES ARE CORRECTED.
240 |
245 | NOTE 5: ANY WINDOW OF DATA FROM THE DAM DATA MAY BE PLOTTED
250 | EITHER ON THE HP9826 CRT OR HP9872C PLOTTER. ALL FOUR
255 | CHANNELS OF DATA ARE PLOTTED, THE CO2 AND O2 CHANNELS
260 | BEING PLOTTED WITH A TIME DELAY EQUAL TO THE AVERAGE
265 | TIME DELAY ENTERED BY THE USER. DATA PLOTTED ON THE
270 | HP9826 CRT MAY ALSO BE DUMPED TO THE HP2673A THERMAL
275 | PRINTER.
280 |
285 | NOTE 6: ONCE BREATH-BY-BREATH ANALYSIS OF THE DAM BEGINS,
290 | INFORMATION CONCERNING EACH BREATH IS PRINTED ON THE
295 | DECwriter PRINTER.
300 |
305 | NOTE 7: ONCE THE DATA ARRAYS ARE EXHAUSTED SUMMARY DATA FOR THE
310 | ENTIRE RUN IS COMPUTED AND PRINTED. FILE NAMES AS WELL

```



```

315 | AS CRITICAL CALIBRATION PARAMETERS ARE ALSO PRINTED.
320 | *****
325 |
330 | Analysis enhancements for version 2.0
335 |
340 | Note 1: The breath-by-breath results as analysis is proceeding
345 | may be omitted. The breath-by-breath variables may be
350 | plotted or printed post-analysis.
355 |
360 | Note 2: The respiratory flow may be corrected for variations in
365 | gas viscosity and temperature.
370 |
375 | Note 3: The breath-by-breath variables of interest may be
380 | displayed, printed or plotted, post-analysis. The
385 | individual breath values may be combined by one of two
390 | methods.
395 | (1) Breath Averaging. The individual breath values
400 | are averaged for a specified number of breaths
405 | (including averaging one breath).
410 | (2) Time Window averaging. The breaths occurring in
415 | a specified window are averaged.
420 |
425 | Note 4: The data arrays, calibration values are retained in a
430 | COMMON area of memory. This allows the data to stay
435 | resident in memory as various respiratory analysis pro-
440 | grams are executed. It is also a very useful tool during
445 | program debugging.
450 |
455 | Note 5: Many of the functional portions of the program have been
460 | transferred to true subroutines. This enhances the read-
465 | ability by building a structured format.
470 |
475 | *****
480 |
485 |
490 | Declare the common area of memory.
495 |
500 | The respiratory data
505 | COM /Resp_data1/ INTEGER Line1(1:24000),Line2(1:24000)
510 | COM /Resp_data2/ INTEGER Line3(1:24000),Line4(1:24000)
515 | COM /Resp_data3/ INTEGER Cmin,Cmax,Qmin,Qmax,Fmin,Fmax,Tmin,Tmax
520 | COM /Resp_data4/ INTEGER No_points
525 | COM /Resp_data5/ C1$(10),O2$(10),V$(10),T$(10)
530 |
535 | The calibration data
540 | COM /Cal_data1/ Cal$(10),Date$(25)
545 | COM /Cal_data2/ INTEGER Co2_dc_offset,O2_dc_offset,Bin_zero_flow,S
550 | COM /Cal_data3/ REAL Co2_cal,O2_cal
555 | COM /Cal_data4/ REAL Non_c_i_flowcal,Non_c_e_flowcal
560 | COM /Cal_data5/ REAL Corr_i_flowcal,Corr_e_flowcal
565 | COM /Cal_data6/ REAL Ta,Tb,Tc
570 | COM /Cal_data7/ REAL Time_delay,O1,Pb,Rel_humid,Room_temp
575 |
580 | The data used by the Analysis routines.
585 | COM /Anal_data1/ INTEGER Data_available
590 | COM /Anal_data2/ INTEGER True,False
595 | COM /Anal_data3/ INTEGER Time_of_brth,O2_cons,Co2_prod,Insp_min_vent
600 | COM /Anal_data4/ INTEGER Expr_min_vent,V_tid_insp,V_tid_expr,Resp_freq
605 | COM /Anal_data5/ INTEGER Breath_good,Resp_quotient,Formfd$(1)
610 | COM /Anal_data5a/ INTEGER Frc_o2_cons,Frc_co2_prod,Volume_of_lung
615 | COM /Anal_data6/ INTEGER Corr_flag,REAL Room_fh2o,T
620 | COM /Anal_data7/ Vap(0:250),Fh2o_sat(0:250)
625 | COM /Anal_data8/ Resp_var(0:12,1:500)
630 | COM /Anal_data9/ Name$(25),Comment$(46)
635 |

```

```

640 !*** SPECIAL FUNCTION KEY DECLARATION
645 !
650 Define_keys:
655   ON KEY 2 LABEL "ANALYSIS" GOSUB Anal_routine
660   ON KEY 9 LABEL "EXIT" GOTO Done
665   GOTO Define_keys
670 !
675 !*** SIGNAL END OF ROUTINE AND RETURN TO AUTOST
680 !
685 Done:OFF KEY
690   DISP "PROGRAM RUN COMPLETE"
695   MASS STORAGE IS ":INTERNAL"
700   LOAD "AUTOST",1
705 !
710 !
715 Anal_routine: !
720 !
725 !*** BEGINNING OF ANALYSIS SUBROUTINE
730   OFF KEY ! Turn the SOFT KEYS off.
735   INTEGER Good_insp_count,Good_exp_count,Insp_begin,Expr_begin
740   INTEGER A,Z,Breath_count,Final_insp
745   INTEGER Found,B_by_b_output ! Flags
750 !
755 !
760 !
765 !
770   True=(1=1) ! Corresponds to a logical True value.
775   False=(1=0) ! Logical False value.
780   Formfd$=CHR$(12) ! The ASCII character for a form feed.
785 !
790 !
795 !
800   Time_of_brth=0
805   O2_cons=Time_of_brth+1
810   Co2_prod=O2_cons+1
815   Frc_o2_cons=Co2_prod+1
820   Frc_co2_prod=Frc_o2_cons+1
825   Insp_min_vent=Frc_co2_prod+1
830   Expr_min_vent=Insp_min_vent+1
835   V_tid_insp=Expr_min_vent+1
840   V_tid_expr=V_tid_insp+1
845   Volume_of_lung=V_tid_expr+1
850   Resp_freq=Volume_of_lung+1
855   Resp_quotient=Resp_freq+1
860   Breath_good=Resp_quotient+1
865 !
870 !
875   BEEP
880   INPUT "ENTER THE SUBJECT'S NAME OR IDENTIFIER",Name$
885 !
890 !
895 !
900   IF Data_available THEN
905     PRINT Formfd$
910     PRINT "Data is resident in memory."
915     PRINT "      data file names      Max      Min"
920     PRINT "      CO2: "&C1$&"      "&VAL$(Cmax)&"      "&VAL$(Cmin)"
925     PRINT "      O2: "&O$&"      "&VAL$(Omax)&"      "&VAL$(Omin)"
930     PRINT "      FLOW: "&V$&"      "&VAL$(Fmax)&"      "&VAL$(Fmin)"
935     PRINT "      TEMP: "&T$&"      "&VAL$(Tmax)&"      "&VAL$(Tmin)"
940     PRINT "There are "&VAL$(No_points)&" data points"
945     PRINT "Calibration values"
950     IF Cal$="" THEN
955       PRINT "      No calibration data is resident in memory"
960     ELSE

```

```

965      PRINT "   The CALIBRATION file name is "&Cal$
970  END IF
975  PRINT "   Offsets:      CO2: ";Co2_dc_offset
980  PRINT "                  O2: ";O2_dc_offset
985  PRINT "   Binary zero flow: ";Bin_zero_flow
990  PRINT "   CO2 cal: ";Co2_cal;"      O2 cal: ";O2_cal
995  PRINT "   Non Corrected flow cal$"
1000 PRINT "      Insp. ";Non_c_i_flowcal;"      Expr. ";Non_c_e_flowcal
1005 PRINT "   Corrected flow cal$"
1010 PRINT "      Insp. ";Corr_i_flowcal;"      Expr. ";Corr_e_flowcal
1015 !
1020 !
1025 !      See if the user wishes to keep the present
1030      QS="N"      calibration data. If not, enter the new data.
1035  BEEP      !Set the default to No (get new data)
1040  INPUT "DO YOU WISH TO USE THESE CALIBRATION DATA? (Y/N)",QS
1045  IF QS="N" OR QS="n" THEN
1050      GOSUB Rtc1
1055  PRINT "New cal data loaded. B_by_B data is the same"
1060  END IF
1065 !
1070 !
1075 !      See if the user wishes to keep the present
1080      QS="N"      respiratory data. If not, enter the new data.
1085  BEEP      !Set the default to No (get new data)
1090  INPUT "DO YOU WISH TO USE THESE B_by_B DATA? (Y/N)",QS
1095  IF QS="N" OR QS="n" THEN
1100      BEEP
1105  INPUT "ENTER THE TOTAL NUMBER OF POINTS TO BE ANALYZED",No_points
1110  GOSUB Rtd1
1115  END IF
1120  PRINT Formfd$      !Clear the screen
1125 !
1130 ELSE
1135      ! No data is resident. Read in the data.
1140 !
1145 !      *** LOAD BINARY CALIBRATION FILE IF REQUESTED
1150  BEEP
1155  QS="N"      ! Set the default to No.
1160  INPUT "LOAD CALIBRATION FACTORS FROM DISK ? (Y/N)",QS
1165  IF QS="Y" OR QS="y" THEN GOSUB Rtc1
1170  BEEP
1175  INPUT "ENTER THE TOTAL NUMBER OF POINTS TO BE ANALYZED",No_points
1180 !
1185 !      *** LOAD FOUR CHANNELS OF BINARY DATA
1190  GOSUB Rtd1
1195  Data_available=True      ! Set the data resident in memory flag.
1200  END IF
1205  BEEP
1210 !
1215 !      Set experimental time which data collection began.
1220  INPUT "Enter the beginning time of data collection. (sec)",Begtime_colct
1225 !
1230 Analyze: !
1235 !      Enter a comment to be printed on the hard copy output.
1240  BEEP
1245  INPUT "ENTER A COMNT TO BE PRINTED ON THE HRD CPY OUTPUT.",Comments$
1250 !      *** CHOOSE APPROPRIATE SAMPLING FREQUENCY
1255  S=50
1260  QS="N"      ! Set the default to No.
1265  BEEP
1270  INPUT "CHANGE SAMPLING FREQUENCY FROM 50 HZ.? (Y/N)",QS
1275  IF QS="Y" OR QS="y" THEN
1280      INPUT "ENTER DESIRED SAMPLING FREQUENCY (HZ.)",S
1285  END IF

```

```

1290 QS=""
1295 !
1300 !*** CHOOSE B-BY-B TIME DELAYS OR A FIXED GMS TIME DELAY
1305 !
1310 BEEP
1315 QS="F" !Set the default to fixed.
1320 INPUT "B-BY-B TIME DELAY OR FIXED TIME DELAY (B/F) ?",QS
1325 IF QS="B" OR QS="b" THEN
1330 !
1335 !*** FOR B-BY-B DELAYS, CHOOSE STARTING VALUE FOR AVERAGE DELAY
1340 !
1345 BEEP
1350 INPUT "AVERAGE TIME DELAY FOR BAD BREATH PROBLEMS (msec)?",Time_delay_sum
1355 Avg_time_delay=Time_delay_sum
1360 Time_delay_flag=1 !Time_delay_flag=1 FOR B-BY-B TIME DELAYS
1365 ELSE
1370 !
1375 !*** FOR FIXED TIME DELAY, ENTER DESIRED TIME DELAY
1380 !
1385 Time_delay_flag=0 !Time_delay_flag=0 FOR FIXED TIME DELAYS
1390 PRINT "CURRENT TIME DELAY IS ";Time_delay;" msec"
1395 QS=""
1400 BEEP
1405 INPUT "CHANGE TIME DELAY? (Y/N)",QS
1410 IF QS="Y" OR QS="y" THEN
1415 INPUT "ENTER DESIRED TIME DELAY (msec.)",Time_delay
1420 END IF
1425 END IF
1430 !
1435 ! See if viscosity and temperature corrections are desired.
1440 BEEP
1445 QS=""
1450 INPUT "USE TEMP. AND VISCOSITY CORRECTIONS? (Y/N)",QS
1455 IF QS="Y" OR QS="y" THEN
1460 !
1465 !*** IF STPD/BTPS DESIRED, LOAD IN WATER VAPOR PRESSURE TABLE
1470 ! Bypass if the vapor pressures are already present.
1475 IF Vap(0)=0 THEN
1480 DISP "READING WATER VAPOR PRESSURES"
1485 ASSIGN @Vap_path TO "VAP_BASIC:HP9895,702,3"
1490 ON END @Vap_path GOTO 1520
1495 ENTER @Vap_path;Vap(*)
1500 ASSIGN @Vap_path TO *
1505 END IF
1510 Corr_flag=True ! Set the temperatur/viscosity correction flag.
1515 IF Body_temp=0 THEN Body_temp=(98.6-32)*5/9
1520 Body_temp=Body_temp*9/5+32 ! Convert body temp to deg F.
1525 BEEP
1530 INPUT "ENTER THE BODY TEMPERATURE (deg F)",Body_temp
1535 Body_temp=(Body_temp-32)*5/9 ! Convert body temp to deg C.
1540 ! Display the ambient conditions.
1545 IF Room_temp=0 THEN Room_temp=(70-32)*5/9
1550 PRINT Formfd$,TABXY(1,15);" Barometric pressure = ";Pb/25.4
1555 PRINT " Relative humidity = ";Rel_humid*100
1560 PRINT USING "K,DDD.DD";" Room temperature = ";Room_temp*9/5+32
1565 BEEP
1570 QS="N"
1575 INPUT "Do you wish to use the ambient cond. above? (Y/N)",QS
1580 IF NOT (QS="y" OR QS="Y") THEN
1585 Pb=Pb/25.4 ! Convert to inches Hg.
1590 BEEP
1595 INPUT "Enter the new barometric pressure. (inches)",Pb
1600 Pb=Pb*25.4 ! Convert to torr.
1605 Rel_humid=Rel_humid*100

```

```

1610      BEEP
1615      INPUT "Enter the new percent relative humidity",Rel_humid
1620      Rel_humid=Rel_humid/100
1625      Room_temp=Room_temp*9/5+32      ! Convert to deg F
1630      BEEP
1635      INPUT "Enter the new room temperature",Room_temp
1640      Room_temp=(Room_temp-32)*5/9      ! Convert to deg C.
1645      END IF
1650      PRINT Formfd$
1655      !
1660      !           Generate the Fractional water vapor concentration of the
1665      !           saturated gas.
1670      FOR I=0 TO 250
1675          Fh2o_sat(I)=Vap(I)/Pb
1680      NEXT I
1685      !
1690      !
1695      !           Get the water fraction under room conditions and the vapor
1700      !           pressure at body temperature, calculate STPD to BTPS
1705      !           conversion factor and use the temperature corrected flow
1710      !           calibration factors.
1715      Room_fh2o=Rel_humid*Fh2o_sat((Room_temp-20)*10)
1720      Ph2o_body=Vap((Body_temp-20)*10)
1725      Stpd_to_btps=(273.15+Body_temp)/273.15*760/(Pb-Ph2o_body)
1730      Btps_to_stpd=1/Stpd_to_btps
1735      Insp_flowcal=Corr_i_flowcal
1740      Expr_flowcal=Corr_e_flowcal
1745      ELSE
1750      !           Set the correction flag to False. Set conversion factors
1755      !           to unity. Set the flow calibration factors equal to the
1760      !           non-corrected calibration factors.
1765      Corr_flag=False
1770      Stpd_to_btps=1
1775      Btps_to_stpd=1
1780      Insp_flowcal=Non_c_i_flowcal
1785      Expr_flowcal=Non_c_e_flowcal
1790      END IF
1795      PRINT Formfd$      ! Clear the screen.
1800      !
1805      ! See if FRC calculations are desired. (FRC calculations have not been
1810      ! fine tuned in this program. See Rick Pieschl.)
1815      BEEP
1820      QS=""
1825      INPUT "Do you wish to use FRC corrections? (Y/N)",QS
1830      IF QS="Y" OR QS="y" THEN
1835          Frc_flag=True
1840          IF NOT (Corr_flag) THEN      !Body temp. and Pb has not been entered.
1845              BEEP
1850              INPUT "Enter the body temperature (deg F)",Body_temp
1855              Body_temp=(Body_temp-32)*5/9
1860              Ph2o_body=Vap((Body_temp-20)*10)
1865              BEEP
1870              INPUT "Enter the barometric pressure(inches)",Pb
1875              Pb=Pb*25.4
1880          END IF
1885          Frac_h2o_body=Ph2o_body/Pb
1890      ELSE
1895          Frc_flag=False
1900      END IF
1905      !
1910      !*** SEE IF PLOT OF DATA IS DESIRED
1915      !
1920      QS="N"
1925      BEEP
1930      INPUT "WOULD YOU LIKE A PLOT OF THE DATA?(Y/N)",QS

```

```

1935 !
1940 !*** IF SO, GO PLOT THE DATA
1945 !
1950 IF QS="Y" OR QS="y" THEN GOSUB DtploT
1955 !
1960 !
1965 !           Get the first and last data points to be analyzed.
1970 BEEP
1975 INPUT "ENTER STARTING POINT TO ANALYZE.",Start
1980 IF Start>No_points-50 THEN GOTO 1970
1985 A=Start+1
1990 Z=Start+1
1995 BEEP
2000 INPUT "ENTER ENDING POINT TO ANALYZE.",End
2005 IF End>No_points OR End<Start THEN GOTO 1995
2010 !
2015 !           See if the breath-by-breath values are to be printed during
2020 !           analysis.
2025 PRINT TABXY(1,18);"Do you wish to omit the breath by breath output of"
2030 PRINT "the results as the data is being analyzed? (Y/N)"
2035 QS="N"
2040 BEEP
2045 INPUT QS
2050 PRINT Formfd$
2055 IF QS="N" OR QS="n" THEN
2060     B_by_b_output=True
2065 ELSE
2070     B_by_b_output=False
2075 END IF
2080 !
2085 !           *** INITIALIZE NECESSARY ANALYSIS PARAM.
2090 IF OI=0 THEN OI=.11
2095 T=1/S
2100 Num_breaths=0
2105 Good_insp_count=0
2110 Good_exp_count=0
2115 Time_delay_cnt=1
2120 Tot_vol_insp=0
2125 Tot_vol_exp=0
2130 Tot_o2_insp=0
2135 Tot_co2_insp=0
2140 Tot_o2_exp=0
2145 Tot_co2_exp=0
2150 Tot_o2_cons=0
2155 Tot_co2_prod=0
2160 Tot_time_insp=0
2165 Tot_time_expr=0
2170 Lung_vol=.4
2175 Net_lung_chng=0
2180 !
2185 !           *** LOCATE FIRST INSPIRATION IN FLOW SIGNAL
2190 !           *** The first breath begins at point A when the (A-1)'th point
2195 !           is an expiratory flow and the A'th point is an inspiration.
2200 REPEAT
2205     IF Line3(A-1)-Bin_zero_flow>0 AND FNInspiration((A)) THEN
2210         Found=True
2215     ELSE
2220         Found=False
2225         A=A+1
2230     END IF
2235 UNTIL Found
2240 Init_index=A
2245 !
2250 !
2255 !           *** GO PRINT DATA TABLE HEADER ON PRINTER LISTING

```



```

2260 GOSUB Hard_copy_head
2265 Breath_count=0
2270 Still_calc=True
2275 !
2280 !
2285 !*****
2290 !           Compute the breath by breath values. Repeat the
2295 !           computations until the stopping point has been
2300 !           reached.
2305 REPEAT
2310     DISP "Calc. the results of breath starting at",A
2315     Insp_count=A
2320     Breath_count=Breath_count+1
2325     Resp_var(Time_of_brth,Breath_count)=A*T+Begtime_colct
2330 !
2335 !           Determine the GMS time delay.
2340     IF Time_delay_flag<>0 THEN ! Use the B-by-B time delay.
2345       GOSUB Bbb_time_delay
2350 !
2355 !           IF B-BY-B TIME DELAY OUTSIDE LIMITS, SUBSTITUTE AVERAGE DELAY
2360     IF (Time_delay>560) OR (Time_delay<330) THEN
2365 !
2370 !           *** The time delay was bad. ***
2375       Time_delay=Avg_time_delay
2380       Time_delay_flag=2
2385     ELSE
2390 !
2395 !           *** The time delay was good so update the running average
2400       Time_delay_flag=1
2405       Time_delay_sum=Time_delay_sum+Time_delay
2410       Time_delay_cnt=Time_delay_cnt+1
2415       Avg_time_delay=Time_delay_sum/Time_delay_cnt
2420     END IF
2425   END IF
2430 !
2435 !           *** ADJUST CO2 AND O2 INDEX (Z) FOR PROPER POINT SELECTION
2440   Z=A+INT(Time_delay/1000*S+.5)
2445 !
2450 !           *** COMPUTE HALF THE AREA FOR THE FIRST TRAPEZOID
2455   Calc_sig_val((A),(Z),("INSP"),Incr_vol,Fo2,Fco2)
2460   Air_insp=.5*Incr_vol
2465   Co2_insp=.5*Fco2*Incr_vol
2470   O2_insp=.5*Fo2*Incr_vol
2475 !
2480 !           *** Sum up the inspiratory volumes.
2485   A=A+1
2490   Z=Z+1
2495   REPEAT
2500     IF Z>End-50 THEN ! Exit if to close to the end.
2505       Still_calc=False
2510       GOTO Done_calc
2515     END IF
2520 !
2525     Calc_sig_val((A),(Z),("INSP"),Incr_vol,Fo2,Fco2)
2530     Air_insp=Air_insp+Incr_vol
2535     Co2_insp=Co2_insp+Fco2*Incr_vol
2540     O2_insp=O2_insp+Fo2*Incr_vol
2545 !
2550     A=A+1
2555     Z=Z+1
2560 !           *** LOOP UNTIL END OF INSPIRATION
2565   UNTIL NOT (FNInspiration(A))
2570   Insp_time=(A-Insp_count)*T !Time of inspiration in seconds
2575 !
2580 !           *** PUT 1/2 OF THE LAST TRAPEZOIDAL AREA CORRESPONDING TO THE

```

```

2585 !      INSPIRATORY/EXPIRATORY TRANSITION ON THE INSPIRATION AND 1/2
2590 !      OF THE AREA ON THE EXPIRATION
2595 Calc_sig_val((A),(Z),("INSP"),Incr_vol,Fo2,Fco2)
2600 Air_insp=Air_insp+.5*Incr_vol
2605 Co2_insp=Co2_insp+.5*Fco2*Incr_vol
2610 O2_insp=O2_insp+.5*Fo2*Incr_vol
2615 !
2620 Calc_sig_val((A),(Z),("EXPR"),Incr_vol,Fo2,Fco2)
2625 Air_expr=.5*Incr_vol
2630 Co2_expr=.5*Fco2*Incr_vol
2635 O2_expr=.5*Fo2*Incr_vol
2640 Expr_begin=A
2645 !
2650 !
2655 !      Determine the expiratory tidal volume and expired CO2 and
2660 !      O2 volumes.
2665 !
2670 A=A+1
2675 Z=Z+1
2680 REPEAT
2685 IF Z>End-50 THEN          ! Exit if to close to the end.
2690     Still_calc=False
2695     GOTO Done_calc
2700 END IF
2705 !
2710 Calc_sig_val((A),(Z),("EXPR"),Incr_vol,Fo2,Fco2)
2715 Air_expr=Air_expr+Incr_vol
2720 Co2_expr=Co2_expr+Fco2*Incr_vol
2725 O2_expr=O2_expr+Fo2*Incr_vol
2730 !
2735 A=A+1
2740 Z=Z+1
2745 !      *** LOOP UNTIL END OF EXPIRATION
2750 UNTIL NOT (FNEExpiration(A))
2755 !
2760 !
2765 !      *** INCLUDE HALF OF THE TRAPEZOIDAL AREA CORRESPONDING TO THE
2770 !      EXPIRATORY/INSPIRATORY TRANSITION.
2775 !
2780 Calc_sig_val((A),(Z),("EXPR"),Incr_vol,Fo2,Fco2)
2785 Air_expr=Air_expr+.5*Incr_vol
2790 Co2_expr=Co2_expr+.5*Fco2*Incr_vol
2795 O2_expr=O2_expr+.5*Fo2*Incr_vol
2800 !
2805 !      *****
2810 !      *** BEGIN CALCULATIONS FOR THIS PARTICULAR BREATH ***
2815 !
2820 !      INSPIRATORY VOLUME FOR THIS BREATH (LITERS)
2825 Air_insp=Air_insp*Insp_flowcal*Stpd_to_btps
2830 !
2835 Co2_insp=Co2_insp*Insp_flowcal      !CO2 INSPIRED FOR THIS BREATH (L)
2840 O2_insp=O2_insp*Insp_flowcal      !O2 INSPIRED FOR THIS BREATH (L)
2845 !
2850 !      EXPIRATORY VOLUME FOR THIS BREATH (LITERS)
2855 Air_expr=Air_expr*Expr_flowcal*Stpd_to_btps
2860 !
2865 Co2_expr=Co2_expr*Expr_flowcal      !CO2 EXPIRED FOR THIS BREATH (L)
2870 O2_expr=O2_expr*Expr_flowcal      !O2 EXPIRED FOR THIS BREATH (L)
2875 O2cons=O2_insp+O2_expr              !CONSUMED O2 FOR THIS BREATH (L)
2880 Co2prod=Co2_insp+Co2_expr            !CO2 PRODUCED FOR THIS BREATH (L)
2885 Num_breaths=Num_breaths+1          !TOTAL NUMBER OF BREATHS ANALYZED
2890 !
2895 !
2900 !
2905 !      Start FRC corrections. These corrections are not
      implemented in version 2.0. See Rick Pieschl.

```



```

2910 IF Frc_flag=True THEN
2915 ! *** COMPUTE THE END EXPIRATE VALUES AND THEN COMPUTE
2920 ! THE ALVEOLAR VALUES, THE CHANGE IN LUNG VOLUME,
2925 ! AND THE LUNG VOLUME.
2930 Max_pnt=FNMax_co2_pnt(Line1(*),A)
2935 ! Compute the dry aveolar gas concentrations and then convert them
2940 ! to wet values.
2945 Frac_co2_1=(Line1(Max_pnt)-Co2_dc_offset)*Co2_cal
2950 Frac_o2_1=(Line2(Max_pnt)-O2_dc_offset)*O2_cal+O1
2955 Frac_co2_1=Frac_co2_1*(1-Frac_h2o_body)
2960 Frac_o2_1=Frac_o2_1*(1-Frac_h2o_body)
2965 IF NumBreaths>1 THEN
2970 Chng_fo2=Frac_o2_1-Frac_o2_2
2975 Chng_fco2=Frac_co2_1-Frac_co2_2
2980 !
2985 ! Compute the change in lung volume.
2990 Chng_lung_vol=-Air_insp/(1-Frac_h2o_body)-Air_expr+(O2cons+Co2
prod)*Stpd_to_btps
2995 Chng_lung_vol=Chng_lung_vol+Lung_vol*(Chng_fo2+Chng_fco2)
3000 Chng_lung_vol=Chng_lung_vol/(1-Frac_o2_1-Frac_co2_1)
3005 !
3010 Frc_o2cons=O2cons+(Chng_lung_vol*Frac_o2_1+Chng_fo2*Lung_vol)*
Btps_to_stpd
3015 Frc_co2prod=Co2prod+(Chng_lung_vol*Frac_co2_1+Chng_fco2*Lung_v
ol)*Btps_to_stpd
3020 Lung_vol=Lung_vol+Chng_lung_vol
3025 END IF
3030 Frac_o2_2=Frac_o2_1
3035 Frac_co2_2=Frac_co2_1
3040 ELSE
3045 Frc_o2cons=O2cons
3050 Frc_co2prod=Co2prod
3055 END IF
3060 !
3065 !
3070 Expr_time=(A-Expr_begin)*T !TIME FOR CURRENT EXPIRATION (SECONDS)
3075 Final_index=A
3080 Final_insp=Insp_count
3085 Tot_time=(Expr_time+Insp_time)/60
3090 !
3095 ! Compute and store the breath-by-breath values
3100 ! for this breath.
3105 Resp_var(O2_cons,Breath_count)=-O2cons/Tot_time
3110 Resp_var(Co2_prod,Breath_count)=Co2prod/Tot_time
3115 Resp_var(Insp_minVent,Breath_count)=-Air_insp/Tot_time
3120 Resp_var(Expr_minVent,Breath_count)=Air_expr/Tot_time
3125 Resp_var(Vtid_insp,Breath_count)=-Air_insp
3130 Resp_var(Vtid_expr,Breath_count)=Air_expr
3135 Resp_var(Resp_freq,Breath_count)=1/(Insp_time+Expr_time)*60
3140 Resp_var(Resp_quotient,Breath_count)=ABS(Co2prod/O2cons)
3145 Resp_var(Frc_o2_cons,Breath_count)=-Frc_o2cons/Tot_time
3150 Resp_var(Frc_co2_prod,Breath_count)=Frc_co2prod/Tot_time
3155 Resp_var(Volume_of_lung,Breath_count)=Lung_vol
3160 !
3165 IF B_by_b_output THEN
3170 !
3175 ! *** GO PRINT CALCULATED VALUES FOR THIS BREATH
3180 GOSUB Hard_output
3185 END IF
3190 !
3195 ! *** KEEP TRACK OF GOOD INSPIRATIONS AND EXPIRATIONS
3200 IF ABS(Air_insp)>.4 AND ABS(Air_expr)>.4 THEN
3205 Resp_var(Breath_good,Breath_count)=True
3210 ELSE
3215 Resp_var(Breath_good,Breath_count)=False

```

```

3220 END IF
3225 !
3230 IF ABS(Air_insp)>.4 THEN
3235 Good_insp_count=Good_insp_count+1
3240 END IF
3245 IF ABS(Air_expr)>.4 THEN
3250 Good_exp_count=Good_exp_count+1
3255 END IF
3260 !
3265 ! *** ADJUST RUNNING TOTAL VALUES FOR ENTIRE TRIAL
3270 Tot_vol_insp=Tot_vol_insp+Air_insp
3275 Tot_vol_exp=Tot_vol_exp+Air_expr
3280 Tot_o2_insp=Tot_o2_insp+O2_insp
3285 Tot_o2_exp=Tot_o2_exp+O2_expr
3290 Tot_co2_insp=Tot_co2_insp+Co2_insp
3295 Tot_co2_exp=Tot_co2_exp+Co2_expr
3300 Tot_o2_cons=Tot_o2_cons+O2cons
3305 Tot_co2_prod=Tot_co2_prod+Co2prod
3310 Tot_time_insp=Tot_time_insp+Insp_time
3315 Tot_time_expr=Tot_time_expr+Expr_time
3320 !
3325 R=-Tot_co2_prod/Tot_o2_cons
3330 Done_calc: ! Keep repeating until the end has been reached.
3335 UNTIL Still_calc=False
3340 Breath_count=Breath_count-1
3345 DISP
3350 !
3355 !*****
3360 !
3365 ! COMPUTE FINAL TRIAL AVERAGES
3370 !
3375 Tot_time_resp=(Final_index-Init_index)*T !TOTAL RESPIRATORY TIME (SEC)
3380 Minvol=Tot_vol_insp*60/Tot_time_resp !INSP. MINUTE VOLUME (L/MIN)
3385 Minvole=Tot_vol_exp*60/Tot_time_resp !EXP. MINUTE VOLUME (L/MIN)
3390 Num_breaths=(Good_insp_count+Good_exp_count)/2
3395 Avg_air_insp=Tot_vol_insp/Num_breaths !AVERAGE INSPIRATORY VOLUME (L)
3400 Avg_air_expr=Tot_vol_exp/Num_breaths !AVERAGE EXPIRATORY VOLUME (L)
3405 Resp_f=Num_breaths*60/Tot_time_resp !RESP. FREQUENCY (BREATHS/MIN)
3410 Avg_o2_insp=Tot_o2_insp/Num_breaths !AVERAGE INSPIRED O2/BREATH (L)
3415 Avg_o2_expr=Tot_o2_exp/Num_breaths !AVERAGE EXPIRED O2/BREATH (L)
3420 Avg_co2_insp=Tot_co2_insp/Num_breaths !AVERAGE INSPIRED CO2/BREATH (L)
3425 Avg_co2_expr=Tot_co2_exp/Num_breaths !AVERAGE EXPIRED CO2/BREATH (L)
3430 Avo2cons=Tot_o2_cons/Num_breaths !AVERAGE O2 CONSUMED/BREATH (L)
3435 Avco2prod=Tot_co2_prod/Num_breaths
3440 V_dot_o2=Tot_o2_cons/Tot_time_resp*60
3445 V_dot_co2=Tot_co2_prod/Tot_time_resp*60
3450 R=ABS(V_dot_co2/V_dot_o2)
3455 !
3460 ! *** GO PRINT MEAN VALUES
3465 !
3470 PRINTER IS 9
3475 GOSUB Means
3480 PRINTER IS 1
3485 !
3490 Q$=""
3495 BEEP
3500 INPUT "DISPLAY THE BREATH-BY-BREATH DATA? (Y/N)",Q$
3505 IF Q$="Y" OR Q$="y" THEN
3510 CALL Disp_results(Breath_count,Corr_flag)
3515 END IF
3520 !
3525 BEEP
3530 Q$=""
3535 INPUT "REDO ANALYSIS? (Y/N)",Q$
3540 IF Q$="Y" OR Q$="y" THEN GOTO Analyze

```

```

3545 !
3550 !*** END OF ANALYSIS ROUTINE
3555 !
3560 RETURN ! Exit the Analysis portion.
3565 !
3570 !*** SUBROUTINE TO PRINT STANDARD HEADER TO THE DECwriter II PRINTER
3575 !
3580 Hard_copy_head:PRINTER IS 9
3585 AS="Air"
3590 BS="O2"
3595 CS="CO2"
3600 DS="Inspired"
3605 ES="Expired"
3610 FS="(liters)"
3615 GS="BTPS"
3620 HS="STPD"
3625 PRINT USING "2/,K";"SUBJECT IDENTIFIER: "&Name$
3630 PRINT USING "2/,K";"DATE: "&Date$
3635 PRINT USING "/,K,2/";"COMMENT: "&Comment$
3640 IF B_by_b_output THEN
3645 PRINT USING "#,2X,K,5X,K,7X,K,8X,K,8X,K,7X,K";"Breath";AS;AS;BS;BS;C
$
3650 PRINT USING "#,7X,K,8X,K,7X,K,7X,K,6X,K,5X,K";CS;BS;CS;"Insp";"Expr".
; "Delay"
3655 PRINT
3660 PRINT USING "#,2X,K,4X,K,2X,K,3X,K,2X,K";"Start";DS;ES;DS;ES
3665 PRINT USING "#,3X,K,2X,K,3X,K,2X,K";DS;ES;"Consumed";"Produced"
3670 PRINT USING "#,4X,K,6X,K,6X,K";"TIME";"TIME";"TIME"
3675 PRINT
3680 PRINT USING "#,2X,K,4X,K,2X,K,2X,K,2X,K,2X,K";"Index";FS;FS;FS;FS;FS
3685 PRINT USING "#,2X,K,2X,K,2X,K,3X,K,5X,K,5X,K";FS;FS;FS;"(sec)";"(sec
)" ; "(msec)"
3690 PRINT
3695 IF Corr_flag THEN
3700 PRINT USING "#,13X,K,6X,K,6X,K,6X,K,6X,K";GS;GS;HS;HS;HS
3705 PRINT USING "#,6X,K,6X,K,6X,K";HS;HS;HS
3710 PRINT
3715 END IF
3720 PRINT USING "120( ""-"" )"
3725 END IF
3730 PRINTER IS 1
3735 RETURN
3740 !
3745 !*** SUBROUTINE TO PRINT A SINGLE LINE OF BREATH-BY-BREATH INFORMATION
3750 !
3755 Hard_output: !
3760 PRINTER IS 9
3765 !PRINT USING "#,70X,K,18X,K";"|" ; "|"
3770 PRINT
3775 PRINT USING "#,2X,DDDD";Insp_count
3780 PRINT USING "#,5X,DD.DDD,3(4X,DD.DDD)";Air_insp;Air_expr;O2_insp;O2_expr
3785 PRINT USING "#,4X,D.DDD,5X,D.DDD,3X,K,1X,D.DDD";Co2_insp;Co2_expr;"I";O
2cons
3790 PRINT USING "#,5X,D.DDD,2X,K";Co2prod;"I"
3795 PRINT USING "#,3X,D.DD,6X,D.DD";Insp_time;Expr_time
3800 IF Time_delay_flag<>2 THEN PRINT USING "#,6X,DDD";Time_delay
3805 IF Time_delay_flag=2 THEN PRINT USING "#,4X,K,DDD,K";"";"Time_delay;""
*
3810 PRINT
3815 PRINTER IS 1
3820 RETURN
3825 !
3830 !*** SUBROUTINE TO PRINT TRIAL AVERAGE VALUE INFORMATION
3835 !
3840 Means: !

```

```

3845 PRINT
3850 PRINT
3855 PRINT "      Summary data and average values"
3860 PRINT
3865 PRINT "                        Data Point   Time (sec)"
3870 An_pnts: IMAGE K, 5D, K, 3D, DD
3875 Temporary=(Start-1)*T+Begtime_colct
3880 PRINT USING An_pnts; "Beginning analysis point: ", Start, "      ", Temp
orary
3885 Temporary=(Init_index-1)*T+Begtime_colct
3890 PRINT USING An_pnts; "The first inspiration:      ", Init_index, "      "
, Temporary
3895 Temporary=(Final_insp-1)*T+Begtime_colct
3900 PRINT USING An_pnts; "The last inspiration:      ", Final_insp, "      "
, Temporary
3905 Temporary=(End-1)*T+Begtime_colct
3910 PRINT USING An_pnts; "Ending analysis point:      ", End, "      ", Tempor
ary
3915 PRINT
3920 PRINT
3925 IF NOT (Corr_flag) THEN
3930   HS=""
3935   GS=""
3940 END IF
3945 PRINT USING "2/, #, K, 4D, D"; "Inspiratory minute volume = "; Minvoli
3950 PRINT USING "K, 4A"; " liters per minute ", GS
3955 PRINT USING "/", #, K, 3D, D; "Expiratory minute volume = "; Minvole
3960 PRINT USING "K, 4A"; " liters per minute ", GS
3965 PRINT USING "/", #, K, 3D, 3D; "O2 consumed per minute = "; V_dot_o2
3970 PRINT USING "K, 4A"; " liters per minute ", HS
3975 PRINT USING "/", #, K, 3D, 3D; "CO2 produced per minute = "; V_dot_co2
3980 PRINT USING "K, 4A"; " liters per minute ", HS
3985 PRINT USING "/", K, DDD, 3D; "RESPIRATORY QUOTIENT = "; R
3990 PRINT USING "2/, K, DDD, 4D, K, 4A"; "Inspiratory tidal volume = "; Avg_air_in
sp; " liters ", GS
3995 PRINT USING "/", K, DDD, 4D, K, 4A; "Expiratory tidal volume = "; Avg_air_expr
; " liters ", GS
4000 PRINT USING "/", K, DDDD, D, K; "Respiratory frequency = "; Respf; " breaths p
er minute"
4005 PRINT USING "/", K, DDD, 3D, K, 4A; "Mean O2 inspired = "; Avg_o2_insp; " liter
s ", HS
4010 PRINT USING "/", K, DDD, 3D, K, 4A; "Mean O2 expired = "; Avg_o2_expr; " liters
", HS
4015 PRINT USING "/", K, DDD, 3D, K, 4A; "Mean CO2 inspired = "; Avg_co2_insp; " lit
ers ", HS
4020 PRINT USING "/", K, DDD, 3D, K, 4A; "Mean CO2 expired = "; Avg_co2_expr; " lite
rs ", HS
4025 PRINT USING "/", K, DDD, 3D, K, 4A; "Mean O2 consumed per breath = "; Avco2cons
; " liters ", HS
4030 PRINT USING "/", K, DDD, 3D, K, 4A; "Mean CO2 produced per breath = "; Avco2pro
d; " liters ", HS
4035 PRINT USING "/", K, 3D, D, K; "Total time of inspiration = "; Tot_time_insp; "
sec"
4040 PRINT USING "/", K, 3D, D, K; "Total time of expiration = "; Tot_time_expr; "
sec"
4045 PRINT USING "/", K, 3D, D, K; "Total time of respiration = "; Tot_time_resp; "
sec"
4050 PRINT USING "/", K, 3D, D; "Number of good inspirations = "; Good_insp_count
4055 PRINT USING "/", K, 3D, D; "Number of good expirations = "; Good_exp_count
4060 PRINT USING "/", K, 3D, D; "Number of good breaths = "; Num_breaths
4065 PRINT USING "3/"
4070 PRINT "      Calibration data and File names"
4075 IF Corr_flag THEN
4080   PRINT USING "2/, #, K"; "The flow signal was incrementally corrected "
4085   PRINT "for changes in gas"

```

```

4090 PRINT "temperature and viscosity."
4095 PRINT USING "/,K,DD,D,K";"Relative Humidity = ";Rel_humid*100;"%"
4100 PRINT USING "/,K,DD,DD,K";"Body Temperature = ";Body_temp;" deg C"
4105 PRINT USING "/,K,DD,DD,K,DD,3D,K";"PH2O at ";Body_temp;" deg C = ";P
h2o_body;" torr"
4110 PRINT USING "/,K,3D,DD,K";"Barometric Pressure = ";Pb;" torr"
4115 PRINT USING "/,K,3D,DD,K";"Room temperature = ";Room_temp;" deg C"
4120 END IF
4125 PRINT USING "/,K,4D";"FLOW DC OFFSET = ";Bin_zero_flow
4130 PRINT USING "/,K,4D";"CO2 DC OFFSET = ";Co2_dc_offset
4135 PRINT USING "/,K,4D";"O2 DC OFFSET = ";O2_dc_offset
4140 PRINT USING "/,K,D,4DE";"CO2 CALIBRATION FACTOR = ";Co2_cal
4145 PRINT USING "/,K,D,4DE";"O2 CALIBRATION FACTOR = ";O2_cal
4150 PRINT USING "/,K";"THE NON CORRECTED FLOW CALIBRATION FACTORS"
4155 PRINT USING "/, #, K";"    INSPIRATORY FLOW CALIBRATION FACTOR = "
4160 PRINT USING "D,4DE";Non_c_i_flowcal
4165 PRINT USING "/, #, K";"    EXPIRATORY FLOW CALIBRATION FACTOR = "
4170 PRINT USING "D,4DE";Non_c_e_flowcal
4175 PRINT USING "2/,K";"THE TEMPERATURE CORRECTED FLOW CALIBRATION FACTORS"
4180 PRINT USING "/, #, K";"    INSPIRATORY FLOW CALIBRATION FACTOR = "
4185 PRINT USING "D,4DE";Corr_i_flowcal
4190 PRINT USING "/, #, K";"    EXPIRATORY FLOW CALIBRATION FACTOR = "
4195 PRINT USING "D,4DE, /";Corr_e_flowcal
4200 PRINT USING "/, #, K,MD,4DE,K";"TEMPERATURE CORRECTION = ";Ta;"X^2 "
4205 PRINT USING "#,K,MD,4DE,K";"+ ";Tb;"X "
4210 PRINT USING "K,MD,4DE";"+ ";Tc
4215 PRINT USING "/,K,DDD";"SAMPLING FREQUENCY = ";S
4220 PRINT USING "/,K";"FLOW CALIBRATION FILENAME: "&Ca1$
4225 PRINT USING "/,K";"CO2 DATA FILENAME: "&C1$
4230 PRINT USING "/,K";"O2 DATA FILENAME: "&O$
4235 PRINT USING "/,K";"FLOW DATA FILENAME: "&F$
4240 PRINT USING "/,K";"TEMPERATURE DATA FILENAME: "&T$
4245 PRINTER IS 1
4250 RETURN
4255 !
4260 !*** SUBROUTINE TO PLOT OUT THE FOUR BINARY DATA SETS
4265 !
4270 Dtplo:PRINT Formfd$;"          DATA PLOTTING ROUTINE"
4275 PRINT USING "3/,K,5D,K";"THERE ARE ";No_points;" DATA POINTS AVAILABLE"
4280 !
4285 !*** OBTAIN STARTING AND ENDING POINTS TO PLOT
4290 !
4295 BEEP
4300 INPUT "ENTER STARTING POINT TO PLOT.",Start
4305 IF Start<1 OR Start>No_points THEN GOTO 4300
4310 BEEP
4315 INPUT "ENTER ENDING POINT TO PLOT.",End
4320 IF End<=Start OR End>No_points THEN GOTO 4315
4325 !
4330 !*** COMPUTER NUMBER OF POINTS TO PROCESS
4335 !
4340 P=End-Start+1
4345 !
4350 !*** COMPUTE PLOTTING OFFSET FOR MASS SPECTROMETER DELAYS
4355 !
4360 Offset=INT(Time_delay/1000*S)
4365 !
4370 !*** DETERMINE MAXIMUM AND MINIMUM VALUES FOR THE PLOTTED POINTS
4375 !
4380 Cmax=Line1(Start)
4385 Cmin=Line1(Start)
4390 Omax=Line2(Start)
4395 Omin=Line2(Start)
4400 Fmax=Line3(Start)
4405 Fmin=Line3(Start)

```



```

4410 Tmax=Line4(Start)
4415 Tmin=Line4(Start)
4420 FOR A=Start+1 TO End
4425   IF Cmax<Line1(A) THEN Cmax=Line1(A)
4430   IF Cmin>Line1(A) THEN Cmin=Line1(A)
4435   IF Omax<Line2(A) THEN Omax=Line2(A)
4440   IF Omin>Line2(A) THEN Omin=Line2(A)
4445   IF Fmax<Line3(A) THEN Fmax=Line3(A)
4450   IF Fmin>Line3(A) THEN Fmin=Line3(A)
4455   IF Tmax<Line4(A) THEN Tmax=Line4(A)
4460   IF Tmin>Line4(A) THEN Tmin=Line4(A)
4465 NEXT A
4470 !
4475 !*** DISPLAY THE MAXIMUM AND MINIMUM VALUES ON THE CRT
4480 !
4485 DISP
4490 PRINT
4495 PRINT "CO2 MAX: ";Cmax;TAB(25);"CO2 MIN: ";Cmin
4500 PRINT
4505 PRINT "O2 MAX: ";Omax;TAB(25);"O2 MIN: ";Omin
4510 PRINT
4515 PRINT "FLOW MAX: ";Fmax;TAB(25);"FLOW MIN: ";Fmin
4520 PRINT
4525 PRINT "TEMP MAX: ";Tmax;TAB(25);"TEMP MIN: ";Tmin
4530 !
4535 !*** ADJUST MAXIMUM AND MINIMUM PLOTTING VALUES FOR SMALL INPUT CHANGES
4540 !
4545 IF Fmax-Fmin<=100 THEN
4550   Fmax=4095
4555   Fmin=0
4560 END IF
4565 IF Cmax-Cmin<=100 THEN
4570   Cmax=4095
4575   Cmin=0
4580 END IF
4585 IF Omax-Omin<=100 THEN
4590   Omax=4095
4595   Omin=0
4600 END IF
4605 IF Tmax-Tmin<=100 THEN
4610   Tmax=4095
4615   Tmin=0
4620 END IF
4625 !
4630 !*** IF NO TEMPERATURE CALIBRATION DATA IS AVAILABLE, ONLY PLOT BINARY
4635 !*** TEMPERATURE DATA
4640 !
4645 IF (Ta=0) AND (Tc=0) THEN
4650   Ta=0
4655   Tc=0
4660   Tb=1
4665 END IF
4670 !
4675 !*** ALLOW USER TO SELECT PLOTTING DEVICE
4680 !
4685 BEEP
4690 ON KBD,15 GOTO Sel_plt_dev
4695 PRINT
4700 PRINT
4705 PRINT "You have 20 seconds to select a PLOTTING device."
4710 PRINT "If you do not select a device in that time, the"
4715 PRINT "CRT will automatically be selected. To select"
4720 PRINT "a device press the space bar."
4725 FOR I=1 TO 100000
4730 !

```

--- This loop delays approximately 20 seconds.

```

4735 NEXT I
4740 OFF KBD
4745 QS="CRT"
4750 GOTO 4795          ! Skip and use the CRT.
4755 !
4760 !
4765 Sel_plt_dev:OFF KBD ! Allow the user to select the plotting device.
4770 QS=""
4775 BEEP
4780 INPUT "OUTPUT ON PLOTTER OR CRT ? (PLOTTER/CRT)",QS
4785 !
4790 !
4795 IF QS="PLOTTER" THEN
4800 !
4805 !*** SET SYSTEM FOR HP9872C PLOTTER
4810 !
4815 PLOTTER IS 705,"HPGL"
4820 PRINTER IS 705
4825 PRINT "VS5;"
4830 PRINTER IS 1
4835 ELSE
4840 PLOTTER IS 3,"INTERNAL"
4845 DUMP DEVICE IS 701
4850 END IF
4855 !
4860 !*** INITIALIZE GRAPHICS SYSTEM
4865 !
4870 GRAPHICS ON
4875 GCLEAR
4880 PRINT Formfd$
4885 PEN 1
4890 DEG !SET DEGREES MODE
4895 !
4900 !*** PLOT THE TEMPERATURE DATA ARRAY
4905 !
4910 View(0,100,4,24)
4915 Ctmin=Ta*Tmin^2+Tb*Tmin+Tc
4920 Ctmax=Ta*Tmax^2+Tb*Tmax+Tc
4925 Left=-P*.13
4930 Right=P
4935 WINDOW Left,Right,Ctmin,Ctmax
4940 CLIP 0,Right,Ctmin,Ctmax
4945 LINE TYPE 1 !SET FOR SOLID LINE
4950 CSIZE 2.8
4955 LDIR 0
4960 LORG 2 !SET LABEL ORIGIN TO POSITION 8
4965 AXES P/20,(Ctmax-Ctmin)/10,0,Ctmin
4970 CLIP Left,Right,Ctmin,Ctmax
4975 IF (Ctmin=Tmin) AND (Ctmax=Tmax) THEN 5015
4980 Incr=(Ctmax-Ctmin)/5
4985 LORG 8
4990 FOR I=Ctmin+Incr TO 1.001*(Ctmax-Incr) STEP Incr
4995 MOVE 0,I
5000 LABEL USING 5005;I
5005 IMAGE ZZ.D," "
5010 NEXT I
5015 CSIZE 3.3
5020 MOVE 1,Ta*Line4(Start)^2+Tb*Line4(Start)+Tc
5025 PEN 2
5030 FOR I=Start TO End
5035 Temp=Ta*Line4(I)*Line4(I)+Tb*Line4(I)+Tc
5040 PLOT I-Start+1,Temp
5045 NEXT I
5050 PENUP
5055 PEN 1

```

```

5060 CSIZE 2.5
5065 LINE TYPE 1
5070 !
5075 !*** LABEL THE TEMPERATURE PLOT
5080 !
5085 MOVE Left, (Ctmin+Ctmax)/2
5090 LONG 6
5095 LDIR 90
5100 LABEL "FLOW TEMP"
5105 MOVE Left*.85, (Ctmin+Ctmax)/2
5110 LABEL "DEGREES C"
5115 View(0,100,24,28)
5120 WINDOW 0,10,0,10
5125 MOVE 2,10
5130 LDIR 0
5135 LONG 3
5140 LABEL "START POINT ="&VAL$(Start)& " END POINT = "&VAL$(End)
5145 MOVE 10,10
5150 LONG 9
5155 LABEL "1 TICK =" ; DROUND(P/(20*S),3); " SECONDS "
5160 !
5165 !*** PLOT THE FLOW DATA ARRAY
5170 !
5175 View(0,100,28,48)
5180 WINDOW Left,Right,Fmin*1.02,Fmax*1.02
5185 LINE TYPE 1
5190 CLIP 0,Right,Fmin,Fmax
5195 AXES P/20, (Fmax-Fmin)/10,0,Bin_zero_flow
5200 CLIP Left,Right,Fmin,Fmax
5205 IF NOT (Non_c_i_flowcal=0) THEN
5210     CSIZE 2.8
5215     LONG 8
5220     IMAGE DDD.DD, " "
5225     Incr=(Fmax-Fmin)/5
5230 !
5235 !   Label the expiratory flow axis
5240 !
5245     FOR I=Bin_zero_flow TO Fmax STEP Incr
5250         MOVE 0,I
5255         LABEL USING 5220;(I-Bin_zero_flow)*Non_c_e_flowcal
5260     NEXT I
5265 !
5270 !   Label the inspiratory flow
5275     FOR I=Bin_zero_flow-Incr TO Fmin STEP -Incr
5280         MOVE 0,I
5285         LABEL USING 5220;(I-Bin_zero_flow)*Non_c_i_flowcal
5290     NEXT I
5295 END IF
5300 CSIZE 3.3
5305 MOVE 1,Line3(Start)
5310 PEN 2
5315 FOR I=Start TO End
5320     PLOT I-Start+1,Line3(I)
5325 NEXT I
5330 PENUP
5335 PEN 1
5340 LINE TYPE 1
5345 CSIZE 2.5
5350 !
5355 !*** LABEL THE FLOW PLOT
5360 !
5365 MOVE Left, (Fmax+Fmin)/2
5370 LONG 6
5375 LDIR 90
5380 LABEL "FLOW [L/S]"

```



```

5385 !
5390 !*** PLOT THE O2 DATA ARRAY
5395 !
5400 View(0,100,52,72)
5405 WINDOW Left,Right,Qmin,Qmax
5410 CLIP 0,Right,Qmin,Qmax
5415 AXES P/20,Qmax/10,0,Qmin
5420 CLIP Left,Right,Qmin,Qmax
5425 LDIR 0
5430 IF NOT (O2_cal=0) THEN
5435     CSIZE 2.8
5440     LORG 8
5445     IMAGE DD.D," "
5450     Incr=(Qmax-Qmin)/5
5455     FOR I=Qmin+Incr TO (Qmax-Incr)*1.01 STEP Incr
5460         MOVE 0,I
5465         LABEL USING 5445;((I-O2_dc_offset)*O2_cal+01)*100
5470     NEXT I
5475 END IF
5480 MOVE 1,Line2(Start+Offset)-O2_dc_offset
5485 PEN 2
5490 FOR I=Start TO End-Offset
5495     PLOT I-Start+1,Line2(I+Offset)
5500 NEXT I
5505 PENUP
5510 PEN 1
5515 !
5520 !*** LABEL THE O2 PLOT
5525 !
5530 MOVE Left,(Qmax+Qmin)/2
5535 LORG 6
5540 LDIR 90
5545 CSIZE 2.5
5550 LABEL "FRACTIONAL O2"
5555 MOVE Left*.85,(Qmax+Qmin)/2
5560 LABEL "CONCENTRATION"
5565 !
5570 !*** PLOT THE CO2 DATA ARRAY
5575 !
5580 View(0,100,76,96)
5585 WINDOW Left,Right,Qmin,Qmax
5590 CLIP 0,Right,Qmin,Qmax
5595 AXES P/20,(Qmax-Qmin)/10,0,Qmin
5600 CLIP Left,Right,Qmin,Qmax
5605 IF NOT (Co2_cal=0) THEN
5610     LDIR 0
5615     CSIZE 2.8
5620     LORG 8
5625     Incr=(Qmax-Qmin)/5
5630     FOR I=Qmin+Incr TO (Qmax-Incr)*1.01 STEP Incr
5635         MOVE 0,I
5640         LABEL USING 5445;(I-Co2_dc_offset)*Co2_cal*100
5645     NEXT I
5650 END IF
5655 LINE TYPE 1
5660 MOVE 1,Line1(Start+Offset)
5665 PEN 2
5670 FOR I=Start TO End-Offset
5675     PLOT I-Start+1,Line1(I+Offset)
5680 NEXT I
5685 PENUP
5690 PEN 1
5695 !
5700 !*** LABEL THE CO2 PLOT
5705 !

```

```

5710  LOGR 6
5715  CSIZE 2.3
5720  LDIR 90
5725  MOVE Left,(Gmax+Cmin)/2
5730  LABEL "FRACTIONAL CO2"
5735  MOVE Left*.85,(Gmax+Cmin)/2
5740  LABEL "CONCENTRATION"
5745  QS=""
5750  !
5755  !*** PUT PEN AWAY AND PAUSE FOR USER TO OBSERVE PLOT
5760  !
5765  PEN 0
5770  BEEP
5775  PAUSE
5780  !
5785  !*** ONCE PAUSE IS COMPLETE, PROMPT THE USER FOR REDO OF GRAPHICS
5790  !
5795  GRAPHICS OFF
5800  QS=""
5805  BEEP
5810  INPUT "REDO GRAPHICS? (Y/N)",QS
5815  !
5820  !*** IF DESIRED, GO START PLOTTING SUBROUTINE OVER
5825  !
5830  IF QS="Y" OR QS="y" THEN GOTO DtploT
5835  !
5840  !*** OTHERWISE, RETURN BACK TO BEGIN BREATH-BY-BREATH ANALYSIS
5845  !
5850  RETURN
5855  !
5860  !***SUBROUTINE FOR RETRIEVING FOUR CHANNELS OF BINARY DATA FROM STORAGE
5865  !
5870  !
5875  !*** GET THE NAMES OF THE FOUR FILES
5880  !
5885  Rtdata:BEEP
5890  INPUT "ENTER THE CO2 SIGNAL FILE NAME",C1$
5895  BEEP
5900  O$="O"&C1$(2,LEN(C1$)) ! Set the default oxygen file name
5905  INPUT "ENTER THE O2 SIGNAL FILE NAME",O$
5910  BEEP
5915  V$="V"&C1$(2,LEN(C1$)) ! Set the default flow file name
5920  INPUT "ENTER THE FLOW SIGNAL FILE NAME",V$
5925  BEEP
5930  T$="T"&C1$(2,LEN(C1$)) ! Set the default temperature file name
5935  INPUT "ENTER THE FLOW TEMPERATURE SIGNAL FILE NAME",T$
5940  !
5945  !*** SELECT PROPER MASS STORAGE UNIT AND OPEN THE FILES
5950  !
5955  MASS STORAGE IS ":HP9895,700,0"
5960  ASSIGN @Co2_path TO C1$
5965  ASSIGN @O2_path TO O$
5970  ASSIGN @Flow_path TO V$
5975  ASSIGN @Temp_path TO T$
5980  !
5985  !*** TELL PROGRAM WHEN TO QUIT READING THE FILES
5990  !
5995  ON END @Co2_path GOTO 6055
6000  ON END @O2_path GOTO 6080
6005  ON END @Flow_path GOTO 6105
6010  ON END @Temp_path GOTO 6130
6015  !
6020  !*** READ THE CO2 DATA FILE
6025  !
6030  ENTER @Co2_path;Gmax,Cmin

```

```

6035 ENTER @Co2_path;Line1(*)
6040 !
6045 !*** READ THE O2 DATA FILE
6050 !
6055 ENTER @O2_path;Qmax,Qmin
6060 ENTER @O2_path;Line2(*)
6065 !
6070 !*** READ THE FLOW DATA FILE
6075 !
6080 ENTER @Flow_path;Fmax,Fmin
6085 ENTER @Flow_path;Line3(*)
6090 !
6095 !*** READ THE TEMPERATURE DATA FILE
6100 !
6105 ENTER @Temp_path;Tmax,Tmin
6110 ENTER @Temp_path;Line4(*)
6115 !
6120 !*** CLOSE THE FILES AND SET MASS STORAGE UNIT BACK TO INTERNAL FLOPPY
6125 !
6130 ASSIGN @Co2_path TO *
6135 ASSIGN @O2_path TO *
6140 ASSIGN @Flow_path TO *
6145 ASSIGN @Temp_path TO *
6150 MASS STORAGE IS ":INTERNAL"
6155 !
6160 !*** RETURN BACK TO ANALYSIS ROUTINE
6165 !
6170 RETURN
6175 !
6180 !*** SUBROUTINE FOR RETRIEVING CALIBRATION FACTORS FROM MASS STORAGE
6185 !
6190 !
6195 !*** GET CALIBRATION FILE NAME AND ASSIGN PROPER MASS STORAGE UNIT
6200 !
6205 Rtccl:BEEP
6210 INPUT "ENTER CALIBRATION FILE FILENAME",Cal$
6215 !
6220 !*** OPEN CALIBRATION FILE AND TELL PROGRAM WHEN TO STOP READING FILE
6225 !
6230 ASSIGN @Cal_path TO Cal$&" :HP9895,700,0"
6235 ON END @Cal_path GOTO Cal_flg_is_read
6240 !
6245 !*** READ PARAMETERS IN CALIBRATION FILE
6250 !
6255 ENTER @Cal_path;Co2_dc_offset,O2_dc_offset,Bin_zero_flow
6260 ENTER @Cal_path;Co2_cal,O2_cal
6265 ENTER @Cal_path;Non_c_i_flowcal,Non_c_e_flowcal
6270 ENTER @Cal_path;Time_delay,S,O1,Ta,Tb,Tc,Date$
6275 ENTER @Cal_path;Corr_i_flowcal,Corr_e_flowcal
6280 ENTER @Cal_path;Pb,Rel_humid,Room_temp
6285 !
6305 Cal_flg_is_read: ! The calibration file has been entered so return.
6310 ASSIGN @Cal_path TO * !close Cal_path
6315 RETURN
6320 !
6325 !*** SUBROUTINE TO DETERMINE MASS SPECTROMETER TIME DELAY ON A BREATH-
6330 !*** BY-BREATH BASIS
6335 !
6340 Bbb_time_delay:Temp_a=A
6345 Temp_z=Z
6350 C=Co2_dc_offset !SET C TO BINARY ZERO CO2 VALUE
6355 !
6360 !*** BEGINNING AT POINT ON FLOW SIGNAL CORRESPONDING TO ZERO FLOW,
6365 !*** LOCATE PEAK END EXPIRED CO2 VALUE
6370 !

```

```

6375 Hunt_max:=Z-A          !CO2 INDEX CORRESPONDING TO ZERO FLOW
6380 IF No_points-Z<50 THEN Bomb_out  !MAKE SURE 50 POINTS FOLLOW ZERO CROS
SING
6385 Co2max=Line1(Z)-C      !SET INITIAL CO2MAX LEVEL TO FIRST CO2 VALUE
6390 Max_index=Z
6395 FOR Wye=Z TO Z+.75*S  !SEARCH AHEAD FOR THE MAX END EXPIRED FCO2 VALUE
6400     IF Line1(Wye)-C>Co2max THEN Max_index=Wye
6405     IF Line1(Wye)-C>Co2max THEN Co2max=Line1(Wye)-C
6410 NEXT Wye
6415 !
6420 !*** FIND THE MIDDLE INDEX (THAT POINT CORRESPONDING TO 50% OF THE MAX.
6425 !*** END EXPIRED CO2 VALUE)
6430 !
6435 Mid_index=Max_index
6440 FOR Wye=Max_index TO Z+.75*S
6445     IF Line1(Wye)-C>.5*Co2max THEN Next_wye
6450     Mid_index=Wye      ! INDEX OF THE 50% DOWN POINT ON FCO2 CURVE
6455     GOTO Set_limits
6460 Next_wye:NEXT Wye
6465 !
6470 !** FIND THE MINIMUM INDEX (THAT POINT CORRESPONDING TO THE MINIMUM END
6475 !** EXPIRED CO2 VALUE
6480 !
6485 Set_limits:Min_index=Mid_index
6490 Co2min=Line1(Mid_index)-C
6495 FOR Wye=Mid_index TO Mid_index+Mid_index-Max_index
6500     IF Line1(Wye)-C>Co2min THEN Next_y
6505     Min_index=Wye
6510     Co2min=Line1(Wye)-C
6515 Next_y:NEXT Wye
6520 !
6525 !*** INITIALIZE INDEXES FOR START OF INTEGRATION OF CO2 SIGNAL
6530 !
6535 Best_match=1.E+50
6540 Beg_pt=Max_index
6545 End_pt=Min_index
6550 !
6555 !*** EXIT ROUTINE IF ADEQUATE NUMBER OF POINTS DO NOT EXIST
6560 !
6565 IF End_pt>No_points THEN Bomb_out
6570 Beg_intg=Max_index
6575 End_intg=Min_index
6580 !
6585 !*** USE TRAPEZOIDAL RULE TO COMPUTE THE AREA ABOVE AND BELOW THE CURVE
6590 !
6595 New_sum:=Asum:=0
6600 Bsum=0
6605 !
6610 !*** FIRST, ABOVE THE CURVE, 1/2 OF FIRST AND LAST POINTS
6615 !
6620 Asum=.5*(Co2max-(Line1(Beg_pt)-C))+.5*(Co2max-(Line1(Beg_intg)-C))
6625 FOR Wye=Beg_pt+1 TO Beg_intg-1
6630     Asum=Asum+Co2max-(Line1(Wye)-C)
6635 NEXT Wye
6640 !
6645 !*** NEXT, BELOW THE CURVE, 1/2 OF FIRST AND LAST POINTS
6650 !
6655 Bsum=.5*(Line1(Beg_intg)-Co2_dc_offset)+.5*(Line1(End_pt)-Co2_dc_offset)
6660 FOR Wye=Beg_intg+1 TO End_pt-1
6665     Bsum=Bsum+Line1(Wye)-Co2_dc_offset
6670 NEXT Wye
6675 !
6680 !*** COMPUTE DIFFERENCE IN THE TWO AREAS
6685 !
6690 Adiff=ABS(Asum-Bsum)

```

```

6695 !
6700 !*** IF AREA DIFFERENCE IS A MINIMUM, REMEMBER THE PROPER INDEX
6705 !
6710 IF Adiff<Best_match THEN Best_index=Beg_intg
6715 IF Adiff<Best_match THEN Best_match=Adiff
6720 !
6725 !*** BUMP THE CENTER INTEGRATION POINT AND GO TRY ANOTHER IF STILL
6730 !*** WITHIN OUTER LIMITS OF INTEGRATION
6735 !
6740 Beg_intg=Beg_intg+1 ! IF NOT TO ENDPOINT SHIFT THE CENTER INTEGR POINT
6745 IF Beg_intg<=End_intg THEN New_sum ! GO COMPUTE NEW AREAS FOR LIMITS
6750 !
6755 !*** COMPUTE MASS SPECTROMETER TIME DELAY FOR THIS BREATH AND RETURN
6760 !*** BACK TO ANALYSIS ROUTINE WITH VARIABLES UNALTERED.
6765 !
6770 Bomb_out: ! DATA STREAM EXHAUSTED
6775 Time_delay=(Best_index-Z)/S*1000
6780 A=Temp_a
6785 Z=Temp_z
6790 RETURN
6795 END
6800 !*****
6805 !
6810 !

```

```

6815 SUB Calc_sig_val(INTEGER A,Z,Insp_or_expr$,REAL Incr_vol,Fo2,Fco2)
6820   GOTO Skip_comments
6825 ! *****
6830 ! *****
6835 ! ****
6840 !**** Section Title: Inspiratory and expiratory signal values. ****
6845 !****
6850 !**** Revision      Date              Programmer      ****
6855 !**** -----      -              -              ****
6860 !****      1.0      January 1, 1985      Michael Masters ****
6865 !****
6870 !*****
6875 !****
6880 !**** Purpose: To calculate the incremental signal values for ****
6885 !**** current data sample. The incremental volume is calc-****
6890 !**** ulated and is converted to STPD conditions if the ****
6895 !**** Temperature correction is requested. The fractional ****
6900 !**** carbon dioxide and oxygen fractional concentrations ****
6905 !**** are also calculated. ****
6910 !****
6915 !**** Parameters passed from the calling routine ****
6920 !**** A - The index to the flow and temperature data. ****
6925 !****
6930 !**** Z - The index to the gas (O2 and CO2) data. ****
6935 !****
6940 !**** Insp_or_expr$ - a flag indicating an inspiratory or ****
6945 !**** an expiratory flow. ****
6950 !****
6955 !**** Parameters returned to the calling routine ****
6960 !**** Incr_vol - the incremental volume of air under STPD ****
6965 !**** conditions. ****
6970 !****
6975 !**** Fo2,Fco2 - the dry fractional values of O2 and CO2. ****
6980 !****
6985 !**** Routine(s) Called: ****
6990 !**** Function FNRel_viscos ****
6995 !****
7000 !*****
7005 Skip_comments: !
7010 COM /Resp_data1/ INTEGER Line1(1:24000),Line2(1:24000)
7015 COM /Resp_data2/ INTEGER Line3(1:24000),Line4(1:24000)
7020 COM /Cal_data2/ INTEGER Co2_dc_offset,O2_dc_offset,Bin_zero_flow,S
7025 COM /Cal_data3/ REAL Co2_cal,O2_cal
7030 COM /Cal_data6/ REAL Ta,Tb,Tc
7035 COM /Cal_data7/ REAL Time_delay,O1,Pb,Rel_humid,Room_temp
7040 COM /Anal_data6/ INTEGER Corr_flag,REAL Room_fh2o,T
7045 COM /Anal_data7/ Vap(0:250),Fh2o_sat(0:250)
7050 !
7055 ! Determine the CO2 and O2 fractional concentrations
7060 !
7065 Fco2=(Line1(Z)-Co2_dc_offset)*Co2_cal
7070 Fco2=(Line2(Z)-O2_dc_offset)*O2_cal+O1
7075 !
7080 !
7085 IF Corr_flag THEN
7090 Temperature=Ta*Line4(A)*Line4(A)+Tb*Line4(A)+Tc
7095 IF Insp_or_expr$="INSP" THEN
7100 Fh2o=Room_fh2o
7105 ELSE
7110 Fh2o=Fh2o_sat((Temperature-20)*10)
7115 END IF
7120 Fco2_wet=Fco2*(1.0-Fh2o)
7125 Fo2_wet=Fo2*(1.0-Fh2o)
7130 Fn2_wet=1.0-Fco2_wet-Fo2_wet-Fh2o
7135 !

```

```

7140 !           The binary flow is equal to (binary delta-P/viscosity).
7145 Rel_viscosity=FNRel_viscos(Fo2_wet,Fco2_wet,Fn2_wet,Fh2o,Temperat
ure)
7150 Bin_flow=(Line3(A)-Bin_zero_flow)/Rel_viscosity
7155 !
7160 !           Convert the incremental binary volume to STPD conditions.
7165 Incr_vol=Bin_flow*(1.0-Fh2o)*273.15/(273.15+Temperature)*Pb/760.0
*T
7170 ELSE
7175 Incr_vol=(Line3(A)-Bin_zero_flow)*T
7180 END IF
7185 SUBEND
7190 !
7195 !

7200 DEF FNRel_viscos(Fo2,Fco2,Fn2,Fh2o,Temperature)
7205 GOTO Skip_comments
7210 !*****
7215 !*****
7220 !****
7225 !**** Routine Title: Relative viscosity function
7230 !****
7235 !**** HP BASIC FILENAME: Analysis
7240 !****
7245 !**** Department of Electrical and Computer Engineering,
7250 !**** Kansas State University
7255 !****
7260 !**** Revision Date Programmer
7265 !**** -----
7270 !**** 1.0 August 23, 1984 Michael Masters
7275 !****
7280 !*****
7285 !****
7290 !**** Purpose: To calculate the relative viscosity of a gas
7295 !**** containing carbon dioxide (CO2), oxygen (O2), nitrogen
7300 !**** (N2), and water vapor at a temperature (T). The
7305 !**** viscosity is expressed relative to room air under STPD
7310 !**** conditions. The calling sequence is:
7315 !****
7320 !**** variable = FNRel_viscos(Fo2,Fco2,Fn2,Fh2o,Temperature)
7325 !****
7330 !**** where:
7335 !****
7340 !**** Fo2,Fco2,Fn2,Fh2o - the fractional gas conc.
7345 !**** of O2, CO2, and water vapor in the gas.
7350 !****
7355 !**** Temperature - the instantaneous temperature of the gas
7360 !****
7365 !*****
7370 Skip_comments: !
7375 !
7380 !           Calculate the individual viscosities
7385 Vis_n2=165.4+.451*Temperature
7390 Vis_o2=188.0+.606*Temperature
7395 Vis_co2=187.1+.612*Temperature
7400 Vis_h2o=117.6+.506*Temperature
7405 !
7410 Rel_vis=(Fo2*Vis_o2+Fco2*Vis_co2+Fn2*Vis_n2+Fh2o*Vis_h2o)/170.17502
7415 RETURN Rel_vis
7420 FNEND
7425 !
7430 !

```



```

7435 DEF FNInspiration(INTEGER Pntr)
7440   GOTO Skip_comments
7445   !*****
7450   !*****
7455   !****
7460   !**** Function Title:  Inspiratory flow.
7465   !****
7470   !**** Revision      Date              Programmer
7475   !**** -----      -
7480   !****      1.0      January 1, 1985    Michael Masters
7485   !****
7490   !*****
7495   !****
7500   !**** Purpose: To determine if the flow point is an inspiration.
7505   !**** The point is an inspiratory flow if it is less than the
7510   !**** zero flow value or any of the next five data points are
7515   !**** less than or equal to the zero flow value.
7520   !****
7525   !**** Parameters passed from the calling routine
7530   !****
7535   !****      Pntr - Points to the flow data point.
7540   !****
7545   !**** The routine returns a logical value of True if the flow is
7550   !**** inspiratory, otherwise false.
7555   !****
7560   !**** Routine(s) Called:      None
7565   !****
7570   !*****
7575   !*****
7580 Skip_comments: !
7585   COM /Resp_data2/ INTEGER Line3(1:24000),Line4(1:24000)
7590   COM /Cal_data2/  INTEGER Co2_dc_offset,O2_dc_offset,Bin_zero_flow,S
7595   INTEGER Inspiration,I
7600   Inspiration=(Line3(Pntr)<Bin_zero_flow)
7605   I=1
7610   WHILE NOT (Inspiration) AND I<=5
7615     Inspiration=(Line3(Pntr+I)<=Bin_zero_flow)
7620     I=I+1
7625   END WHILE
7630   RETURN Inspiration
7635 FNEND
7640 !
7645 !

```



```

7650 DEF FNExpiration(INTEGER Pntr)
7655     GOTO Skip_comments
7660 !*****
7665 !*****
7670 !****
7675 !**** Function Title: Expiratory flow. ****
7680 !****
7685 !**** Revision      Date              Programmer ****
7690 !**** -----
7695 !**** 1.0          January 1, 1985    Michael Masters ****
7700 !****
7705 !*****
7710 !****
7715 !**** Purpose: To determine if the flow point is an expiration. ****
7720 !**** The point is an expiratory flow if it is greater than ****
7725 !**** the zero flow value or any of the next five data points ****
7730 !**** are greater than or equal to the zero flow value. ****
7735 !****
7740 !**** Parameters passed from the calling routine ****
7745 !****
7750 !**** Pntr - Points to the flow data point. ****
7755 !****
7760 !**** The routine returns a logical value of True if the flow is ****
7765 !**** expiratory, otherwise false. ****
7770 !****
7775 !**** Routine(s) Called: None ****
7780 !****
7785 !*****
7790 !*****
7795 Skip_comments: !
7800     COM /Resp_data2/ INTEGER Line3(1:24000),Line4(1:24000)
7805     COM /Cal_data2/ INTEGER Co2_dc_offset,O2_dc_offset,Bin_zero_flow,S
7810     INTEGER Expiration,l
7815     Expiration=(Line3(Pntr)>Bin_zero_flow)
7820     l=1
7825     WHILE NOT (Expiration) AND l<=5
7830         Expiration=(Line3(Pntr+l)>=Bin_zero_flow)
7835         l=l+1
7840     END WHILE
7845     RETURN Expiration
7850 FNEND

```

```

7855 DEF FNMax_co2_pntr(INTEGER Line1(*),A)
7860 !*****
7865 !*****
7870 !****
7875 !**** Function Title: Find maximum CO2 value.
7880 !****
7885 !**** Revision      Date              Programmer
7890 !**** -----
7895 !**** 1.0          December 1, 1984    Rick Pieschl
7900 !****
7905 !*****
7910 !****
7915 !**** Purpose: To determine the point where the maximum CO2
7920 !**** value occurred. This point is assumed to be the end
7925 !**** expiratory point.
7930 !****
7935 !**** Parameters passed from the calling routine
7940 !****
7945 !**** Line1 - The Binary CO2 data.
7950 !****
7955 !**** A - The point corresponding to expiratory/inspiratory
7960 !**** transition.
7965 !****
7970 !**** The routine returns a value equal to the end expirate value
7975 !****
7980 !**** Routine(s) Called:      None
7985 !****
7990 !*****
7995 !*****
8000 INTEGER Max,I
8005 Max=A-50
8010 I=A-50
8015 REPEAT
8020 IF Line1(I)>Line1(Max) THEN Max=I
8025 Max=I
8030 I=I+1
8035 UNTIL I>A
8040 RETURN Max
8045 FNEND
8050 !
8055 !
8060 SUB Disp_results(INTEGER Breaths,Corr_flag)
8065 !*****
8070 !****
8075 !**** Routine Title: Disp_results
8080 !****
8085 !**** HP BASIC FILENAME: ANALYSIS
8090 !****
8095 !**** Department of Electrical and Computer Engineering,
8100 !**** Kansas State University
8105 !****
8110 !**** Revision      Date              Programmer
8115 !**** -----
8120 !**** 1.0          Sept. 10, 1984    Michael Masters
8125 !****
8130 !*****
8135 !****
8140 !**** Purpose:
8145 !**** This subroutine displays the breath by breath
8150 !**** respiratory data calculated in the analysis routine.
8155 !****
8160 !****
8165 !**** Routine(s) Called
8170 !**** Max_min - Determines the maximum and minum values of
8175 !**** the respiratory variable to be plotted.

```

```

8180 !****
8185 !****      Veiw - Sets the plotting areas on the screen or the ****
8190 !****      plotter. ****
8195 !**** ****
8200 !****      Make_axes - Defines the dimensions of the plotting ****
8205 !****      area based on the maximum and minum values to ****
8210 !****      be plotted. Draws and labels the axes and ****
8215 !****      also labels the plot. ****
8220 !**** ****
8225 !****      Plot_values - Plots the values of the respiratory ****
8230 !****      variable. ****
8235 !**** ****
8240 !****      Print_values - Plots the values of the respiratory ****
8245 !****      variable. ****
8250 !**** ****
8255 !*****
8260 !*****
8265 COM /Cal_data1/ Cal$[10],Date$[25]
8270 COM /Anal_data2/ INTEGER True,False
8275 COM /Anal_data3/ INTEGER Time_of_brth,O2_cons,Co2_prod,Insp_min_vent
8280 COM /Anal_data4/ INTEGER Expr_min_vent,V_tid_insp,V_tid_expr,Resp_fr
      eq
8285 COM /Anal_data5/ INTEGER Breath_good,Resp_quotient,Formfd$[1]
8290 COM /Anal_data5a/ INTEGER Frc_o2_cons,Frc_co2_prod,Volume_of_lung
8295 COM /Anal_data8/ Resp_var(0:12,1:500)
8300 COM /Anal_data9/ Name$[25],Comment$[46]
8305 COM /Plot_resp_data1/ INTEGER Omit_bad,Num_breaths,No_b_avg
8310 COM /Plot_resp_data2/ Start_time,End_time,W_period,W_width
8315 INTEGER Fig1,Fig2
8320 DIM Time1$[20],Event1$[50],Time2$[20],Event2$[50]
8325 DIM Title$[40],Avg_bad_comnt$[65],Avg_type$[7],Result_type$[5]
8330 Num_breaths=Breaths
8335 !      Repeat until the user no longer desires to plot the
8340 !      results.
8345 REPEAT
8350 PRINT Formfd$
8355 PRINT "Which of the following options do you wish to do?"
8360 PRINT
8365 PRINT " 1. Plot the results."
8370 PRINT " 2. Print the results."
8375 REPEAT
8380 QS=""
8385 BEEP
8390 INPUT "Enter the option (1 or 2) ",QS
8395 UNTIL QS="1" OR QS="2"
8400 IF QS="1" THEN
8405 Result_type$="PLOT"
8410 ELSE
8415 Result_type$="PRINT"
8420 END IF
8425 PRINT Formfd$,"How do you wish to combine breaths?"
8430 PRINT
8435 PRINT " 1. The individual breaths."
8440 PRINT " 2. Average individual breaths."
8445 PRINT " 3. Avarage windows of breaths."
8450 REPEAT
8455 QS=""
8460 BEEP
8465 INPUT "Enter the option (1,2 or 3) ",QS
8470 UNTIL QS="1" OR QS="2" OR QS="3"
8475 PRINT Formfd$
8480 SELECT QS
8485 CASE "1"
8490 Avg_type$="AVERAGE"
8495 No_b_avg=1

```

```

8500      Start_time=Resp_var(Time_of_brth,1)
8505      IF Start_time<=5 THEN Start_time=0
8510      End_time=Resp_var(Time_of_brth,NumBreaths)
8515      CASE ="2"
8520          Avg_type$="AVERAGE"
8525          BEEP
8530          INPUT "How many breaths do you wish to average?",No_b_avg
8535          Start_time=Resp_var(Time_of_brth,1)
8540          IF Start_time<=5 THEN Start_time=0
8545          End_time=Resp_var(Time_of_brth,NumBreaths)
8550      CASE ="3"
8555          Avg_type$="WINDOW"
8560          BEEP
8565          INPUT "Enter the windowing period. (seconds)",W_period
8570          BEEP
8575          INPUT "Enter the window width. (seconds)",W_wdth
8580          BEEP
8585          INPUT "Enter the starting time (seconds)",Start_time
8590          BEEP
8595          INPUT "Enter the ending time (seconds)",End_time
8600      END SELECT
8605      !
8610      !           See if the user wishes to omit those breaths tagged
8615      !           as bad by the data calculation routine. These bad
8620      !           breaths are those with an inspiratory tidal volume
8625      !           or expiratory tidal volume below a specified volume.
8630      QS=""
8635      BEEP
8640      INPUT "Do you wish to omit the bad breaths? (Y/N)",QS
8645      IF QS="Y" OR QS="y" THEN
8650          Omit_bad=True
8655      ELSE
8660          Omit_bad=False
8665      END IF
8670      PRINT Formfd$
8675      IF Result_type$="PLOT" THEN
8680          GCLEAR
8685          GINIT
8690      !
8695      !           Prompt the user for the plots he wants.
8700      PRINT
8705      PRINT "Which of the following two respiratory variables"
8710      PRINT "do you wish to plot? Enter the number "
8715      PRINT "corresponding to the variable you wish."
8720      PRINT
8725      PRINT "  1. Oxygen consumed"
8730      PRINT "  2. Carbon dioxide produced"
8735      PRINT "  3. Aveolar oxygen consumption"
8740      PRINT "  4. Aveolar carbon dioxide production"
8745      PRINT "  5. Inspiratory Minute ventilation"
8750      PRINT "  6. Expiratory Minute ventilation"
8755      PRINT "  7. Inspiratory Tidal volume"
8760      PRINT "  8. Expiratory Tidal volume"
8765      PRINT "  9. Lung volume"
8770      PRINT " 10. Respiratory frequency"
8775      PRINT " 11. Respiratory quotient"
8780      REPEAT
8785          BEEP
8790          INPUT "Enter the first plot",Fig1
8795          IF Fig1<O2_cons OR Fig1>Resp_quotient THEN
8800              PRINT "Invalid response"
8805          END IF
8810      UNTIL Fig1>=O2_cons AND Fig1<=Resp_quotient
8815      REPEAT
8820          BEEP

```

```

8825         INPUT "Enter the second plot",Fig2
8830         IF Fig2<O2_cons OR Fig2>Resp_quotient THEN
8835             PRINT "Invalid response"
8840         END IF
8845         UNTIL Fig2>=O2_cons AND Fig2<=Resp_quotient
8850         Plot_dev$="CRT"           ! Set the default
8855         BEEP
8860         INPUT "OUTPUT ON PLOTTER OR CRT ? (PLOTTER/CRT)",Plot_dev$
8865         IF Plot_dev$="PLOTTER" THEN
8870             PRINT
8875             PRINT "Press CONTINUE when you have prepared the plotter"
8880             PAUSE
8885             PLOTTER IS 705,"HPGL"
8890             PRINTER IS 705
8895             PRINT "VS5;"
8900             PRINTER IS 1
8905             PEN 1
8910         ELSE
8915             DUMP DEVICE IS 701
8920         END IF
8925         PRINT Formfd$
8930         !
8935         !
8940         !
8945         !*****
8950         !           Determine the maximum and minimum values to be
8955         !           plotted. Allow for the user to define their own
8960         !           maximum and minimum value of R.
8965         !
8970         Max_min(Fig1,Avg_type$,Max1,Min1)
8975         IF ABS(Min1)<.001 THEN Min1=0
8980         Max_min(Fig2,Avg_type$,Max2,Min2)
8985         IF ABS(Min2)<.001 THEN Min2=0
8990         IF Fig1=Resp_quotient THEN
8995             BEEP
9000             INPUT "Enter min value of R or CONT for calculated min.",Mi
n1
9005             BEEP
9010             INPUT "Enter max value of R or CONT for calculated max.",Ma
x1
9015         END IF
9020         IF Fig2=Resp_quotient THEN
9025             BEEP
9030             INPUT "Enter min value of R or CONT for calculated min.",Mi
n2
9035             BEEP
9040             INPUT "Enter max value of R or CONT for calculated max.",Ma
x2
9045         END IF
9050         !
9055         !
9060         !
9065         !*****
9070         !           Plot the values.
9075         !
9080         !           Set up the plotting area, determine the starting and
9085         !           ending times, make the axes, and finally plot the values
9090         GRAPHICS ON
9095         View(0,100,58,100)
9100         !           ***** First Plot *****
9105         Make_axes(Fig1,Corr_flag,Min1,Max1)
9110         Plot_values(Fig1,Avg_type$)
9115         !           ***** Second Plot *****
9120         View(0,100,15,57)
9125         Make_axes(Fig2,Corr_flag,Min2,Max2)

```

```

9130      Plot_values(Fig2,Avg_type$)
9135      !
9140      !*****
9145      !      Title the plot and specify events
9150      !
9155      BEEP
9160      View(0,100,0,15)
9165      WINDOW 0,100,0,100
9170      CSIZE 3.5
9175      IF Avg_type$="AVERAGE" THEN
9180          Avg_bad_commt$=VAL$(No_b_avg)&" Breath(s)/point"
9185      ELSE
9190          Avg_bad_commt$=VAL$(W_period)&" s Window period; "
9195          Avg_bad_commt$=Avg_bad_commt$&VAL$(W_width)&"s Window width"
9200      END IF
9205      IF Omit_bad THEN
9210          Avg_bad_commt$=Avg_bad_commt$&" Bad breaths omitted"
9215      END IF
9220      LORG 6
9225      MOVE 50,98
9230      LABEL Avg_bad_commt$
9235      PENUP
9240      WAIT 1 ! Allow the user to look at the data a second.
9245      GRAPHICS OFF
9250      !
9255      !
9260      !      See if the user desires to define certain events.
9265      !
9270      QS=""
9275      BEEP
9280      INPUT "Do wish to define events on the plot? (Y/N)",QS
9285      IF QS="Y" OR QS="y" THEN
9290          BEEP
9295          INPUT "Enter the time of the first event.",Time1$
9300          BEEP
9305          INPUT "Enter the event occurring at the first time.",Event1$
9310          BEEP
9315          INPUT "Enter the time of the second event.",Time2$
9320          BEEP
9325          INPUT "Enter the event occurring at the second time.",Event2$
9330          LORG 3
9335          MOVE 10,78
9340          LABEL Time1$&": "&Event1$
9345          MOVE 10,60
9350          LABEL Time2$&": "&Event2$
9355          PENUP
9360      END IF
9365      CSIZE 5.5
9370      LORG 4
9375      MOVE 50,0
9380      BEEP
9385      INPUT "Enter a Title for this plot",Title$
9390      LABEL Title$&": "&Name$&": "&Date$
9395      PENUP
9400      PEN 0
9405      GRAPHICS ON
9410      PAUSE
9415      GRAPHICS OFF
9420      ELSE
9425          Print_results(Avg_type$)
9430      END IF
9435      !
9440      !
9445      BEEP

```

```

9450      QS=""
9455      INPUT "Do you wish to exit to the analysis routine? (Y/N)",QS
9460      UNTIL QS="Y" OR QS="y"
9465      GINIT
9470      SUBEND
9475      !
9480      !
9485      !

```

```

9490      SUB View(Left,Right,Bottom,Top)
9495      !*****
9500      !****                                     ****
9505      !****      Routine Title:      View                                     ****
9510      !****                                     ****
9515      !****      HP BASIC FILENAME: ANALYSIS                                     ****
9520      !****                                     ****
9525      !****      Department of Electrical and Computer Engineering,         ****
9530      !****      Kansas State University                                     ****
9535      !****                                     ****
9540      !****      Revision      Date      Programmer                                     ****
9545      !****      -----      -----      -----                                     ****
9550      !****      1.0      Sept. 10, 1984      Michael Masters                                     ****
9555      !****                                     ****
9560      !*****
9565      !****                                     ****
9570      !****      Purpose:                                     ****
9575      !****      This subroutine defines a viewport on the plotting ****
9580      !****      device. The total plotting area is made to be 100 by ****
9585      !****      100. By using this routine to define the VIEWPORT the ****
9590      !****      plots will have the same symetry independent of which ****
9595      !****      axis is longer.                                     ****
9600      !****                                     ****
9605      !****                                     ****
9610      !****                                     ****
9615      !****                                     ****
9620      !****      Routine(s) Called:      None                                     ****
9625      !****                                     ****
9630      !****      Parameters passed from the calling routine                                     ****
9635      !****                                     ****
9640      !****      Left - The location of the left edge of the plotting ****
9645      !****      window (0 to 100).                                     ****
9650      !****                                     ****
9655      !****      Right - The location of the right edge of the plotting ****
9660      !****      window (0 to 100 and larger than Left). ****
9665      !****                                     ****
9670      !****      Bottom - The location of the bottom edge of the ****
9675      !****      plotting window.                                     ****
9680      !****                                     ****
9685      !****      Top - The location of the Top edge of the plotting ****
9690      !****      window (0 to 100 and larger than Bottom). ****
9695      !****                                     ****
9700      !*****
9705      !*****
9710      IF RATIO>1 THEN
9715      VIEWPORT Left*Ratio,Right*Ratio,Bottom,Top
9720      ELSE
9725      VIEWPORT Left,Right,Bottom/Ratio,Top/Ratio
9730      END IF
9735      SUBEND
9740      !
9745      !
9750      !

```



```

9755 SUB Max_min(INTEGER Variable,Avg_type$,REAL Max,Min)
9760 !*****
9765 !*****
9770 !****
9775 !**** Routine Title: Compute maximum and minimum. ****
9780 !****
9785 !**** Revision      Date              Programmer ****
9790 !**** -----
9795 !****      1.0      January 1, 1985      Michael Masters ****
9800 !****
9805 !*****
9810 !****
9815 !**** Purpose: Determine the maximum and minimum values of the resp-****
9820 !**** iratory parameter being plotted. ****
9825 !****
9830 !**** Parameters passed from the calling routine ****
9835 !****
9840 !****      Variable - The parameter for which the maximum and min. ****
9845 !****      values are desired. ****
9850 !****
9855 !****      Avg_type$ - Contains the desired averaging technique. ****
9860 !****
9865 !****
9870 !**** Parameters returned to the calling routine ****
9875 !****
9880 !****      Max - The maximum averaged value. ****
9885 !****
9890 !****      Min - The minimum averaged value. ****
9895 !****
9900 !****
9905 !**** Routine(s) Called: ****
9910 !****      Avg_breath or Avg_window. ****
9915 !****
9920 !*****
9925 !*****
9930 COM /Anal_data8/ Resp_var(0:12,1:500)
9935 COM /Plot_resp_data1/ INTEGER Omit_bad,Num_breaths,No_b_avg
9940 COM /Plot_resp_data2/ Start_time,End_time,W_period,W_width
9945 INTEGER Br_pntr,Br_in_w_flag,Num_bad_breaths
9950 !
9955 ! Point to the first breath and initialize the maximum and minimum
9960 ! values.
9965 Br_pntr=1
9970 Min=999999999999.9
9975 Max=-999999999999.9
9980 IF Avg_type$="AVERAGE" THEN
9985 !
9990 ! Determine the maximum and minimum values of all the breaths or
9995 ! averaged breaths.
10000 REPEAT
10005 Avg_breath(Variable,Br_pntr,Time,Average,Num_bad_breaths)
10010 IF Average>Max THEN
10015 Max=Average
10020 END IF
10025 IF Average<Min THEN
10030 Min=Average
10035 END IF
10040 Br_pntr=Br_pntr+No_b_avg+Num_bad_breaths
10045 UNTIL Br_pntr>Num_breaths
10050 ELSE
10055 W_cntr=Start_time
10060 REPEAT
10065 Avg_window(Average,Br_in_w_flag,Variable,Br_pntr,W_cntr)

```



```

10070         IF Br_in_w_flag THEN
10075             IF Average>Max THEN
10080                 Max=Average
10085             END IF
10090             IF Average<Min THEN
10095                 Min=Average
10100             END IF
10105         END IF
10110         W_cntr=W_cntr+W_period
10115         UNTIL W_cntr>End_time
10120     END IF
10125 SUBEND
10130 !
10135 !
10140 !

10145 SUB Avg_breath(INTEGER Variable,Br_pntr,REAL Time,Average,INTEGER Num_b
ad_breaths)
10150 !*****
10155 !*****
10160 !****
10165 !**** Routine Title: Average breaths ****
10170 !****
10175 !**** Revision      Date              Programmer ****
10180 !**** -----      -----          ----- ****
10185 !****      1.0      January 1, 1985    Michael Masters ****
10190 !****
10195 !*****
10200 !****
10205 !**** Purpose: To average the breath-by-breath values of consec-****
10210 !**** utive breaths. Bad breaths may be omitted in the ****
10215 !**** average. ****
10220 !****
10225 !**** Parameters passed from the calling routine ****
10230 !****
10235 !**** Variable - The respiratory parameter being averaged. ****
10240 !****
10245 !**** Br_pntr - points to the initial breath to be averaged. ****
10250 !****
10255 !**** Num_bad_breaths - The number of breaths skipped because ****
10260 !**** they were a 'Bad Breath' ****
10265 !****
10270 !**** Parameters returned to the calling routine ****
10275 !****
10280 !**** Time - The time midway between the first breath ****
10285 !**** averaged and the last breath averaged. ****
10290 !****
10295 !**** Average-The average of the specified number of breaths ****
10300 !****
10305 !**** Routine(s) Called: None ****
10310 !****
10315 !*****
10320 !*****
10325 CCM /Anal_data3/ INTEGER Time_of_brth,O2_cons,Co2_prod,Insp_min_vent
10330 CCM /Anal_data5/ INTEGER Breath_good,Resp_quotient,Form_sd[1]
10335 CCM /Anal_data5a/ INTEGER Frc_o2_cons,Frc_co2_prod,Volume_of_lung
10340 CCM /Anal_data8/ Resp_var(0:12,1:500)
10345 CCM /Plot_resp_data1/ INTEGER Omit_bad,Num_breaths,No_b_avg
10350 INTEGER J,Pointer
10355 !
10360 !
10365 ! Sum up the specified number of breaths to determine the average
10370 ! value.

```

```

10375 Average=0
10380 J=0
10385 Num_badBreaths=0
10390 Pointer=Br_ptr
10395 WHILE J+1<=No_b_avg AND Pointer<=NumBreaths
10400 !
10405     IF Omit_bad THEN
10410         WHILE NOT (Resp_var(Breath_good,Pointer)) AND Pointer<=NumBreaths
10415             Num_badBreaths=Num_badBreaths+1
10420             Pointer=Br_ptr+J+Num_badBreaths
10425         END WHILE
10430     END IF
10435 !
10440 !
10445     Average=Average+Resp_var(Variable,Pointer)
10450     J=J+1
10455     Pointer=Br_ptr+J+Num_badBreaths
10460 END WHILE
10465 !
10470 !
10475 !     Determine the average and the time which is centered
10480 !     about the number of breaths which are averaged. The
10485 !     value of J is used rather than No_b_avg in the event
10490 !     the data array was exhausted before the specified number
10495 !     of breaths had been averaged.
10500 !
10505 Average=Average/J
10510 Time=(Resp_var(Time_of_brth,Br_ptr)+Resp_var(Time_of_brth,Pointer-1))/2
10515 SUBEND
10520 !
10525 !
10530 !
10535 !

```

```

10540 SUB Avg_window(Average,INTEGER Br_in_w_flag,Variable,Br_pntr,REAL W_cntr
r)
10545 !*****
10550 !*****
10555 !****
10560 !**** Routine Title: Average a time window. ****
10565 !**** . ****
10570 !**** Revision Date Programmer ****
10575 !**** -----
10580 !**** 1.0 January 1, 1985 Michael Masters ****
10585 !**** ****
10590 !*****
10595 !**** ****
10600 !**** Purpose: To compute the average of the breath-by-breath ****
10605 !**** values occurring in a time window. ****
10610 !**** ****
10615 !**** Parameters passed from the calling routine ****
10620 !**** ****
10625 !**** Variable - The respiratory parameter being averaged. ****
10630 !**** ****
10635 !**** Br_pntr - points to the initial breath to be averaged. ****
10640 !**** ****
10645 !**** W_cntr - the time which the widow is centered around. ****
10650 !**** ****
10655 !**** Parameters returned to the calling routine ****
10660 !**** ****
10665 !**** Average - The average of all breaths in the window. ****
10670 !**** ****
10675 !**** Br_in_w_flag - Set to true if the window did contain ****
10680 !**** data and set to false if it did not. ****
10685 !**** ****
10690 !**** Routine(s) Called: None ****
10695 !**** ****
10700 !*****
10705 !*****
10710 COM /Anal_data2/ INTEGER True,False
10715 COM /Anal_data3/ INTEGER Time_of_brth,O2_cons,Co2_prod,Insp_min_vent
10720 COM /Anal_data5/ INTEGER Breath_good,Resp_quotient,Form_fd$[1]
10725 COM /Anal_data5a/ INTEGER Frc_o2_cons,Frc_co2_prod,Volume_of_lung
10730 COM /Anal_data8/ Resp_var(0:12,1:500)
10735 COM /Plot_resp_data1/ INTEGER Omit_bad,Num_breaths,No_b_avg
10740 COM /Plot_resp_data2/ Start_time,End_time,W_period,W_wdth
10745 INTEGER Num_b_in_window,Fstbr_in_w_fnd
10750 !
10755 ! Find the first breath in the window.
10760 Left_edge_w=W_cntr-W_wdth/2
10765 REPEAT
10770 SELECT Resp_var(Time_of_brth,Br_pntr)
10775 CASE >=Left_edge_w
10780 ! Breath is right of the left window edge.
10785 IF Br_pntr=1 THEN
10790 Fstbr_in_w_fnd=True
10795 ELSE
10800 IF Resp_var(Time_of_brth,Br_pntr-1)<Left_edge_w THEN
10805 ! The first breath in the window has been found
10810 Fstbr_in_w_fnd=True
10815 ELSE
10820 Br_pntr=Br_pntr-1
10825 END IF
10830 END IF
10835 CASE <Left_edge_w
10840 ! Breath is left of the left window edge.
10845 Br_pntr=Br_pntr+1
10850 Fstbr_in_w_fnd=False
10855 END SELECT

```

```

10860 UNTIL Fstbr_in_w_fnd OR Br_pntr>Num_breaths
10865 !
10870 !
10875 Num_b_in_window=0
10880 Average=0
10885 WHILE Resp_var(Time_of_brth,Br_pntr)<W_cntr+W_wdth/2 AND Br_pntr<=Num_breaths
10890 !
10895 !           If the breath is not good and bad breaths are to be
10900 !           omitted do not include this breath, other wise include it.
10905 IF Qnit_bad AND NOT (Resp_var(Breath_good,Br_pntr)) THEN
10910 Br_pntr=Br_pntr+1
10915 ELSE
10920 Average=Average+Resp_var(Variable,Br_pntr)
10925 Br_pntr=Br_pntr+1
10930 Num_b_in_window=Num_b_in_window+1
10935 END IF
10940 END WHILE
10945 IF Num_b_in_window=0 THEN
10950 Br_in_w_flag=False
10955 ELSE
10960 Br_in_w_flag=True
10965 Average=Average/Num_b_in_window
10970 END IF
10975 SUBEND
10980 !
10985 !
10990 !

```

```

10995 SUB Make_axes(INTEGER Variable,Corr_flag,REAL Min,Max)
11000 !*****
11005 !*****
11010 !****
11015 !**** Routine Title: Make axes ****
11020 !****
11025 !**** Revision      Date      Programmer ****
11030 !**** -----      -----      ----- ****
11035 !****      1.0      January 1, 1985      Michael Masters ****
11040 !****
11045 !*****
11050 !****
11055 !**** Purpose: Used to draw the axes on the plotting device and ****
11060 !**** label plots for the breath-by-breath data. ****
11065 !****
11070 !**** Parameters passed from the calling routine ****
11075 !****
11080 !**** Variable - The parameter to be plotted; O2_cons, ****
11085 !**** Co2_prod,etc. ****
11090 !****
11095 !**** Corr_flag - Set to true if temperature and viscosity ****
11100 !**** corrections were used in analyzing the data. ****
11105 !****
11110 !**** Min - The minimum value of the parameter to be plotted ****
11115 !****
11120 !**** Max - The maximum value of the parameter to be plotted ****
11125 !****
11130 !****
11135 !**** Routine(s) Called: None ****
11140 !****
11145 !*****
11150 !*****
11155 !
11160 COM /Ana1_data3/ INTEGER Time_of_brth,O2_cons,Co2_prod,Insp_min_vent
11165 COM /Ana1_data4/ INTEGER Expr_min_vent,V_tid_insp,V_tid_expr,Resp_fr
eq
11170 COM /Ana1_data5/ INTEGER Breath_good,Resp_quotient,Form_fd$[1]
11175 COM /Ana1_data5a/ INTEGER Frc_o2_cons,Frc_co2_prod,Volume_of_lung
11180 COM /Plot_resp_data2/ Start_time,End_time,W_period,W_width
11185 DIM Heading$(1:11)[30]
11190 !
11195 !
11200 !
11205 ! Define the individual plot titles.
11210 Heading$(O2_cons)="Minute O2 Consumption"
11215 Heading$(Co2_prod)="Minute CO2 Production"
11220 Heading$(Frc_o2_cons)="Aveolar Minute O2 Consumption"
11225 Heading$(Frc_co2_prod)="Aveolar Minute CO2 Production"
11230 Heading$(Insp_min_vent)="Inspiratory Minute Ventilation"
11235 Heading$(Expr_min_vent)="Expiratory Minute Ventilation"
11240 Heading$(V_tid_insp)="Inspiratory Tidal Volume"
11245 Heading$(V_tid_expr)="Expiratory Tidal Volume"
11250 Heading$(Volume_of_lung)="Lung Volume"
11255 Heading$(Resp_freq)="Respiratory Frequency"
11260 Heading$(Resp_quotient)="Respiratory Quotient"
11265 !
11270 !
11275 !
11280 ! Define the plotting area and make the axes.
11285 Top=Max+.2*(Max-Min)
11290 Bottom=Min-.26*(Max-Min)
11295 Left=Start_time-.1*(End_time-Start_time)
11300 Right=End_time+.05*(End_time-Start_time)
11305 FRAME
11310 WINDOW Left,Right,Bottom,Top

```

```

11315 CLIP Start_time,End_time,Min,Max
11320 Xtick=(Start_time-End_time)/10
11325 Ytick=(Max-Min)/4
11330 AXES Xtick,Ytick,Start_time,Min
11335 !
11340 ! Label the time axis.
11345 CLIP Left,Right,Bottom,Top
11350 LORG 6
11355 CSIZE 3
11360 FOR X=Start_time TO 1.05*End_time STEP (End_time-Start_time)/5
11365 MOVE X,Min-(Max-Min)/75
11370 LABEL DROUND(X,3)
11375 NEXT X
11380 LORG 4
11385 MOVE (Start_time+End_time)/2,Bottom
11390 LABEL "Data collection Time (seconds)"
11395 !
11400 ! Label the axis of the dependent variable
11405 LORG 8
11410 FOR Y=Min TO 1.05*Max STEP (Max-Min)/4
11415 MOVE Start_time,Y
11420 LABEL DROUND(Y,3)
11425 NEXT Y
11430 IF Variable=Resp_quotient THEN
11435 MOVE Start_time,1
11440 DRAW End_time,1
11445 END IF
11450 !
11455 ! Put the appropriate units on the dependent axis.
11460 LORG 3
11465 MOVE Left,Top
11470 SELECT Variable
11475 CASE =Resp_freq
11480 LABEL " BrPM"
11485 CASE =V_tid_insp,=V_tid_expr,=Volume_of_lung
11490 IF Corr_flag THEN
11495 LABEL " Liters (BTPS)"
11500 ELSE
11505 LABEL " Liters"
11510 END IF
11515 CASE =Insp_min_vent,=Expr_min_vent
11520 IF Corr_flag THEN
11525 LABEL " L/Min (BTPS)"
11530 ELSE
11535 LABEL " L/Min"
11540 END IF
11545 CASE =O2_cons,=Co2_prod,=Frc_o2_cons,=Frc_co2_prod
11550 IF Corr_flag THEN
11555 LABEL " L/Min (STPD)"
11560 ELSE
11565 LABEL " L/Min"
11570 END IF
11575 CASE =Resp_quotient
11580 ! Respiratory quotient is unitless.
11585 END SELECT
11590 !
11595 !
11600 ! Label the plot.
11605 !
11610 MOVE End_time,Top
11615 LORG 9
11620 CSIZE 4
11625 LABEL Heading$(Variable)&" .vs. Time"
11630 CLIP Start_time,End_time,Min,Max
11635 SUBEND

```

```

11640 !
11645 !
11650 !
11655 !

11660 SUB Plot_values(INTEGER Variable,Avg_type$)
11665 !*****
11670 !*****
11675 !****
11680 !**** Routine Title: Plot breath-by-breath data. ****
11685 !****
11690 !**** Revision      Date              Programmer ****
11695 !**** -----      -              - ****
11700 !**** 1.0          January 1, 1985   Michael Masters ****
11705 !****
11710 !*****
11715 !****
11720 !**** Purpose: To plot the breath by breath data using the ****
11725 !**** specified averaging technique. ****
11730 !****
11735 !**** Parameters passed from the calling routine ****
11740 !****
11745 !**** Variable - The parameter to be plotted. ****
11750 !****
11755 !**** Avg_type$ - Contains the desired averaging technique. ****
11760 !****
11765 !**** Parameters returned to the calling routine ****
11770 !**** None ****
11775 !****
11780 !**** Routine(s) Called: ****
11785 !**** Avg_breath or Avg_window ****
11790 !****
11795 !*****
11800 !*****
11805 !
11810 COM /Anal_data8/ Resp_var(0:12,1:500)
11815 COM /Plot_resp_data1/ INTEGER Omit_bad,Num_breaths,No_b_avg
11820 COM /Plot_resp_data2/ Start_time,End_time,W_period,W_width
11825 INTEGER Br_pntr,Br_in_w_flag,Num_bad_breaths
11830 LOG 5
11835 CSIZE 1.5
11840 Br_pntr=1
11845 IF Avg_type$="AVERAGE" THEN
11850 REPEAT
11855 Avg_breath(Variable,Br_pntr,Time,Average,Num_bad_breaths)
11860 MOVE Time,Average
11865 LABEL "O"
11870 Br_pntr=Br_pntr+No_b_avg+Num_bad_breaths
11875 UNTIL Br_pntr>Num_breaths
11880 ELSE
11885 W_cntr=Start_time
11890 REPEAT
11895 Avg_window(Average,Br_in_w_flag,Variable,Br_pntr,W_cntr)
11900 IF Br_in_w_flag THEN
11905 MOVE W_cntr,Average
11910 LABEL "O"
11915 END IF
11920 W_cntr=W_cntr+W_period
11925 UNTIL W_cntr>End_time
11930 END IF
11935 SUBEND
11940 !
11945 !

```



```

11950 SUB Print_results(Avg_type$)
11955 ! *****
11960 ! *****
11965 ! ****
11970 ! **** Routine Title: Print breath-by-breath data. ****
11975 ! ****
11980 ! **** Revision Date Programmer ****
11985 ! **** -----
11990 ! **** 1.0 January 1, 1985 Michael Masters ****
11995 ! ****
12000 ! *****
12005 ! ****
12010 ! **** Purpose: To print the breath by breath data using the ****
12015 ! **** specified averaging technique. ****
12020 ! ****
12025 ! **** Parameters passed from the calling routine ****
12030 ! ****
12035 ! **** Avg_type$ - Contains the desired averaging technique. ****
12040 ! ****
12045 ! **** Parameters returned to the calling routine ****
12050 ! **** None ****
12055 ! ****
12060 ! **** Routine(s) Called: ****
12065 ! **** Avg_breath or Avg_window ****
12070 ! ****
12075 ! *****
12080 ! *****
12085 COM /Anal_data3/ INTEGER Time_of_brth,O2_cons,Co2_prod,Insp_min_vent
12090 COM /Anal_data4/ INTEGER Expr_min_vent,V_tid_insp,V_tid_expr,Resp_fr
eq
12095 COM /Anal_data5/ INTEGER Breath_good,Resp_quotient,Formfds[1]
12100 COM /Anal_data5a/ INTEGER Frc_o2_cons,Frc_co2_prod,Volume_of_lung
12105 COM /Anal_data6/ INTEGER Corr_flag,REAL Room_fh2o,T
12110 COM /Anal_data8/ Resp_var(0:12,1:500)
12115 COM /Anal_data9/ Name$(25),Comment$(46)
12120 COM /Cal_data1/ Cal$(10),Date$(25)
12125 COM /Plot_resp_data1/ INTEGER Omit_bad,Num_breaths,No_b_avg
12130 COM /Plot_resp_data2/ Start_time,End_time,W_period,W_wdth
12135 DIM Values(1:11)
12140 INTEGER Br_pntr,Br_index,Br_in_w_flag,I,Some_rs_to_big,Num_bad_breat
hs
12145 Some_rs_to_big=(1=0)
12150 !
12155 !
12160 PRINTER IS 9
12165 PRINT USING "K,K,/";"Date: ",Date$
12170 PRINT USING "K,K,/";"Comment: ",Comment$
12175 PRINT USING "K,K,/";"Subject identifier: ",Name$
12180 IF Avg_type$="AVERAGE" THEN
12185 IF No_b_avg=1 THEN
12190 PRINT USING "K";"The individual breath-by-breath values are sh
own."
12195 ELSE
12200 PRINT USING "K,K,/";"The number of breaths averaged is ",No_b_
avg
12205 PRINT USING "#,K,K";"The breaths are combined by AVERAGING. "
,No_b_avg
12210 PRINT USING "K,2,/";" successive breaths are averaged together.
"
12215 END IF
12220 ELSE
12225 PRINT USING "K,DDDD.D,K,/";"The window period is ",W_period," sec

```



```

onds"
12230 PRINT USING "K,DDDD.D,K,/";"The window width is ",W_width," second
ds"
12235 PRINT USING "K,K,K";"The starting time is ",Start_time," seconds"
12240 PRINT USING "K,K,K,/";"The ending time is ",End_time," seconds"
12245 PRINT USING "#,K";"The breaths are combined by WINDOWING. The br
eaths occurring"
12250 PRINT USING "K,K,K";" in a window ",W_width," second(s) wide are a
veraged."
12255 PRINT USING "#,K,K";"The center of the window is moved ",W_period
12260 PRINT USING "K,K";" seconds between successive averages. The cente
r of the"
12265 PRINT USING "#,K,K";"first window is ",Start_time
12270 PRINT USING "K,K,K,2/";" seconds and the ending time is ",End_tim
e," seconds."
12275 END IF
12280 IF Omit_bad THEN
12285 PRINT " * BAD BREATHS OMITTED *"
12290 PRINT USING "#,K";"The bad breaths are not included in the averag
ing technique."
12295 PRINT USING "K";" Bad breaths are those breaths with"
12300 PRINT USING "#,K";"an inspiratory volume or an expiratory"
12305 PRINT USING "K,2/";" volume of less than 0.4 Liters."
12310 END IF
12315 PRINT USING "#,K";"The R' value is equal to the averaged CO2 produce
d value "
12320 PRINT USING "K";"divided by the averaged O2 consumed value. It is"
12325 PRINT USING "#,K";"a better estimate of the true R value for the bre
aths "
12330 PRINT USING "K,2/";"averaged than the average of the individual R va
lues."
12335 PRINT "
12340 PRINT USING "#,K";"
| Alveolar | Alveolar |
| Resp. | | O2 | CO2 | O2 | CO2
12345 PRINT USING "K";" Averaged | Ventilation | Tidal Volume | Resp.
|
12350 PRINT USING "#,K";" | Time | Consumed | Produced | Consumed | Produce
d | Quotient |"
12355 PRINT USING "K";"CO2/O2 :R' | Insp. | Expr. | Insp. | Expr. | Freq.
| Lung
12360 PRINT USING "#,K";" | (sec) | (L/min) | (L/min) | (L/min) | (L/min) |
12365 PRINT USING "K";" | (L/min) | (L/min) | (L) | (L) | (br/min)
| Vol. (L) |"
12370 IF Corr_flag THEN
12375 PRINT USING "#,K";" | | (STPD) | (STPD) | (STPD) | (ST
PD) |
12380 PRINT USING "K";" | (BTPS) | (BTPS) | (BTPS) | (BTPS) |
| (BTPS) |"
12385 END IF
12390 PRINT USING "#,K";" | | | | |
| | | | |
12395 PRINT USING "K";" | | | | |
| | | | |
12400 Br_pntr=1
12405 IF Avg_type$="AVERAGE" THEN
12410 REPEAT
12415 FOR I=O2_cons TO Resp_quotient
12420 Avg_breath(I,Br_pntr,Time,Average,Num_bad_breaths)
12425 Values(I)=Average
12430 NEXT I
12435 PRINT USING "#,K,4D.D,K";" | Time, " |"
12440 GOSUB Print_line
12445 Br_pntr=Br_pntr+No_b_avg+Num_bad_breaths
12450 -- UNTIL Br_pntr>Num_breaths
12455 ELSE

```

```

12460      W_cntr=Start_time
12465      REPEAT
12470          FOR I=O2_cons TO Resp_quotient
12475              Br_index=Br_pntr
12480              Avg_window(Average,Br_in_wflag,I,Br_index,W_cntr)
12485              Values(I)=Average
12490          NEXT I
12495          Br_pntr=Br_index
12500          PRINT USING "#,K,DDDD.D,K";"I",W_cntr,"I"
12505          IF Br_in_wflag THEN
12510              GOSUB Print_line
12515          ELSE
12520              PRINT "      ****      The window did not contain any breaths
12525          END IF
12530          W_cntr=W_cntr+W_period
12535      UNTIL W_cntr>End_time
12540      END IF
12545      PRINT USING "#,K";"I"
12550      PRINT USING "K";"
12555      IF Some_rs_to_big THEN
12560          PRINT
12565          PRINT USING "#,K";"
12570          PRINT USING "K";"***.*** The averaged R value was larger than 99.9
12575      END IF
12580      PRINT USING "#,2/"
12585      PRINTER IS 1
12590      SUBEXIT
12595      Print_line: !
12600      PRINT USING "#,K,DD.3D,K";" ",Values(O2_cons)," I"
12605      PRINT USING "#,K,DD.3D,K";" ",Values(Co2_prod)," I"
12610      PRINT USING "#,K,DD.3D,K";" ",Values(Frc_o2_cons)," I"
12615      PRINT USING "#,K,DD.3D,K";" ",Values(Frc_co2_prod)," I"
12620      !
12625      IF Values(Resp_quotient)<100 THEN
12630          PRINT USING "#,K,DD.3D,K";" ",Values(Resp_quotient)," I"
12635      ELSE
12640          PRINT USING "#,K";" **.* ** I"
12645          Same_rs_to_big=(1=1)
12650      END IF
12655      !
12660      IF ABS(Values(Co2_prod)/Values(O2_cons))<100 THEN
12665          PRINT USING "#,K,DD.3D,K";" ",ABS(Values(Co2_prod)/Values(O2_con
12670      ELSE
12675          PRINT USING "#,K";" **.* ** I"
12680          Same_rs_to_big=(1=1)
12685      END IF
12690      !
12695      PRINT USING "#,K,3D.DD,K";" ",Values(Insp_min_vent)," I"
12700      PRINT USING "#,K,3D.DD,K";" ",Values(Expr_min_vent)," I"
12705      PRINT USING "#,K,DD.DD,K";" ",Values(V_ttid_insp)," I"
12710      PRINT USING "#,K,DD.DD,K";" ",Values(V_ttid_expr)," I"
12715      PRINT USING "#,K,3D.2D,K";" ",Values(Resp_freq)," I"
12720      PRINT USING "#,K,DD.3D,K";" ",Values(Volume_of_lung)," I"
12725      PRINT
12730      RETURN
12735      SUBEND
12740      !
12745      !
12750      !

```

```

12755 SUB Expanded_dump
12760 !*****
12765 !*****
12770 !****
12775 !**** Function Title: Expanded graphics dump. ****
12780 !****
12785 !**** Revision      Date              Programmer ****
12790 !**** -----
12795 !****      1.0      March 1,1985      Michael Masters ****
12800 !****
12805 !*****
12810 !****
12815 !**** Purpose: To dump the screen to the printer and expand the ****
12820 !**** size by 4 to 1. Simply use the command ****
12825 !****
12830 !**** CALL Expanded_dump ****
12835 !**** This command is keyboard executable. ****
12840 !****
12845 !**** Parameters passed from the calling routine ****
12850 !**** None ****
12855 !****
12860 !*****
12865 !*****
12870 GRAPHICS OFF
12875 PRINT "ADJUST THE THERMAL PAPER TO THE TOP OF THE PAGE"
12880 PRINT "AND PRESS CONTINUE."
12885 BEEP
12890 PAUSE
12895 PRINT CHR$(12)
12900 GRAPHICS ON
12905 DUMP DEVICE IS 701,EXPANDED ! Set to the expanded mode
12910 !
12915 ! Adjust the right side of the paper so that the figure
12920 ! will fit on the page
12925 PRINTER IS 701
12930 PRINT CHR$(27)&"*r70xA"
12935 PRINTER IS 1
12940 DUMP GRAPHICS
12945 !
12950 ! Readjust the right side of the paper so that the normal
12955 ! dumps are centered on the page.
12960 PRINTER IS 701
12965 PRINT CHR$(27)&"*r175xA"
12970 DUMP DEVICE IS 701
12975 PRINTER IS 1
12980 BEEP
12985 SUBEND

```

A7.7 STOREHR: a Basic Program Which Stores the Heart Rate Values

The STOREHR program is used to store the subjects experimental heart rate data in a file compatible with Sprick's plotting program [16]. The data are entered by the operator. Once entered the operator has the opportunity to review the data and make any necessary corrections.

A7.7.1 The Main Routine of STOREHR

The main routine provides the operator prompts necessary to obtain the heart rate data. The data are stored in the file format specified by Sprick [16]. This format is necessary in order to use Sprick's plotting routine.

Common Blocks Used by the Subroutine

None

Variable definitions

- Heart_rate - a real array which contains the heart rate data.
- I - a real variable used in conjunction with the variable J as a pointer into the Heat_rate array.
- J - a real variable used in conjunction with the variable I as a pointer into the Heat_rate array.
- Name\$ - a string variable equal to an operator defined file name. The heart rate data are stored in the file specified by Name\$.
- Pointer - a real variable used as a pointer into the Heart_rate array.
- Q\$ - a string variable used to obtain the operator's response to a question.
- True - a real variable used as the Boolean value of true.
- Value - a real variable used as a pointer into the Heart_rate array.

A7.7.2 Load autost Subroutine

The Load_autost subroutine loads the AUTOST (A7.3) program into memory. The AUTOST program begins execution once loaded.

Common Blocks Used by the Subroutine

None

Variables passed to the procedures

None

Variables returned by the procedures

None

A7.7.3 Load_plot Subroutine

The Load_plot subroutine loads the PLOT program developed by Sprick [16] into memory. The PLOT program begins execution once loaded.

Common Blocks Used by the Subroutine

None

Variables passed to the procedures

None

Variables returned by the procedures

None

A7.7.4 Options Subroutine

The Options subroutine presents the operator with the options which may be taken once the data have been entered and stored. These options give the operator the ability to load the AUTOST program, load the PLOT program, or store additional heart rate data.

Common Blocks Used by the Subroutine

None

Variables passed to the procedures

None

Variables returned by the procedures

None

A7.7.5 STOREHR Program Listing

```

10 | *****
20 | *****
30 | ****
40 |**** Routine Title:      Store Heart Rate      ***
50 |****
60 |**** HP BASIC FILENAME:  STOREHR                ***
70 |****
80 |**** Department of Electrical and Computer Engineering ***
90 |**** Kansas State University                    ***
100 |****
110 |**** Revision      Date              Programmer    ***
120 |**** -----      -
130 |****      1.0      August 20, 1984      Michael Masters ***
140 |****
150 | *****
160 | ****
170 |**** Purpose:  To store the heart rate of the subject as recorded ***
180 |****           by the heart rate monitor.  The heart rate is      ***
190 |****           for each 30 second interval.                      ***
200 |****
210 | *****
220 GCLEAR
230 CALL Options
240 PRINT CHR$(12)
250 PRINT "*****"
260 PRINT "*"
270 PRINT "*"
280 PRINT "*"          Save the heart Rate          "*"
290 PRINT "*"
300 PRINT "*"
310 PRINT "*****"
320 DIM Heart_rate(1:50)
330 PRINT
340 PRINT
350 PRINT "Enter the file name.  The file will be stored on"
360 PRINT "the data disk in a format which can be read by"
370 PRINT "the PLOT routine."
380 BEEP
390 INPUT "Enter the name of the Heart Rate file",Name$
400 True=(1=1)
410 Pointer=0
420 PRINT CHR$(12)
430 PRINT
440 PRINT
450 PRINT "Enter the heart rate for each 30 second interval."
460 PRINT
470 PRINT "If you have entered all heart rate values;"
480 PRINT "  Enter a negative number in response to the"
490 PRINT "  'Enter the Heart Rate' prompt."
500 PRINT
510 PRINT "You will be given an opportunity to correct any"
520 PRINT "mistakes at a latter time."
530 REPEAT
540   Pointer=Pointer+1
550   PRINT TABXY(1,24),"
560   PRINT TABXY(1,24),"Enter the heart rate for the time, t=";(Pointer-
570 1)*.5;" min."
570   BEEP
580   INPUT Heart_rate(Pointer)
590   UNTIL Heart_rate(Pointer)<0
600   Pointer=Pointer-1
610   FOR J=1 TO Pointer STEP 10

```

```

620 Print_values:True=(1=1)
630     I=0
640     PRINT CHR$(12)
650     PRINT
660     PRINT
670     PRINT "Value      Time      Heart Rate"
680     WHILE True
690         IF I+J<=Pointer AND I<10 THEN
700             PRINT USING "X,DD,7X,DD.D,8X,DDDD";I+J;(I+J-
1)*.5;Heart_rate(I+J)
710         ELSE
720             True=(1=0)
730         END IF
740         I=I+1
750     END WHILE
760     QS="N"
770     BEEP
780 Change:INPUT "Do you wish to change any of these values? (Y/N)",QS
790     IF QS<>"N" AND QS<>"n" AND QS<>"y" AND QS<>"Y" THEN Change
800     IF QS="y" OR QS="Y" THEN
810         Value=0
820         BEEP
830         INPUT "Which value do you wish to change?",Value
840         IF Value<>0 THEN
850             BEEP
860             INPUT "Enter the new value.",Heart_rate(Value)
870             GOTO Print_values
880         END IF
890     END IF
900     QS=""
910 NEXT J
920     !
930     !
940     ! Store the heart rate values.
950     !
960     PRINT CHR$(12)
970     PRINT
980     PRINT
990     PRINT "Storing the values"
1000    CREATE BDAT Name&&:"HP9895,700",Pointer*8/256+1
1010    ASSIGN @Path1 TO Name&&:"HP9895,700"
1020    ON END @Path1 GOTO 1050
1030    OUTPUT @Path1;Pointer
1040    OUTPUT @Path1;Heart_rate(*)
1050    !
1060    !
1070    PRINT CHR$(12)
1080    PRINT
1090    PRINT "You may obtain a plot of these values using"
1100    PRINT "Sprick's PLOT routine. To obtain a plot answer"
1110    PRINT "Y to the next question"
1120    QS="N"
1130    BEEP
1140    INPUT "Would you like to plot the values? (Y/N)",QS
1150    SELECT QS
1160    CASE ="Y",="y"
1170        PRINT CHR$(12)
1180        PRINT
1190        PRINT
1200        PRINT "When instructed by PLOT to enter the X axis label,"
1210        PRINT "enter TIME using capital letters"
1220        PRINT
1230        PRINT "Press CONTINUE when you are ready to proceed."
1240        PAUSE
1250        PRINT CHR$(12)

```

```
1260     PRINT
1270     PRINT "      Now loading PLOT"
1280     CALL Load_plot
1290     CASE ="N",="n"
1300     PRINT CHR$(12)
1310     PRINT
1320     PRINT "Program run complete"
1330     CASE ELSE
1340     GOTO 1120
1350     END SELECT
1360     CALL Options
1370     END
1380     SUB Options
1390     Keys: !
1400     ON KEY 1 LABEL "PLOT" CALL Load_plot
1410     ON KEY 4 LABEL "STOREHR" GOTO End
1420     ON KEY 9 LABEL "EXIT" CALL Load_autost
1430     GOTO Keys
1440     !
1450     !
1460     End:SUBEND
1470     SUB Load_plot
1480     OFF KEY
1490     MASS STORAGE IS ":HP9895,700,0"
1500     LOAD "PLOT:HP9895,702,3",1
1510     SUBEND
1520     SUB Load_autost
1530     OFF KEY
1540     LOAD "AUTOST:INTERNAL"
1550     SUBEND
```


A7.8 TXDCR_VALS: a Basic Program Which Computes the Component Values of the Temperature Transducer

The TXDCR_VALS program aids in the determination of the component values of the temperature transducer. The operator defines the input temperature range and the desired output voltage range. Also, the operator must define a value for the V_r , R_s , R_f , and R_c . With the range information and the defined components the necessary values of R_g , R_t , and R_r are computed. The operator can experiment with different ranges and values of the defined components to see the effect on the calculated components. The program may also generate an output voltage versus temperature table.

A7.8.1 The Main Routine of TXDCR_VALS

The main routine of TXDCR_VALS provides the main control of the program. Most operator input is accomplished via the various subroutines.

Variable definitions

- R_c - a real variable equal to the value of the R_c .
- R_f - a real variable equal to the value of the R_f .
- R_s - a real variable equal to the value of the R_s .
- $T_{ambient}$ - a real variable equal to the average ambient temperature.
- T_{max} - a real variable equal to the maximum temperature the transducer is to measure.
- T_{min} - a real variable equal to the minimum temperature the transducer is to measure.
- V_{max} - a real variable equal to the output voltage corresponding to a temperature equal to T_{max} .
- V_{min} - a real variable equal to the output voltage corresponding to a temperature equal to T_{min} .
- V_r - a real variable equal to the reference voltage.

A7.8.2 Enter_rfr Subroutine

The Enter_rfr subroutine is used to prompt the operator for the value of the resistors R_f and R_c .

Variables passed to the procedures

None

Variables returned by the procedures

Rc - real.

Rf - real.

Variable definitionsRc - a real variable equal to the operator defined value of R_C .Rf - a real variable equal to the operator defined value of R_F .A7.8.3 Enter_rs Subroutine

The Enter_rs subroutine is used to prompt the operator for the value of the resistor R_S .

Variables passed to the procedures

None

Variables returned by the procedures

Rs - real.

Variable definitionsRs - a real variable equal to the operator defined value of R_S .A7.8.4 Print Subroutine

The Print subroutine prints the values to transducer components. The subroutine computes the values of all components which have not been defined.

Variables passed to the procedures

None

Variables returned by the procedures

None

Variable definitions

K1 - a real variable equal to the gain of the pre-amplifier.

K2 - a real variable equal to the gain of the instrumentation amplifier.

Rc - a real variable equal to the operator defined value of

- R_c -
- Rf - a real variable equal to the operator defined value of R_f .
- Rg - a real variable equal to the calculated value of R_g .
- Rr - a real variable equal to the calculated value of R_r .
- Rs - a real variable equal to the operator defined value of R_s .
- Rt - a real variable equal to the calculated value of R_t .
- T_vcomp0 - a real variable equal to the temperature corresponding to a compensation voltage of zero.
- Tambient - a real variable equal to the average ambient temperature.
- Tmax - a real variable equal to the maximum temperature the transducer is to measure.
- Tmin - a real variable equal to the minimum temperature the transducer is to measure.
- Tot_gain - a real variable equal to the total gain of the transducer.
- Vcomp_ta - a real variable equal to the compensation voltage corresponding to the ambient temperature.
- Va - a real variable equal to the second order coefficient of the second order function relating the thermocouple voltage to the sensing junction temperature.
- Vb - a real variable equal to the first order coefficient of the second order function relating the thermocouple voltage to the sensing junction temperature.
- Vmax - a real variable equal to the output voltage corresponding to a temperature equal to Tmax.
- Vmin - a real variable equal to the output voltage corresponding to a temperature equal to Tmin.
- Vr - a real variable equal to the reference voltage.
- Vr_over_rr - a real variable equal to the reference voltage divided by the reference resistor (R_r).

A7.8.5 Print_results Subroutine

The Print_results subroutine prints a table of the transducer output voltage versus the thermocouple temperature. The subroutine uses the calculated component values to determine the output voltage.

Variables passed to the procedures

None

Variables returned by the procedures

None

Variable definitions

- A - a real variable used as a pointer into the Printer array.
- I - a real variable used as a loop counter.
- J - a real variable used as a loop counter.
- Printer - a real array of three elements. The elements contain the specification of the CRT, the thermal printer, and the DECwriter printer.
- Rr - a real variable equal to the calculated value of R_r .
- Rs - a real variable equal to the operator defined value of R_s .
- Rt - a real variable equal to the calculated value of R_t .
- Tambient - a real variable equal to the average ambient temperature.
- Temp - a real variable equal to the temperature value for which the output voltage is computed.
- Tmax - a real variable equal to the maximum temperature the transducer is to measure.
- Tmin - a real variable equal to the minimum temperature the transducer is to measure.
- Tot_gain - a real variable equal to the total gain of the transducer.
- Vout - a real variable equal to the output voltage corresponding to a temperature equal to Temp.
- Vr - a real variable equal to the reference voltage.

A7.8.6 Txdcr_range Subroutine

The Txdcr_range subroutine prompts the operator for the temperature range the transducer will measure, the output voltage corresponding to the temperature range, and the ambient temperature.

Variables passed to the procedures

None

Variables returned by the procedures

Tambient - real.

Tmax - real.

Tmin - real.

Vmax - real.

Vmin - real.

Variable definitions

Tambient - a real variable equal to the average ambient temperature.

Tmax - a real variable equal to the maximum temperature the transducer is to measure.

Tmin - a real variable equal to the minimum temperature the transducer is to measure.

Vmax - a real variable equal to the output voltage corresponding to a temperature equal to Tmax.

Vmin - a real variable equal to the output voltage corresponding to a temperature equal to Tmin.

A7.8.7 Vr Subroutine

The Vr subroutine is used to prompt the operator for the value of the voltage reference V_r .

Variables passed to the procedures

None

Variables returned by the procedures

Vr - real.

Variable definitions

Vr - a real variable equal to the operator defined value of V_r .

A7.8.8 Vtc Function

The Vtc function calculates the thermocouple voltage corresponding to the specified sensing junction temperature and a specified reference junction temperature.

Variables passed to the procedures

Tj - real.

Tref - real.

Variable definitions

Tj - a real variable equal to the sensing junction temperature.

Tref - a real variable equal to the reference junction temperature.

Va - a real variable equal to the second order coefficient of the second order function relating the thermocouple voltage to the sensing junction temperature.

Vb - a real variable equal to the first order coefficient of the second order function relating the thermocouple voltage to the sensing junction temperature.

Vc - a real variable equal to the zero order coefficient of the second order function relating the thermocouple voltage to the sensing junction temperature.

Vtc - a real variable equal to the thermocouple voltage corresponding to a sensing junction temperature of Tj and a reference junction temperature of Tref.

A7.8.9 TXDCR_VALS Program Listing

```

10  !*****
20  !*****
30  !***
40  !*** Routine Title:      TXDCR_VALS
50  !***
60  !*** HP BASIC FILENAME: TXDCR_VALS
70  !***
80  !*** Department of Electrical and Computer Engineering
90  !*** Kansas State University
100 !***
110 !*** Revision      Date              Programmer
120 !*** -----
130 !***      1.0      June 4, 1983      Michael Masters
140 !***      2.0      January 30, 1985  Micheal Masters
150 !***
160 !*****
170 !***
180 !*** Purpose:
190 !***      To calculate the component values of the respiratory
200 !***      temperature transducer.
210 !***
220 !*****
230 COM Tmax,Tmin,Vmax,Vmin,Tambient,Rs,Rg,Rc,Rf,Vr,Rt,Rr,Tot_gain
240 PRINTER IS 1
250 CALL Txdcr_range(Tmax,Tmin,Vmax,Vmin,Tambient)
260 CALL Enter_rfrf(Rf,Rc)
270 CALL Enter_rs(Rs)
280 CALL Vr(Vr)
290 CALL Print
300 Define_keys: !
310 !
320 !      ***** Define the special function keys *****
330 ON KEY 2 LABEL "Print" GOTO Print_results
340 ON KEY 5 LABEL "Range" GOTO Txdcr_range
350 ON KEY 6 LABEL "Rf & Rc" GOTO Enter_rfrf
360 ON KEY 7 LABEL "Rs" GOTO Enter_rs
370 ON KEY 8 LABEL "Vr" GOTO Vr
380 ON KEY 9 LABEL "EXIT" GOTO Quit
390 Do_nothing:GOTO Do_nothing
400 !
410 !
420 Txdcr_range: !
430 !-----
440 ! Define the temperature range to be measured, the minimum and maximum
450 ! voltage output, and the average ambient temperature.
460 OFF KEY
470 CALL Txdcr_range(Tmax,Tmin,Vmax,Vmin,Tambient)
480 CALL Print
490 GOTO Define_keys
500 !
510 !
520 Enter_rfrf: !
530 !-----
540 ! Enter the values of the resistors Rf and Rc which develop the gain K1.
550 !
560 OFF KEY
570 CALL Enter_rfrf(Rf,Rc)
580 CALL Print
590 GOTO Define_keys
600 !
610 !
620 Enter_rs: !

```

```

630 !-----
640 !   Enter the value of the resistor Rs.
650 !
660 OFF KEY
670 CALL Enter_rs(Rs)
680 CALL Print
690 GOTO Define_keys
700 !
710 !
720 Vr:!!
730 !-----
740 !   Enter the value of the referenc voltage.
750 !
760 OFF KEY
770 CALL Vr(Vr)
780 CALL Print
790 GOTO Define_keys
800 !
810 !
820 Print_results:!!
830 !-----
840 !   Enter the value of the referenc voltage.
850 !
860 OFF KEY
870 PRINTER IS 1
880 CALL Print_results
890 GOTO Define_keys
900 !
910 !
920 !
930 Quit: !
940 !-----
950 !   Exit the program.
960 !
970 BEEP
980 PRINT "PROGRAM RUN COMPLETE"
990 END
1000 !
1010 !
1020 SUB Txdcr_range(Tmax,Tmin,Vmax,Vmin,Tambient)
1030 !
1040 ! define the temperature range, output voltage, and ambient temperature.
1050 !
1060     INPUT "ENTER THE MINIMUM TEMPERATURE TO BE MEASURED",Tmin
1070     INPUT "ENTER THE MAXIMUM TEMPERATURE TO BE MEASURED",Tmax
1080     INPUT "ENTER VOLTAGE CORRESPONDING TO Tmin",Vmin
1090     INPUT "ENTER VOLTAGE CORRESPONDING TO Tmax",Vmax
1100     INPUT "ENTER THE AVERAGE AMBIENT TEMPERATURE",Tambient
1110 SUBEND
1120 !
1130 !
1140 !
1150 SUB Enter_rfr(Rf,Rc)
1160     INPUT "ENTER THE VALUE OF Rf",Rf
1170     INPUT "ENTER THE VALUE OF Rc",Rc
1180 SUBEND
1190 !
1200 !
1210 !
1220 SUB Enter_rs(Rs)
1230     INPUT "ENTER THE VALUE OF Rs (close to 100k)",Rs
1240 SUBEND
1250 SUB Vr(Vr)
1260     INPUT "ENTER THE VALUE OF THE REFERENCE VOLTAGE",Vr
1270 SUBEND

```



```

1280 !
1290 !
1300 !
1310 SUB Print
1320 !
1330 !     **** Compute the component values and print them. ****
1340 !
1350 COM Tmax,Tmin,Vmax,Vmin,Tambient,Rs,Rg,Rc,Rf,Vr,Rt,Rr,Tot_gain
1360 PRINT CHR$(12) ! Clear the screen.
1370 !
1380 Va=4.585E-8 ! The coefficients of the second order fit of the
1390 Vb=5.865E-5 ! thermocouple voltage to the temperature.
1400 !
1410 !     Compute the total gain, the pre-amp gain, AD521 gain, and Rg.
1420 Tot_gain=(Vmax-Vmin)/(FNVtc(Tmax,Tambient)-FNVtc(Tmin,Tambient))
1430 K1=1+2*Rf/Rc
1440 K2=Tot_gain/K1
1450 Rg=Rs/K2
1460 !
1470 !
1480 !     Compute the value of the feedback resistor in the reference
1490 !     junction compensator and then the reference voltage resistor.
1500 Rt=Tot_gain*(2*Va*Tambient+Vb)*(1.E+6)
1510 Vcomp_ta=Vmin-Tot_gain*FNVtc(Tmin,Tambient)
1520 Vr_over_rr=(Tambient+273.2)*(1.0E-6)-Vcomp_ta/Rt
1530 Rr=Vr/Vr_over_rr
1540 T_vcomp0=Vr_over_rr*(1.0E+6)-273.2
1550 !
1560 !
1570 !     Display the results.
1580 PRINT USING "2(K,DDD.DD)";"TEMPERATURE RANGE: ",Tmin," TO ",Tmax
1590 PRINT USING "/,4(K)";" Vo(",Tmin,",0) = ",Vmin
1600 PRINT USING "4(K)";" Vo(",Tmax,",0) = ",Vmax
1610 PRINT USING "2(K)";"Tambient = ",Tambient
1620 PRINT USING "/,K,DDDD.DD";"TOTAL GAIN = ",Tot_gain
1630 PRINT USING "K";" K1 = ",K1
1640 PRINT USING "K";" K2 = ",K2
1650 PRINT USING "2(K,MD.DDE)";"Rc = ",Rc," Rf = ",Rf
1660 PRINT USING "2(K,MD.DDE)";"Rs = ",Rs," Rg = ",Rg
1670 PRINT USING "/,K,D&D.DDDD";"VOLTAGE REFERENCE = ",Vr
1680 PRINT USING "2(K,MD.DDE)";"Rr = ",Rr," Rt = ",Rt
1690 PRINT USING "/,K,MD.DD";"Tref(Vcomp=0) = ",T_vcomp0
1700 !
1710 !     If Rr is a negative resistance the reference voltage must be
1720 !     changed in polarity.
1730 IF Rr<0 THEN
1740 BEEP
1750 PRINT USING "/,K";"THE SIGN OF Vr MUST BE CHANGED IN ORDER TO"
1760 PRINT "HAVE A POSITIVE Rr!"
1770 END IF
1780 SUBEND
1790 SUB Print_results
1800 COM Tmax,Tmin,Vmax,Vmin,Tambient,Rs,Rg,Rc,Rf,Vr,Rt,Rr,Tot_gain
1810 DIM Printer(1:3)
1820 Printer(1)=1
1830 Printer(2)=701
1840 Printer(3)=9
1850 PRINT CHR$(12)
1860 PRINT "1. CRT"
1870 PRINT "2. HP Thermal printer."
1880 PRINT "3. DecWriter."
1890 A=1
1900 INPUT "WHICH PRINTER DO YOU WANT? 1,2,3",A
1910 PRINTER IS Printer(A)
1920 IF A=2 THEN

```

```

1930      PRINT CHR$(27)&"a1L"
1940  END IF
1950  CALL Print
1960  PRINT USING "3/"
1970  !
1980  !      Print the transducer output voltages.
1990  !      **** The output voltage of the reference junction
compensator. ****
2000  PRINT
2010  PRINT "      |";
2020  FOR I=0 TO .9 STEP .1
2030  PRINT USING "#,K,.D,K"; "      ",I,"      .|"
2040  NEXT I
2050  PRINT USING "/, #, ""      |""",10("-----|""")
2060  FOR I=INT(Tambient-5) TO INT(Tambient+15)
2070  PRINT USING "/, #,MOD,K";I,"---|"
2080  FOR J=0 TO .9 STEP .1
2090  Temp=I+J
2100  Vout=((Temp+273.2)*1.0E-6-Vr/Rr)*Rt
2110  IF Vout>-10 THEN
2120  PRINT USING "#,DD.DDD,K";Vout,"|"
2130  ELSE
2140  PRINT USING "#,K";"***.***|"
2150  END IF
2160  NEXT J
2170  NEXT I
2180  PRINT USING "/, ""      -""",10("-----""")
2190  !
2200  !      Print the transducer output voltages.
2210  PRINT USING "3/"
2220  PRINT "      **** The respiratory temperature transducer output
voltage. ****"
2230  PRINT
2240  PRINT "      |";
2250  FOR I=0 TO .9 STEP .1
2260  PRINT USING "#,K,.D,K"; "      ",I,"      |"
2270  NEXT I
2280  PRINT USING "/, #, ""      |""",10("-----|""")
2290  FOR I=INT(Tmin-5) TO INT(Tmax+5)
2300  PRINT USING "/, #,MOD,K";I,"---|"
2310  FOR J=0 TO .9 STEP .1
2320  Temp=I+J
2330  Vout=Tot_gain*FNVtc(Temp,Tambient)+((Tambient+273.2)*1.E-6-
Vr/Rr)*Rt
2340  IF Vout>-10 THEN
2350  PRINT USING "#,DD.DDD,K";Vout,"|"
2360  ELSE
2370  PRINT USING "#,K";"***.***|"
2380  END IF
2390  NEXT J
2400  NEXT I
2410  PRINT USING "/, ""      -""",10("-----""")
2420  PRINTER IS 1
2430  SUBEND
2440  !
2450  !
2460  !
2470  DEF FNVtc(Tj,Tref)
2480  Va=4.585E-8
2490  Vb=5.865E-5
2500  Vc=1.9807E-7
2510  Vtc=Va*Tj^2+Vb*Tj+Vc-(Va*Tref^2+Vb*Tref+Vc)
2520  RETURN Vtc
2530  FNEND

```

A Computer-Based Respiratory Measurement System
and a Temperature Transducer for
Monitoring Respiratory Flow Temperature

by

MICHAEL HARRY MASTERS

B.S., Kansas State University, 1982

AN ABSTRACT OF A MASTER'S THESIS

submitted in partial fulfillment of the requirements
for the degree

MASTER OF SCIENCE

Department of Electrical and Computer Engineering

KANSAS STATE UNIVERSITY
Manhattan, Kansas

1985

Abstract

Breath-by-breath respiratory function studies require an accurate means of computing inspiratory and expiratory volumes, from which the ventilation values are computed. Most important in these calculations is the attainment of a valid respiratory flow signal under known temperature and pressure conditions. A computer based respiratory measurement system (CBRMS) having the ability to monitor respiratory flow, fractional O_2 , and fractional CO_2 has been enhanced with a respiratory flow temperature transducer and with gas viscosity calculations. These enhancements allow for more accurate volume calculations. Also the display of the results has been enhanced.

A rapidly responding temperature transducer based on a chromel-constantan (type E), 0.001 in. diameter, thermocouple is designed and incorporated into the CBRMS for monitoring respiratory flow temperature. The instantaneous flow gas viscosity is calculated with this temperature signal, the fractional O_2 signal, the fractional CO_2 signal, the ambient conditions, and the calculated water vapor signal. This viscosity is used to compute respiratory flow from the pneumotachograph differential pressure signal, a signal previously assumed to be directly proportional to the flow, in accordance with Poiseuille's law. The temperature signal, water vapor signal, and the barometric pressure are used to convert this flow to STPD conditions. The STPD flow is multiplied by the dry gas concentrations. These products are integrated to obtain the inspiratory and expiratory gas volumes. The difference of these inspiratory and expiratory volumes yields O_2 consumed and CO_2 produced. Inspiratory and expiratory tidal volumes are obtained by integrating the STPD flow and scaling to BTPS conditions. Other ventilation values are computed from these volumes and the respiratory cycle time. These breath-by-breath values may be displayed as the respiratory data are being analyzed and in a variety of formats post-analysis. The mean respiratory variables for the entire analyzed data are displayed post-analysis.

The averages of a specified number of consecutive breath-by-breath values or the average of the breath-by-breath values appearing in a specified time window may then be displayed graphically or printed in a tabular format. The window averages can be computed for specific points in time and compared to window averages of another subject or another exercise regimen.